## Data Sheet

 AD8601/AD8602/AD8604
## FEATURES

Low offset voltage: $\mathbf{5 0 0} \boldsymbol{\mu \mathrm { V }}$ maximum<br>Single-supply operation: 2.7 V to 5.5 V<br>Low supply current: $\mathbf{7 5 0} \mu \mathrm{A} /$ Amplifier<br>Wide bandwidth: 8 MHz<br>Slew rate: $5 \mathrm{~V} / \mu \mathrm{s}$<br>Low distortion<br>No phase reversal<br>Low input currents<br>Unity-gain stable<br>Qualified for automotive applications

## APPLICATIONS

## Current sensing

Barcode scanners
PA controls
Battery-powered instrumentation
Multipole filters
Sensors
ASIC input or output amplifiers
Audio

## GENERAL DESCRIPTION

The AD8601, AD8602, and AD8604 are single, dual, and quad rail-to-rail, input and output, single-supply amplifiers featuring very low offset voltage and wide signal bandwidth. These amplifiers use a new, patented trimming technique that achieves superior performance without laser trimming. All are fully specified to operate on a 3 V to 5 V single supply.
The combination of low offsets, very low input bias currents, and high speed make these amplifiers useful in a wide variety of applications. Filters, integrators, diode amplifiers, shunt current sensors, and high impedance sensors all benefit from the combination of performance features. Audio and other ac applications benefit from the wide bandwidth and low distortion. For the most cost-sensitive applications, the D grades offer this ac performance with lower dc precision at a lower price point.
Applications for these amplifiers include audio amplification for portable devices, portable phone headsets, bar code scanners, portable instruments, cellular PA controls, and multipole filters.
The ability to swing rail-to-rail at both the input and output enables designers to buffer CMOS ADCs, DACs, ASICs, and other wide output swing devices in single-supply systems.

## PIN CONFIGURATIONS



Figure 1. 5-Lead SOT-23 (RJ Suffix)


Figure 2. 8-Lead MSOP (RM Suffix) and 8-Lead SOIC (R-Suffix)


Figure 3. 14-Lead TSSOP (RU Suffix) and 14-Lead SOIC (R Suffix)


Figure 4. 16-Lead Shrink Small Outline QSOP (RQ Suffix)
The AD8601, AD8602, and AD8604 are specified over the extended industrial $\left(-40^{\circ} \mathrm{C}\right.$ to $\left.+125^{\circ} \mathrm{C}\right)$ temperature range. The AD8601, single, is available in a tiny, 5 -lead SOT-23 package. The AD8602, dual, is available in 8-lead MSOP and 8-lead, narrow SOIC surface-mount packages. The AD8604, quad, is available in 14-lead TSSOP, 14-lead SOIC, and 16-lead QSOP packages. See the Ordering Guide for automotive grades.

One Technology Way, P.O. Box 9106, Norwood, MA 02062-9106, U.S.A. Tel: 781.329.4700 ©2000-2020 Analog Devices, Inc. All rights reserved. Technical Support www.analog.com

## AD8601/AD8602/AD8604

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## SPECIFICATIONS

## ELECTRICAL CHARACTERISTICS

$\mathrm{V}_{\mathrm{S}}=3 \mathrm{~V}, \mathrm{~V}_{\mathrm{CM}}=\mathrm{V}_{\mathrm{S}} / 2, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.
Table 1.


[^0]$\mathrm{V}_{\mathrm{S}}=5.0 \mathrm{~V}, \mathrm{~V}_{\mathrm{CM}}=\mathrm{V}_{\mathrm{S}} / 2, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.
Table 2.


## ABSOLUTE MAXIMUM RATINGS

Table 3.

| Parameter | Rating |
| :--- | :--- |
| Supply Voltage | 6 V |
| Input Voltage | GND to V s |
| Differential Input Voltage | $\pm 6 \mathrm{~V}$ |
| Storage Temperature Range | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Operating Temperature Range | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| Junction Temperature Range | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Lead Temperature Range (Soldering, 60 sec ) | $300^{\circ} \mathrm{C}$ |
| ESD | 2 kV HBM |

Stresses at or above those listed under Absolute Maximum Ratings may cause permanent damage to the product. This is a stress rating only; functional operation of the product at these or any other conditions above those indicated in the operational section of this specification is not implied. Operation beyond the maximum operating conditions for extended periods may affect product reliability.

## THERMAL RESISTANCE

$\theta_{\text {IA }}$ is specified for worst-case conditions, that is, a device soldered onto a circuit board for surface-mount packages using a standard 4-layer board.

Table 4. Thermal Resistance

| Package Type | $\boldsymbol{\theta}_{\mathrm{JA}}$ | $\boldsymbol{\theta}_{\mathbf{\prime}}$ | Unit |
| :--- | :--- | :--- | :--- |
| 5-Lead SOT-23 (RJ) | 190 | 92 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| 8-Lead SOIC (R) | 120 | 45 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| 8-Lead MSOP (RM) | 142 | 45 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| 14-Lead SOIC (R) | 115 | 36 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| 14-Lead TSSOP (RU) | 112 | 35 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| 16-Lead QSOP (RQ) | 115 | 36 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |

## ESD CAUTION

|  | ESD (electrostatic discharge) sensitive device. <br> Charged devices and circuit boards can discharge <br> without detection. Although this product features <br> patented or proprietary protection circuitry, damage <br> may occur on devices subjected to high energy ESD. <br> Therefore, proper ESD precautions should be taken to <br> avoid performance degradation or loss of functionality. |
| :--- | :--- |

## TYPICAL PERFORMANCE CHARACTERISTICS



Figure 5. Input Offset Voltage Distribution


Figure 6. Input Offset Voltage Distribution


Figure 7. Input Offset Voltage Drift Distribution


Figure 8. Input Offset Voltage Drift Distribution


Figure 9. Input Offset Voltage vs. Common-Mode Voltage


Figure 10. Input Offset Voltage vs. Common-Mode Voltage


Figure 11. Input Bias Current vs. Temperature


Figure 12. Input Bias Current vs. Temperature


Figure 13. Input Bias Current vs. Common-Mode Voltage


Figure 14. Input Offset Current vs. Temperature


Figure 15. Input Offset Current vs. Temperature


Figure 16. Output Voltage to Supply Rail vs. Load Current


Figure 17. Output Voltage to Supply Rail vs. Load Current


Figure 18. Output Voltage Swing vs. Temperature


Figure 19. Output Voltage Swing vs. Temperature


Figure 20. Output Voltage Swing vs. Temperature


Figure 21. Output Voltage Swing vs. Temperature


Figure 22. Open-Loop Gain and Phase vs. Frequency


Figure 23. Open-Loop Gain and Phase vs. Frequency


Figure 24. Closed-Loop Gain vs. Frequency


Figure 25. Closed-Loop Gain vs. Frequency


Figure 26. Closed-Loop Output Voltage Swing vs. Frequency


Figure 27. Closed-Loop Output Voltage Swing vs. Frequency


Figure 28. Output Impedance vs. Frequency


Figure 29. Output Impedance vs. Frequency


Figure 30. Common-Mode Rejection Ratio vs. Frequency


Figure 31. Common-Mode Rejection Ratio vs. Frequency


Figure 32. Power Supply Rejection Ratio vs. Frequency


Figure 33. Small Signal Overshoot vs. Load Capacitance


Figure 34. Small Signal Overshoot vs. Load Capacitance


Figure 35. Supply Current per Amplifier vs. Temperature


Figure 36. Supply Current per Amplifier vs. Temperature


Figure 37. Supply Current per Amplifier vs. Supply Voltage


Figure 38. Total Harmonic Distortion + Noise vs. Frequency


Figure 39. Voltage Noise Density vs. Frequency


Figure 40. Voltage Noise Density vs. Frequency


Figure 41. Voltage Noise Density vs. Frequency


Figure 42. Voltage Noise Density vs. Frequency


Figure 43. 0.1 Hz to 10 Hz Input Voltage Noise


Figure 44. 0.1 Hz to 10 Hz Input Voltage Noise


Figure 45. Small Signal Transient Response


Figure 46. Small Signal Transient Response


Figure 47. Large Signal Transient Response


Figure 48. Large Signal Transient Response


Figure 49. No Phase Reversal


Figure 50. No Phase Reversal


Figure 51. Settling Time


Figure 52. Output Swing vs. Settling Time


Figure 53. Output Swing vs. Settling Time

## THEORY OF OPERATION

The AD8601/AD8602/AD8604 family of amplifiers are rail-to-rail input and output, precision CMOS amplifiers that operate from 2.7 V to 5.0 V of the power supply voltage. These amplifiers use Analog Devices, Inc., DigiTrim ${ }^{\circ}$ technology to achieve a higher degree of precision than available from most CMOS amplifiers. DigiTrim technology is a method of trimming the offset voltage of the amplifier after it has been assembled. The advantage in postpackage trimming lies in the fact that it corrects any offset voltages due to the mechanical stresses of assembly. This technology is scalable and used with every package option, including the 5-lead SOT-23, providing lower offset voltages than previously achieved in these small packages.

The DigiTrim process is completed at the factory and does not add additional pins to the amplifier. All AD860x amplifiers are available in standard op amp pinouts, making DigiTrim completely transparent to the user. The AD860x can be used in any precision op amp application.
The input stage of the amplifier is a true rail-to-rail architecture, allowing the input common-mode voltage range of the op amp to extend to both positive and negative supply rails. The voltage swing of the output stage is also rail-to-rail and is achieved by using an NMOS and PMOS transistor pair connected in a common-source configuration. The maximum output voltage swing is proportional to the output current, and larger currents limit how close the output voltage can get to the supply rail, which is a characteristic of all rail-to-rail output amplifiers. With 1 mA of output current, the output voltage can reach within 20 mV of the positive rail and within 15 mV of the negative rail. At light loads of $>100 \mathrm{k} \Omega$, the output swings within $\sim 1 \mathrm{mV}$ of the supplies.
The open-loop gain of the AD860x is 80 dB , typical, with a load of $2 \mathrm{k} \Omega$. Because of the rail-to-rail output configuration, the gain of the output stage and the open-loop gain of the amplifier are dependent on the load resistance. Open-loop gain decreases with smaller load resistances. Again, this is a characteristic inherent to all rail-to-rail output amplifiers.

## RAIL-TO-RAIL INPUT STAGE

The input common-mode voltage range of the AD860x extends to both the positive and negative supply voltages. This maximizes the usable voltage range of the amplifier, an important feature for single-supply and low voltage applications. This rail-to-rail input range is achieved by using two input differential pairs, one NMOS and one PMOS, placed in parallel. The NMOS pair is active at the upper end of the common-mode voltage range, and the PMOS pair is active at the lower end.

The NMOS and PMOS input stages are separately trimmed using DigiTrim to minimize the offset voltage in both differential pairs. Both NMOS and PMOS input differential pairs are active in a 500 mV transition region, when the input common-mode voltage is between approximately 1.5 V and 1 V below the positive supply voltage. The input offset voltage shifts slightly in this transition region, as shown in Figure 9 and Figure 10 .The common-mode rejection ratio is also slightly lower when the input common-mode voltage is within this transition band. Compared to the Burr-Brown OPA2340UR rail-to-rail input amplifier, shown in Figure 54, the AD860x, shown in Figure 55, exhibits lower offset voltage shift across the entire input common-mode range, including the transition region.


Figure 54. Burr-Brown OPA2340UR Input Offset Voltage vs. Common-Mode Voltage, 24 SOIC Units @ $25^{\circ} \mathrm{C}$


Figure 55. AD8602AR Input Offset Voltage vs. Common-Mode Voltage, 300 SOIC Units @ $25^{\circ} \mathrm{C}$

## INPUT OVERVOLTAGE PROTECTION

As with any semiconductor device, if a condition could exist that could cause the input voltage to exceed the power supply, the device's input overvoltage characteristic must be considered. Excess input voltage energizes the internal PN junctions in the AD860x, allowing current to flow from the input to the supplies.

This input current does not damage the amplifier, provided it is limited to 5 mA or less. This can be ensured by placing a resistor in series with the input. For example, if the input voltage could exceed the supply by 5 V , the series resistor should be at least $(5 \mathrm{~V} / 5 \mathrm{~mA})=1 \mathrm{k} \Omega$. With the input voltage within the supply rails, a minimal amount of current is drawn into the inputs, which, in turn, causes a negligible voltage drop across the series resistor. Therefore, adding the series resistor does not adversely affect circuit performance.

## OVERDRIVE RECOVERY

Overdrive recovery is defined as the time it takes the output of an amplifier to come off the supply rail when recovering from an overload signal. This is tested by placing the amplifier in a closed-loop gain of 10 with an input square wave of 2 V p-p while the amplifier is powered from either 5 V or 3 V .

The AD860x has excellent recovery time from overload conditions. The output recovers from the positive supply rail within 200 ns at all supply voltages. Recovery from the negative rail is within 500 ns at a 5 V supply, decreasing to within 350 ns when the device is powered from 2.7 V .

## POWER-ON TIME

The power-on time is important in portable applications where the supply voltage to the amplifier may be toggled to shut down the device to improve battery life. Fast power-up behavior ensures that the output of the amplifier quickly settles to its final voltage, improving the power-up speed of the entire system. When the supply voltage reaches a minimum of 2.5 V , the AD860x settles to a valid output within $1 \mu \mathrm{~s}$. This turn-on response time is faster than many other precision amplifiers, which can take tens or hundreds of microseconds for their outputs to settle.

## USING THE AD8602 IN HIGH SOURCE IMPEDANCE APPLICATIONS

The CMOS rail-to-rail input structure of the AD860x allows these amplifiers to have very low input bias currents, typically 0.2 pA . This allows the AD860x to be used in any application that has a high source impedance or must use large value resistances around the amplifier. For example, the photodiode amplifier circuit shown in Figure 56 requires a low input bias current op amp to reduce output voltage error. The AD8601 minimizes offset errors due to its low input bias current and low offset voltage.

The current through the photodiode is proportional to the incident light power on its surface. The $4.7 \mathrm{M} \Omega$ resistor converts this current into a voltage, with the output of the AD8601 increasing at $4.7 \mathrm{~V} / \mu \mathrm{A}$. The feedback capacitor reduces excess noise at higher frequencies by limiting the bandwidth of the circuit to

$$
\begin{equation*}
B W=\frac{1}{2 \pi(4.7 \mathrm{M} \Omega) C_{F}} \tag{1}
\end{equation*}
$$

Using a 10 pF feedback capacitor limits the bandwidth to approximately 3.3 kHz .


Figure 56. Amplifier Photodiode Circuit

## HIGH SIDE AND LOW SIDE, PRECISION CURRENT MONITORING

Because of its low input bias current and low offset voltage, the AD860x can be used for precision current monitoring. The true rail-to-rail input feature of the AD860x allows the amplifier to monitor current on either the high side or the low side. Using both amplifiers in an AD8602 provides a simple method for monitoring both current supply and return paths for load or fault detection. Figure 57 and Figure 58 demonstrate both circuits.


Figure 57. Low-Side Current Monitor


Figure 58. High-Side Current Monitor

Voltage drop is created across the $0.1 \Omega$ resistor that is proportional to the load current. This voltage appears at the inverting input of the amplifier due to the feedback correction around the op amp. This creates a current through R1, which in turn, pulls current through R2. For the low side monitor, the monitor output voltage is given by

$$
\begin{equation*}
\text { Monitor Output }=3 V-\left[R 2 \times\left(\frac{R_{\text {SENSE }}}{R 1}\right) \times I_{L}\right] \tag{2}
\end{equation*}
$$

For the high side monitor, the monitor output voltage is

$$
\begin{equation*}
\text { Monitor Output }=R 2 \times\left(\frac{R_{\text {SENSE }}}{R 1}\right) \times I_{L} \tag{3}
\end{equation*}
$$

Using the components shown, the monitor output transfer function is $2.5 \mathrm{~V} / \mathrm{A}$.

## USING THE AD8601 IN SINGLE-SUPPLY, MIXED SIGNAL APPLICATIONS

Single-supply, mixed signal applications requiring 10 or more bits of resolution demand both a minimum of distortion and a maximum range of voltage swing to optimize performance. To ensure that the ADCs or DACs achieve their best performance, an amplifier often must be used for buffering or signal conditioning. The $750 \mu \mathrm{~V}$ maximum offset voltage of the AD8601 allows the amplifier to be used in 12-bit applications powered from a 3 V single supply, and its rail-to-rail input and output ensure no signal clipping.
Figure 59 shows the AD8601 used as an input buffer amplifier to the AD7476, a 12-bit, 1 MSPS ADC. As with most ADCs, total harmonic distortion (THD) increases with higher source impedances. By using the AD8601 in a buffer configuration, the low output impedance of the amplifier minimizes THD while the high input impedance and low bias current of the op amp minimizes errors due to source impedance. The 8 MHz gain bandwidth product of the AD8601 ensures no signal attenuation up to 500 kHz , which is the maximum Nyquist frequency for the AD7476.


Figure 59. A Complete 3 V 12-Bit 1 MHz Analog-to-Digital Conversion System

Figure 60 demonstrates how the AD8601 can be used as an output buffer for the DAC for driving heavy resistive loads. The AD5320 is a 12 -bit DAC that can be used with clock frequencies up to 30 MHz and signal frequencies up to 930 kHz . The rail-to-rail output of the AD8601 allows it to swing within 100 mV of the positive supply rail while sourcing 1 mA of current. The total current drawn from the circuit is less than 1 mA , or 3 mW from a 3 V single supply.


Figure 60. Using the AD8601 as a DAC Output Buffer to Drive Heavy Loads
The AD8601, AD7476, and AD5320 are all available in spacesaving SOT-23 packages.

## PC100 COMPLIANCE FOR COMPUTER AUDIO APPLICATIONS

Because of its low distortion and rail-to-rail input and output, the AD860x is an excellent choice for low cost, single-supply audio applications, ranging from microphone amplification to line output buffering. Figure 38 shows the total harmonic distortion plus noise (THD +N ) figures for the AD860x. In unity gain, the amplifier has a typical THD +N of $0.004 \%$, or -86 dB , even with a load resistance of $600 \Omega$. This is compliant with the PC100 specification requirements for audio in both portable and desktop computers.

Figure 61 shows how an AD8602 can be interfaced with an AC'97 codec to drive the line output. Here, the AD8602 is used as a unity-gain buffer from the left and right outputs of the AC'97 codec. The $100 \mu \mathrm{~F}$ output coupling capacitors block dc current and the $20 \Omega$ series resistors protect the amplifier from short circuits at the jack.


Figure 61. A PC100-Compliant Line Output Amplifier

## AD8601/AD8602/AD8604

## SPICE MODEL

The SPICE macro-model for the AD860x amplifier can be downloaded at www.analog.com. The model accurately simulates a number of both dc and ac parameters, including open-loop gain, bandwidth, phase margin, input voltage range, output voltage swing vs. output current, slew rate, input voltage noise, CMRR, PSRR, and supply current vs. supply voltage. The model is optimized for performance at $27^{\circ} \mathrm{C}$. Although it functions at different temperatures, it may lose accuracy with respect to the actual behavior of the AD860x.

## OUTLINE DIMENSIONS




COMPLIANT TO JEDEC STANDARDS MS-012-AA CONTROLLING DIMENSIONS ARE IN MILLIMETERS; INCH DIMENSIONS (IN PARENTHESES) ARE ROUNDED-OFF MILLIMETER EQUIVALENTS FOR REFERENCE ONLY AND ARE NOT APPROPRIATE FOR USE IN DESIGN.

Figure 64. 8-Lead Standard Small Outline Package [SOIC_N] (R-8)
Dimensions shown in millimeters and (inches)


COMPLIANT TO JEDEC STANDARDS MS-012-AB
CONTROLLING DIMENSIONS ARE IN MILLIMETERS; INCH DIMENSIONS (IN PARENTHESES) ARE ROUNDED-OFF MILLIMETER EQUIVALENTS FOR REFERENCE ONLY AND ARE NOT APPROPRIATE FOR USE IN DESIGN.

Figure 65. 14-Lead Standard Small Outline Package [SOIC_N] ( $R$-14)
Dimensions shown in millimeters and (inches)


Figure 66. 14-Lead Thin Shrink Small Outline Package [TSSOP] (RU-14)
Dimensions shown in millimeters


COMPLIANT TO JEDEC STANDARDS MO-137-AB
CONTROLLING DIMENSIONS ARE IN INCHES; MILLIMETER DIMENSIONS (IN PARENTHESES) ARE ROUNDED-OFF INCH EQUIVALENTS FOR REFERENCE ONLY AND ARE NOT APPROPRIATE FOR USE IN DESIGN

Figure 67. 16-Lead Shrink Small Outline Package [QSOP] (RQ-16)
Dimensions shown in inches and (millimeters)

## ORDERING GUIDE

| Model ${ }^{1,2}$ | Temperature Range | Package Description | Package Option | Branding |
| :---: | :---: | :---: | :---: | :---: |
| AD8601ARTZ-R2 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 5-Lead SOT-23 | RJ-5 | AAA |
| AD8601ARTZ-REEL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 5-Lead SOT-23 | RJ-5 | AAA |
| AD8601ARTZ-REEL7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 5-Lead SOT-23 | RJ-5 | AAA |
| AD8601WARTZ-RL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 5-Lead SOT-23 | RJ-5 | AAA |
| AD8601WARTZ-R7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 5-Lead SOT-23 | RJ-5 | AAA |
| AD8601WDRTZ-REEL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 5-Lead SOT-23 | RJ-5 | AAD |
| AD8601WDRTZ-REEL7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 5-Lead SOT-23 | RJ-5 | AAD |
| AD8602AR | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8602AR-REEL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8602AR-REEL7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8602ARZ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8602ARZ-REEL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8602ARZ-REEL7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8602WARZ-RL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8602WARZ-R7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8602ARM-REEL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead MSOP | RM-8 | ABA |
| AD8602ARMZ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead MSOP | RM-8 | ABA |
| AD8602ARMZ-REEL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead MSOP | RM-8 | ABA |
| AD8602DR | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8602DR-REEL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8602DR-REEL7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8602DRZ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8602DRZ-REEL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8602DRZ-REEL7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8602DRM-REEL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead MSOP | RM-8 | ABD |
| AD8602DRMZ-REEL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead MSOP | RM-8 | ABD |
| AD8604ARZ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 14-Lead SOIC_N | R-14 |  |
| AD8604WARZ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 14-Lead SOIC_N | R-14 |  |
| AD8604ARZ-REEL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 14-Lead SOIC_N | R-14 |  |
| AD8604ARZ-REEL7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 14-Lead SOIC_N | R-14 |  |
| AD8604WARZ-RL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 14-Lead SOIC_N | R-14 |  |
| AD8604DRZ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 14-Lead SOIC_N | R-14 |  |
| AD8604DRZ-REEL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 14-Lead SOIC_N | R-14 |  |
| AD8604ARUZ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 14-Lead TSSOP | RU-14 |  |
| AD8604ARUZ-REEL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 14-Lead TSSOP | RU-14 |  |
| AD8604DRU | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 14-Lead TSSOP | RU-14 |  |
| AD8604DRU -REEL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 14-Lead TSSOP | RU-14 |  |
| AD8604DRUZ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 14-Lead TSSOP | RU-14 |  |
| AD8604DRUZ-REEL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 14-Lead TSSOP | RU-14 |  |
| AD8604ARQZ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 16-Lead QSOP | RQ-16 |  |
| AD8604ARQZ-RL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 16-Lead QSOP | RQ-16 |  |
| AD8604ARQZ-R7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 16-Lead QSOP | RQ-16 |  |

${ }^{1} \mathrm{Z}=$ RoHS Compliant Part.
${ }^{2} \mathrm{~W}=$ Qualified for Automotive Applications.

## AUTOMOTIVE PRODUCTS

The AD8601W/AD8602W/AD8604W models are available with controlled manufacturing to support the quality and reliability requirements of automotive applications. Note that these automotive models may have specifications that differ from the commercial models; therefore, designers should review the Specifications section of this data sheet carefully. Only the automotive grade products shown are available for use in automotive applications. Contact your local Analog Devices Account Representative for specific product ordering information and to obtain the specific Automotive Reliability reports for these models.
Data Sheet AD8601/AD8602/AD8604

NOTES


[^0]:    ${ }^{1}$ For $\mathrm{V}_{\mathrm{Cm}}$ between 1.3 V and 1.8 V , V os may exceed specified value.

