## FEATURES

Low offset voltage<br>B grade: 0.4 mV maximum (ADA4610-1/ADA4610-2 only)<br>A grade: 1 mV maximum<br>Low offset voltage drift<br>B grade: $2 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ maximum (ADA4610-1/ADA4610-2 only)<br>A grade: $\mathbf{8 \mu V} /{ }^{\circ} \mathrm{C}$ maximum (SOIC, MSOP, LFCSP packages)<br>Low input bias current: 5 pA typical<br>Dual-supply operation: $\pm 5 \mathrm{~V}$ to $\pm 15 \mathrm{~V}$<br>Low voltage noise: $0.45 \boldsymbol{\mu V}$ p-p at 0.1 Hz to 10 Hz<br>Voltage noise density: $\mathbf{7 . 3 0} \mathbf{n V} / \sqrt{ } \mathrm{Hz}$ at $\mathrm{f}=\mathbf{1} \mathbf{~ k H z}$<br>Low THD + N: 0.00025\%<br>No phase reversal<br>Rail-to-rail output<br>Unity-gain stable<br>Long-term offset voltage drift (10,000 hours): $5 \boldsymbol{\mu V}$ typical<br>Temperature hysteresis: $\mathbf{8 \mu V}$ typical

## APPLICATIONS

## Instrumentation

Medical instruments
Multipole filters
Precision current measurement
Photodiode amplifiers

## Sensors

Audio

## GENERAL DESCRIPTION

The ADA4610-1/ADA4610-2/ADA4610-4 are precision junction field effect transistor (JFET) amplifiers that feature low input noise voltage, current noise, offset voltage, input bias current, and rail-torail output. The ADA4610-1 is a single amplifier, the ADA4610-2 is a dual amplifier, and the ADA4610-4 is a quad amplifier.

The combination of low offset, noise, and very low input bias current makes these amplifiers especially suitable for high impedance sensor amplification and precise current measurements using shunts. With excellent dc precision, low noise, and fast settling time, the ADA4610-1/ADA4610-2/ADA4610-4 provide superior accuracy in medical instruments, electronic measurement, and automated test equipment. Unlike many competitive amplifiers, the ADA4610-1/ADA4610-2/ADA4610-4 maintain fast settling performance with substantial capacitive loads. Unlike many older JFET amplifiers, the ADA4610-1/ADA4610-2/ ADA4610-4 do not suffer from output phase reversal when input voltages exceed the maximum common-mode voltage range.
The fast slew rate and great stability with capacitive loads make the ADA4610-1/ADA4610-2/ADA4610-4 ideal for high

## Rev.I

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PIN CONFIGURATION


Figure 1. ADA4610-2 8-Lead SOIC (R Suffix); for Additional Packages and Models, See the Pin Configurations and Function Descriptions Section
performance filters. Low input bias currents, low offset, and low noise result in a wide dynamic range for photodiode amplifier circuits. Low noise and distortion, high output current, and excellent speed make the ADA4610-1/ADA4610-2/ ADA4610-4 great choices for audio applications.
The ADA4610-1/ADA4610-2/ADA4610-4 are specified over the $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ extended industrial temperature range.
The ADA4610-1 is available in an 8-lead SOIC package and in a 5-lead SOT-23 package. The ADA4610-2 is available in 8-lead SOIC, 8-lead MSOP, and 8-lead LFCSP packages. The ADA4610-4 is available in a 14 -lead SOIC package and in a 16-lead LFCSP.

Table 1. Related Precision JFET Operational Amplifiers

| Single | Dual | Quad |
| :--- | :--- | :--- |
| AD8510 | AD8512 | AD8513 |
| AD8610 | AD8620 | Not applicable |
| AD820 | AD822 | AD824 |
| ADA4627-1/ADA4637-1 | Not applicable | Not applicable |
| Not applicable | ADA4001-2 | Not applicable |

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## TABLE OF CONTENTS

Features .....  .1
Applications. .....  1
Pin Configuration .....  1
General Description ..... 1
Revision History ..... 3
Specifications ..... 4
Electrical Characteristics ..... 5
Absolute Maximum Ratings ..... 7
Thermal Resistance ..... 7
ESD Caution .....  7
Pin Configurations and Function Descriptions .....  8
Typical Performance Characteristics ..... 11
Comparative Voltage and Variable Voltage Graphs ..... 17
Theory of Operation ..... 20
Applications Information ..... 21
Input Overvoltage Protection ..... 21
Peak Detector ..... 21
Current to Voltage (I to V) Conversion Applications .....  21
Comparator Operation ..... 22
Long-Term Drift ..... 23
Temperature Hysteresis ..... 23
Outline Dimensions ..... 24
Ordering Guide ..... 27

## REVISION HISTORY

6/2019—Rev. H to Rev. I
Change to Features Section 1
Change to Offset Voltage Drift, B Grade (ADA4610-1/ ADA4610-2) Parameter, Table 2 .....  4
Change to Offset Voltage Drift, B Grade (ADA4610-1/
ADA4610-2) Parameter, Table 3 .....  5
Replaced Figure 10 and Figure 13 ..... 11
Change to Theory of Operation Section ..... 20
5/2017—Rev. G to Rev. H
Changed CP-8-21 to CP-8-11 Throughout .....  1
Changes to Features Section
Changes to Figure 15 Caption, Figure 16 Caption, Figure 18 Caption, and Figure 19 Caption ..... 12
Changed Functional Description Section to Theory of Operation Section ..... 20
Added Long-Term Drift Section, Temperature Hysteresis Section,
Figure 61, Figure 62, and Figure 63; Renumbered Sequentially..... 23
Updated Outline Dimensions ..... 24
Changes to Ordering Guide ..... 27
5/2016-Rev. F to Rev. G
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$\qquad$
Throughout
Changes to Figure 23 Caption and Figure 26 Caption ..... 13
Updated Outline Dimensions ..... 24
Changes to Ordering Guide. ..... 25
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Added Figure 3 and Table 7; Renumbered Sequentially .....  8
Updated Outline Dimensions ..... 23
Changes to Ordering Guide ..... 25
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Added ADA4610-1 ..... Universal
Added 16-Lead LFCSP_WQ ..... Universal
Deleted Figure 1 and Figure 3; Renumbered Sequentially .....  1
Changes to Features Section .....  1
Changes to Table 2 .....  4
Changes to Table 3 .....  .5
Added Figure 2 and Table 6; Renumbered Sequentially .....  7
Added Figure 4 .....  8
Added Figure 7 .....  9
Changes to Table 8 .....  9
Changes to Figure 10 Caption and Figure 13 Caption ..... 10
Changes to Figure 14 Caption, Figure 15, Figure 17 Caption, and Figure 18 ..... 11
Changes to Figure 22 and Figure 25 ..... 12
Changes to Figure 26 to Figure 31 ..... 13
Changes to Figure 32 and Figure 35 ..... 14
Changes to Figure 38 and Figure 40 ..... 15
Changes to Figure 42 to Figure 46 ..... 16
Changes to Figure 48, Figure 50, and Figure 53 ..... 17
Changes to Figure 54 and Figure 55 ..... 18
Changes to Figure 57 and Figure 58 ..... 20
Updated Outline Dimensions ..... 22
Added Figure 64 ..... 23
Changes to Ordering Guide ..... 24
11/2014—Rev. C to Rev. D
Change to Figure 56 ..... 19
5/2014—Rev. B to Rev. C
Added ADA4610-4 and 14-Lead SOIC ..... Universal
Added Voltage Noise Density to Features Section, Figure 3, and
Table 1; Renumbered Sequentially .....  1
Changes to Table 2 ..... 3
Changes to Table 3 ..... 4
Changes to Table 4 ..... 6
Added Pin Configurations and Function Descriptions Section, Figure 4 to Figure 6, Table 6, and Table 7 .....  .7
Changes to Typical Performance Characteristics Section ..... 8
Added Functional Description Section ..... 17
Added Input Overvoltage Protection Section, Peak Detector
Section, I to V Conversion Applications Section, and Photodiode Circuits Section. ..... 18
Change to Figure 56 ..... 18
Added Figure 62, Outline Dimensions ..... 20
Changes to Ordering Guide ..... 20
8/2012-Rev. A to Rev. BChanges to Figure 98
5/2012—Rev. 0 to Rev. A
Changes to Data Sheet Title and General Description Section .. 1Changed Input Impedance Parameter, Differential to Input
Capacitance Parameter, and Differential Parameter, Table 1 .....  3
Added Input Resistance in Table 1 ..... 3
Changed Input Impedance, Differential Parameter to Input Capacitance, Differential Parameter, Table 2 ..... 4
Added Input Resistance Parameter, Table 2 ..... 4
Added Figure 9, Figure 10, and Figure 14; Renumbered Sequentially .....  8
Added Figure 15 .....  9
Updated Outline Dimensions ..... 16
Changes to Ordering Guide ..... 17
12/2011-Revision 0: Initial Version

## SPECIFICATIONS

$\mathrm{V}_{\mathrm{SY}}= \pm 5 \mathrm{~V}, \mathrm{~V}_{\mathrm{CM}}=0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.
Table 2.


| Parameter | Symbol | Test Conditions/Comments | Min | Typ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DYNAMIC PERFORMANCE <br> Slew Rate <br> Rising <br> Falling <br> Gain Bandwidth Product <br> Unity-Gain Crossover <br> Phase Margin <br> -3 dB Closed-Loop Bandwidth <br> Total Harmonic Distortion + Noise | $\begin{aligned} & \pm \mathrm{SR} \\ & \\ & \text { GBP } \\ & \text { UGC } \\ & \varphi_{M} \\ & -3 \mathrm{~dB} \\ & \mathrm{THD}+\mathrm{N} \end{aligned}$ | $\begin{aligned} & R_{L}=2 \mathrm{k} \Omega, A_{v}=1 \\ & V_{\mathbb{N}}=5 \mathrm{mV} p-p, R_{L}=2 \mathrm{k} \Omega, A_{v}=100 \\ & \mathrm{~V}_{\mathbb{N}}=5 \mathrm{mV} p-\mathrm{p}, \mathrm{R}_{\mathrm{L}}=2 \mathrm{k} \Omega, A_{V}=1 \\ & A_{V}=1, \mathrm{~V}_{\mathbb{N}}=5 \mathrm{mV} p-\mathrm{p} \\ & 1 \mathrm{kHz}, A_{V}=1, R_{L}=2 \mathrm{k} \Omega, \mathrm{~V}_{\mathbb{N}}=1 \mathrm{Vrms} \end{aligned}$ | $\begin{aligned} & 15^{1} \\ & 15^{1} \end{aligned}$ | $\begin{aligned} & 21 \\ & 46 \\ & 15.4 \\ & 9.3 \\ & 61 \\ & 10.6 \\ & 0.00025 \end{aligned}$ |  | $\mathrm{V} / \mu \mathrm{s}$ <br> $\mathrm{V} / \mu \mathrm{s}$ <br> MHz <br> MHz <br> Degrees <br> MHz <br> \% |
| NOISE PERFORMANCE Voltage Noise Voltage Noise Density | $\begin{aligned} & e_{n} p-p \\ & e_{n} \end{aligned}$ | $\begin{aligned} & 0.1 \mathrm{~Hz} \text { to } 10 \mathrm{~Hz} \\ & \mathrm{f}=10 \mathrm{~Hz} \\ & \mathrm{f}=100 \mathrm{~Hz} \\ & \mathrm{f}=1 \mathrm{kHz} \\ & \mathrm{f}=10 \mathrm{kHz} \end{aligned}$ |  | $\begin{aligned} & 0.45 \\ & 14 \\ & 8.20 \\ & 7.30 \\ & 7.30 \end{aligned}$ |  | $\mu \mathrm{V}$ p-p <br> $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ <br> $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ <br> $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ <br> $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ |

${ }^{1}$ Guaranteed by design and characterization.

## ELECTRICAL CHARACTERISTICS

$\mathrm{V}_{\mathrm{SY}}= \pm 15 \mathrm{~V}, \mathrm{~V}_{\mathrm{CM}}=0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.
Table 3.

| Parameter | Symbol | Test Conditions/Comments | Min | Typ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| INPUT CHARACTERISTICS |  |  |  |  |  |  |
| Offset Voltage | Vos |  |  |  |  |  |
| B Grade (ADA4610-1/ADA4610-2) |  |  |  | 0.2 | 0.4 | mV |
|  |  | $-40^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<+125^{\circ} \mathrm{C}$ |  |  | 0.8 | mV |
| A Grade |  |  |  | 0.4 | 1 | mV |
|  |  | $-40^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<+125^{\circ} \mathrm{C}$ |  |  | 1.8 | mV |
| Offset Voltage Drift | $\Delta \mathrm{V}_{\text {os }} / \Delta \mathrm{T}$ |  |  |  |  |  |
| B Grade (ADA4610-1/ADA4610-2) ${ }^{1}$ |  |  |  | 0.5 | 2 | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| A Grade ${ }^{1}$ (SOIC, MSOP, LFCSP) |  |  |  | 1 | 8 | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| A Grade ${ }^{1}$ (SOT-23) |  |  |  | 1 | 12 | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| Input Bias Current | $I_{B}$ |  |  | 5 | 25 | pA |
|  |  | $-40^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<+125^{\circ} \mathrm{C}$ |  |  | 1.50 | nA |
| Input Offset Current | los |  |  | 2 | 20 | pA |
|  |  | $-40^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<+125^{\circ} \mathrm{C}$ |  |  | 0.25 | nA |
| Input Voltage Range |  |  | -12.5 |  | +12.5 | V |
| Common-Mode Rejection Ratio | CMRR | $\mathrm{V}_{\text {CM }}=-12.5 \mathrm{~V}$ to +12.5 V | 100 | 115 |  | dB |
|  |  | $-40^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<+125^{\circ} \mathrm{C}$ | 96 |  |  | dB |
| Large Signal Voltage GainADA4610-2 | Avo | $\mathrm{R}_{\mathrm{L}}=2 \mathrm{k} \Omega, \mathrm{V}_{\text {OUT }}= \pm 13.5 \mathrm{~V}$ |  |  |  |  |
|  |  |  | 104 | 107 |  | dB |
|  |  | $-40^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<+125^{\circ} \mathrm{C}$ | 91 |  |  | dB |
| ADA4610-1/ADA4610-4 |  |  | 102 | 104 |  | dB |
|  |  | $-40^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<+125^{\circ} \mathrm{C}$ | 86 |  |  | dB |
| Input Capacitance |  | $\mathrm{V}_{\text {CM }}=0 \mathrm{~V}$ |  |  |  |  |
| Differential |  |  |  | 3.1 |  | pF |
| Common-Mode |  |  |  | 4.8 |  | pF |
| Input Resistance |  | $\mathrm{V}_{\mathrm{Cm}}=0 \mathrm{~V}$ |  | $>10^{13}$ |  | $\Omega$ |

## ADA4610-1/ADA4610-2/ADA4610-4

| Parameter | Symbol | Test Conditions/Comments | Min | Typ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OUTPUT CHARACTERISTICS <br> Output Voltage High <br> Output Voltage Low <br> Short-Circuit Current | Voh $V_{\mathrm{oL}}$ | $\begin{aligned} & \mathrm{R}_{\mathrm{L}}=2 \mathrm{k} \Omega \\ & -40^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<+125^{\circ} \mathrm{C} \\ & \mathrm{R}_{\mathrm{L}}=600 \Omega \\ & -40^{\circ} \mathrm{C}<\mathrm{T}_{A}<+125^{\circ} \mathrm{C} \\ & \mathrm{R}_{\mathrm{L}}=2 \mathrm{k} \Omega \\ & -40^{\circ} \mathrm{C}<\mathrm{T}_{A}<+125^{\circ} \mathrm{C} \\ & \mathrm{R}_{\mathrm{L}}=600 \Omega \\ & -40^{\circ} \mathrm{C}<\mathrm{T}_{A}<+125^{\circ} \mathrm{C} \end{aligned}$ | $\begin{aligned} & 14.80 \\ & 14.65 \\ & 14.25 \\ & 13.35 \end{aligned}$ | $\begin{aligned} & 14.90 \\ & 14.47 \\ & -14.90 \\ & -14.68 \\ & \pm 79 \end{aligned}$ | $\begin{aligned} & -14.85 \\ & -14.75 \\ & -14.60 \\ & -14.30 \end{aligned}$ | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~V} \\ & \mathrm{~V} \\ & \mathrm{~V} \\ & \mathrm{~V} \\ & \mathrm{~V} \\ & \mathrm{~V} \\ & \mathrm{~V} \\ & \mathrm{~mA} \end{aligned}$ |
| POWER SUPPLY <br> Power Supply Rejection Ratio ADA4610-2 <br> ADA4610-1/ADA4610-4 <br> Supply Current per Amplifier | PSRR <br> ISY | $\begin{aligned} & \mathrm{V}_{S Y}= \pm 4.5 \mathrm{~V} \text { to } \pm 18 \mathrm{~V} \\ & -40^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<+125^{\circ} \mathrm{C} \\ & -40^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<+125^{\circ} \mathrm{C} \\ & \text { lout }=0 \mathrm{~mA} \\ & -40^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<+125^{\circ} \mathrm{C} \end{aligned}$ | $\begin{aligned} & 106 \\ & 103 \\ & 104 \\ & 100 \end{aligned}$ | $\begin{aligned} & 125 \\ & 117 \\ & 1.60 \end{aligned}$ | $\begin{aligned} & 1.85 \\ & 2.0 \end{aligned}$ | dB <br> dB <br> dB <br> dB <br> mA <br> mA |
| DYNAMIC PERFORMANCE <br> Slew Rate <br> Rising <br> Falling <br> Gain Bandwidth Product <br> Unity-Gain Crossover <br> Phase Margin <br> -3 dB Closed-Loop Bandwidth <br> Total Harmonic Distortion + Noise | $\pm$ SR GBP UGC $\varphi_{M}$ -3 dB THD $+N$ |  | $\begin{aligned} & 17^{1} \\ & 17^{1} \end{aligned}$ | $\begin{aligned} & 25 \\ & 61 \\ & 16.3 \\ & 9.3 \\ & 66 \\ & 9.5 \\ & 0.00025 \end{aligned}$ |  | $\mathrm{V} / \mu \mathrm{s}$ <br> V/ $\mu \mathrm{s}$ <br> MHz <br> MHz <br> Degrees <br> MHz <br> \% |
| NOISE PERFORMANCE <br> Peak-to-Peak Voltage Noise Voltage Noise Density | $\begin{aligned} & e_{n} p-p \\ & e_{n} \end{aligned}$ | 0.1 Hz to 10 Hz bandwidth $\begin{aligned} & f=10 \mathrm{~Hz} \\ & \mathrm{f}=100 \mathrm{~Hz} \\ & \mathrm{f}=1 \mathrm{kHz} \\ & \mathrm{f}=10 \mathrm{kHz} \end{aligned}$ |  | $\begin{aligned} & 0.45 \\ & 14 \\ & 8.50 \\ & 7.30 \\ & 7.30 \end{aligned}$ |  | $\mu \mathrm{V}$ p-p <br> $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ <br> $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ <br> $n \mathrm{~V} / \sqrt{ } \mathrm{Hz}$ <br> $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ |

[^0]
## ABSOLUTE MAXIMUM RATINGS

Table 4.

| Parameter | Rating |
| :--- | :--- |
| Supply Voltage | $\pm 18 \mathrm{~V}$ |
| Input Voltage | $\pm \mathrm{V}_{\mathrm{s}}$ |
| Input Current ${ }^{1}$ | $\pm 10 \mathrm{~mA}$ |
| Storage Temperature Range | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Operating Temperature Range | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| Junction Temperature Range | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Lead Temperature (Soldering, 10 sec) | $300^{\circ} \mathrm{C}$ |
| Electrostatic Discharge (ESD) |  |
| $\quad$ Human Body Model (HBM) |  |
| $\quad$ Field Induced Charge Device Model (FICDM) ${ }^{2}$ | 2500 V |

${ }^{1}$ The input pins have clamp diodes connected to the power supply pins. Limit the input current to 10 mA or less whenever input signals exceed the power supply rail by 0.3 V .
${ }^{2}$ ESDA/JEDEC JS-001-2011 applicable standard.
${ }^{3}$ JESD22-C101 (ESD FICDM standard of JEDEC) applicable standard.
Stresses at or above those listed under Absolute Maximum Ratings may cause permanent damage to the product. This is a stress rating only; functional operation of the product at these or any other conditions above those indicated in the operational section of this specification is not implied. Operation beyond the maximum operating conditions for extended periods may affect product reliability.

## THERMAL RESISTANCE

Table 5. Thermal Resistance

| Package Type | $\boldsymbol{\theta}_{\mathbf{J A}}{ }^{\mathbf{1}}$ | $\boldsymbol{\theta}_{\mathbf{J c}}$ | Unit |
| :--- | :--- | :--- | :--- |
| 5-Lead SOT-23 | 219.4 | 155.6 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| 8-Lead SOIC | 120 | 43 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| 8-Lead LFCSP | 57 | 12 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| 8-Lead MSOP | 142 | 45 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| 14-Lead SOIC | 115 | 36 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| 16-Lead LFCSP | 65 | 3.2 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |

${ }^{1} \theta_{\mathrm{JA}}$ is specified for worst-case conditions, that is, $\theta_{\mathrm{J}}$ is specified for a device soldered in a circuit board for surface-mount packages.

## ESD CAUTION

|  | ESD (electrostatic discharge) sensitive device. <br> Charged devices and circuit boards can discharge <br> without detection. Although this product features <br> patented or proprietary protection circuitry, damage <br> may occur on devices subjected to high energy ESD. <br> Therefore, proper ESD precautions should be taken to <br> avoid performance degradation or loss of functionality. |
| :--- | :--- |

## PIN CONFIGURATIONS AND FUNCTION DESCRIPTIONS



Figure 2. ADA4610-1 Pin Configuration, 8-Lead SOIC (R Suffix)
Table 6. ADA4610-1 Pin Function Descriptions, 8-Lead SOIC

| Pin No. | Mnemonic | Description |
| :--- | :--- | :--- |
| $1,5,8$ | NIC | Not Internally Connected. |
| 2 | - IN | Inverting Input. |
| 3 | + IN | Noninverting Input. |
| 4 | V- | Negative Supply Voltage. |
| 6 | OUT | Output. |
| 7 | V+ | Positive Supply Voltage. |



Figure 3. ADA4610-1 Pin Configuration, 5-Lead SOT-23 (RJ Suffix)
Table 7. ADA4610-1 Pin Function Descriptions, 5-Lead SOT-23

| Pin No. | Mnemonic | Description |
| :--- | :--- | :--- |
| 1 | OUT | Output. |
| 2 | V- | Negative Supply Voltage. |
| 3 | + IN | Noninverting Input. |
| 4 | - IN | Inverting Input. |
| 5 | V+ | Positive Supply Voltage. |



Figure 4. ADA4610-2 Pin Configuration, 8-Lead SOIC (R Suffix)


Figure 5. ADA4610-2 Pin Configuration, 8-Lead MSOP (RM Suffix)

notes

1. THE EXPOSED PAD MUST BE CONNECTED TO V-.

Figure 6. ADA4610-2 Pin Configuration, 8-Lead LFCSP (CP Suffix)

Table 8. ADA4610-2 Pin Function Descriptions, 8-Lead SOIC, 8-Lead MSOP, and 8-Lead LFCSP

| Pin No. | Mnemonic | Description |
| :--- | :--- | :--- |
| 1 | OUT A | Output Channel A. |
| 2 | -IN A | Inverting Input Channel A. |
| 3 | + IN A | Noninverting Input Channel A. |
| 4 | V- | Negative Supply Voltage. |
| 5 | +IN B | Noninverting Input Channel B. |
| 6 | -IN B | Inverting Input Channel B. |
| 7 | OUT B | Output Channel B. |
| 8 | V+ | Positive Supply Voltage. |
|  | EPAD | Exposed Pad for the 8-Lead LFCSP (CP Suffix). The exposed pad must be connected to V-. |



Figure 7. ADA4610-4 Pin Configuration, 14-Lead SOIC (R Suffix)


Figure 8. ADA4610-4 Pin Configuration, 16-Lead LFCSP (CP Suffix)

Table 9. ADA4610-4 Pin Function Descriptions, 14-Lead SOIC and 16-Lead LFCSP

| Pin No. |  |  |  |
| :--- | :--- | :--- | :--- |
| $\mathbf{1 4 - L e a d ~ S O I C ~}$ | $\mathbf{1 6}$-Lead LFCSP | Mnemonic | Description |
| 1 | 15 | OUT A | Output Channel A. |
| 2 | 1 | IN A | Inverting Input Channel A. |
| 3 | 2 | +IN A | Noninverting Input Channel A. |
| 4 | 3 | V+ | Positive Supply Voltage. |
| 5 | 4 | +IN B | Noninverting Input Channel B. |
| 6 | 5 | -IN B | Inverting Input Channel B. |
| 7 | 6 | OUT B | Output Channel B. |
| 8 | 7 | OUT C | Output Channel C. |
| 9 | 8 | -IN C | Inverting Input Channel C. |
| 10 | 9 | +IN C | Noninverting Input Channel C. |
| 11 | 10 | V- | Negative Supply Voltage. |
| 12 | 11 | +IN D | Noninverting Input Channel D. |
| 13 | 12 | IN D | Inverting Input Channel D. |
| 14 | 14 | OUT D | Output Channel D. |
| Not applicable | 13,16 | NIC | Not Internally Connected. |
| Not applicable |  | EPAD | Exposed Pad. The exposed pad must be connected to V-. |

## TYPICAL PERFORMANCE CHARACTERISTICS

$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.


Figure 9. Input Offset Voltage Distribution, $V_{s Y}= \pm 5 \mathrm{~V}$


Figure 10. Input Offset Voltage Drift (TCVos) Distribution, $V_{S Y}= \pm 5 \mathrm{~V}$


Figure 11. Input Offset Voltage vs. Common-Mode Input Voltage ( $V_{C M}$ ), $V_{S Y}= \pm 5 V, R_{L}=\infty$


Figure 12. Input Offset Voltage Distribution, $V_{S Y}= \pm 15 \mathrm{~V}$


Figure 13. TCV $o s$ Distribution, $V_{S Y}= \pm 15 \mathrm{~V}$


Figure 14. Input Offset Voltage vs. Input Common-Mode Voltage (VCM), $V_{S Y}= \pm 15 \mathrm{~V}, R_{L}=\infty$


Figure 15. Input Bias Current vs. Common-Mode Input Voltage (VCM), Mean and Three Standard Deviations, $V_{S Y}= \pm 5 V, R_{L}=\infty$


Figure 16. Input Bias Current vs. Common-Mode Input Voltage (VCM),
Three Temperatures, $V_{S Y}= \pm 5 \mathrm{~V}, R_{L}=\infty$


Figure 17. Input Bias Current vs. Temperature, $V_{S Y}= \pm 5 \mathrm{~V}$


Figure 18. Input Bias Current vs. Common-Mode Input Voltage (VCM), Mean and Three Standard Deviations, VSY $= \pm 15$ V, $R_{L}=\infty$


Figure 19. Input Bias Current vs. Common-Mode Input Voltage ( $V_{C M}$ ), Three Temperatures, $V_{S Y}= \pm 15 \mathrm{~V}, R_{L}=\infty$


Figure 20. Input Bias Current vs. Temperature, $V_{S Y}= \pm 15 \mathrm{~V}$


Figure 21. Dropout Voltage (V+ - Vout) vs. lout Source, $V_{s y}= \pm 5$ V


Figure 22. Dropout Voltage (Vout $-V-$ ) vs. Iout $\operatorname{Sink}, V_{S Y}= \pm 5 \mathrm{~V}$


Figure 23. Open-Loop Gain and Phase Margin vs. Frequency,
$V_{S Y}= \pm 5 \mathrm{~V}, R_{L}=2 \mathrm{k} \Omega, V_{I N}=5 \mathrm{mV}$


Figure 24. Dropout Voltage ( $V+-V_{\text {out }}$ ) vs. lout Source, $V_{S Y}= \pm 15 \mathrm{~V}$


Figure 25. Dropout Voltage $\left(V_{\text {out }}-V-\right)$ vs. Iout $\operatorname{Sink}, V_{S Y}= \pm 15 \mathrm{~V}$


Figure 26. Open-Loop Gain and Phase Margin vs. Frequency, $V_{S Y}= \pm 15 \mathrm{~V}, R_{L}=2 \mathrm{k} \Omega, V_{I N}=5 \mathrm{mV}$


Figure 27. Closed-Loop Gain vs. Frequency, $V_{S Y}= \pm 5 \mathrm{~V}$


Figure 28. Closed-Loop Output Impedance (Z $Z_{\text {OUT }}$ ) vs. Frequency, $V_{S Y}= \pm 5 \mathrm{~V}$


Figure 29. $P S R R$ vs. Frequency, $V_{S Y}= \pm 5 \mathrm{~V}$


Figure 30. Closed-Loop Gain vs. Frequency, $V_{S Y}= \pm 15 \mathrm{~V}$


Figure 31. Closed-Loop Output Impedance (Zout) vs. Frequency, $V_{S Y}= \pm 15 \mathrm{~V}$


Figure 32. PSRR vs. Frequency, $V_{s y}= \pm 15 \mathrm{~V}$


Figure 33. $C M R R$ vs. Frequency, $V_{S Y}= \pm 5 \mathrm{~V}$


Figure 34. Large Signal Transient Response, $V_{S Y}= \pm 5 \mathrm{~V}, A_{V}=1$,
$R_{L}=2 \mathrm{k} \Omega, C_{L}=100 \mathrm{pF}$


Figure 35. Small Signal Transient Response, $V_{S Y}= \pm 5 V, A v=1$, $R_{L}=2 \mathrm{k} \Omega, C_{L}=100 \mathrm{pF}$


Figure 36. CMRR vs. Frequency, $V_{s y}= \pm 15 \mathrm{~V}$


Figure 37. Large Signal Transient Response, $V_{S Y}= \pm 15 \mathrm{~V}, A_{V}=1$,
$R_{L}=2 \mathrm{k} \Omega, C_{L}=100 \mathrm{pF}$


Figure 38. Small Signal Transient Response, $V_{S Y}= \pm 15 V, A_{V}=1$, $R_{L}=2 \mathrm{k} \Omega, C_{L}=100 \mathrm{pF}$


Figure 39. Voltage Noise Density vs. Frequency, $V_{S Y}= \pm 5 \mathrm{~V}$


Figure 40. Overshoot vs. Load Capacitance, $V_{S Y}= \pm 5 V, A_{v}=1$, $R_{L}=2 \mathrm{k} \Omega, V_{I N}=100 \mathrm{mV} p-p$


Figure 41. Voltage Noise Density vs. Frequency, $V_{S Y}= \pm 15 \mathrm{~V}$


Figure 42. Overshoot vs. Load Capacitance, $V_{S Y}= \pm 15 \mathrm{~V}, A_{v}=1$, $R_{L}=2 \mathrm{k} \Omega, V_{I N}=100 \mathrm{mV}$-p

## COMPARATIVE VOLTAGE AND VARIABLE VOLTAGE GRAPHS



Figure 43. $T H D+N$ vs. Amplitude, $V_{S Y}= \pm 5 \mathrm{~V}$


Figure 44. $T H D+N$ vs. Frequency, $V_{S Y}= \pm 5 \mathrm{~V}$


Figure 45. Channel Separation vs. Frequency


Figure 46. $T H D+N$ vs. Amplitude, $V_{S Y}= \pm 15 \mathrm{~V}$


Figure 47. $T H D+N$ vs. Frequency, $V_{s Y}= \pm 15 \mathrm{~V}$


Figure 48. No Phase Reversal, $V_{s Y}= \pm 15 \mathrm{~V}, A_{v}=+1, R_{L}=2 \mathrm{k} \Omega, C_{L}=100 \mathrm{pF}$


Figure 49. Voltage Noise, 0.1 Hz to 10 Hz


Figure 50. Positive Step Settling Time


Figure 51. Positive Overload Recovery


Figure 52. Supply Current ( $I_{s y}$ ) per Amplifier vs. Supply Voltage ( $V_{s y}$ ) at Various Temperatures


Figure 53. Negative Step Settling Time


Figure 54. Negative Overload Recovery


Figure 55. Positive and Negative Slew Rate $\left(V_{S Y}= \pm 5 \mathrm{~V}, A_{v}=1, R_{L}=2 \mathrm{k} \Omega\right)$


Figure 56. Positive and Negative Slew Rate ( $\left.V_{s Y}= \pm 15 \mathrm{~V}, A_{v}=1, R_{L}=2 \mathrm{k} \Omega\right)$

## THEORY OF OPERATION

The ADA4610-1/ADA4610-2/ADA4610-4 are manufactured using the Analog Devices, Inc., $i$ Polar ${ }^{\oplus}$ process, a 36 V dielectrically isolated (DI) process with P-channel JFET technology. The unique architecture of the ADA4610-1/ADA4610-2/ADA4610-4 makes it possible to combine high precision and high speed characteristics into a high voltage, low power op amp. A simplified schematic for the ADA4610-1/ADA4610-2/ADA4610-4 is shown in Figure 57. The JFET input stage architecture offers advantages of low input bias current, high bandwidth, high gain, low noise, and no phase reversal when the applied input signal exceeds the common-mode voltage range. The output stage is rail-to-rail with high drive characteristics and low dropout voltage for both sinking and sourcing currents.

The ADA4610-1/ADA4610-2/ADA4610-4 are unconditionally stable for all gain configurations, even with capacitive loads well in excess of 1 nF . The devices have internal protective circuitry that allows voltages as high as 0.3 V beyond the supplies to be applied at the input of either terminal without causing damage (for higher input voltages, refer to the Input Overvoltage Protection section).

The ADA4610-1/ADA4610-2 B grades achieve less than 0.4 mV of offset and $2 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ of offset drift; these characteristics are usually associated with very high precision bipolar input amplifiers. The gate current of a typical JFET doubles every $10^{\circ} \mathrm{C}$, resulting in a similar increase in input bias current over temperature. The low power consumption characteristic of the ADA4610-1/ADA4610-2/ADA4610-4 minimizes the die temperature, which warrants low input bias currents even at elevated ambient temperatures, making the amplifiers ideal for applications that require low leakage specifications without active cooling. Ensure proper printed circuit board (PCB) layout to minimize leakage currents between PCB traces. Improper layout and board handling can generate leakage currents exceeding the bias currents of the operational amplifier.

The ADA4610-1/ADA4610-2/ADA4610-4 are fully specified with supply voltages from $\pm 5 \mathrm{~V}$ to $\pm 15 \mathrm{~V}$ over the extended industrial temperature range of $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$. The ADA4610-1 is available in an 8 -lead SOIC. The ADA4610-2 is available in an 8 -lead MSOP, an 8-lead SOIC, and an 8-lead LFCSP. The ADA4610-4 is available in a 14 -lead SOIC and a 16 -lead LFCSP. All these packages are surface-mount type.


Figure 57. Simplified Schematic

## APPLICATIONS INFORMATION

## INPUT OVERVOLTAGE PROTECTION

The ADA4610-1/ADA4610-2/ADA4610-4 have internal protective circuitry that allows voltages as high as 0.3 V beyond the supplies to be applied at the input of either terminal without causing damage. For higher input voltages, a series resistor is necessary to limit the input current. Determine the resistor value by

$$
\frac{V_{I N}-V_{S}}{R_{S}} \leq 10 \mathrm{~mA}
$$

where:
$V_{I N}$ is the input voltage.
$V_{S}$ is the voltage of either $\mathrm{V}+$ or $\mathrm{V}-$.
$R_{S}$ is the series resistor.
With a very low bias current of $<1.5 \mathrm{nA}$ up to $125^{\circ} \mathrm{C}$, higher resistor values can be used in series with the inputs. A $5 \mathrm{k} \Omega$ resistor protects the inputs from voltages as high as 25 V beyond the supplies and adds less than $10 \mu \mathrm{~V}$ to the offset.

## PEAK DETECTOR

The function of a peak detector is to capture the peak value of a signal and produce an output equal to it. By taking advantage of the dc precision and super low input bias current of the JFET input amplifiers, such as the ADA4610-1/ADA4610-2/ADA4610-4, a highly accurate peak detector can be built, as shown in Figure 58.


Figure 58. Positive Peak Detector
In this application, Diode D3 and Diode D4 act as unidirectional current switches that open up when the output is kept constant (in hold mode). To detect a positive peak, U2A drives C3 through D3 and D4 until C3 is charged to a voltage equal to the input peak value. Feedback from the output of the U2B + peak through R6 limits the output voltage of U2A. After detecting the peak, the output of U2A swings low but is clamped by D2. Diode D3 reverses bias and the common node of D3, D4, and R7 is held to a voltage equal to + peak by R7. The voltage across D 4 is 0 V ; therefore, its leakage is small. The bias current of U2B is also small. With almost no leakage, C3 has a long hold time.

The ADA4610-1/ADA4610-2/ADA4610-4, shown in Figure 58, are ideal for building a peak detector because U 2 A requires dc precision and high output current during fast peaks, and U2B requires low input bias current $\left(\mathrm{I}_{\mathrm{B}}\right)$ to minimize capacitance discharge between peaks. A low leakage and low dielectric absorption capacitor, such as polystyrene or polypropylene, is required for C 3 . Reversing the diode directions causes the circuit to detect negative peaks.

## CURRENT TO VOLTAGE (I TO V) CONVERSION APPLICATIONS

## Photodiode Circuits

Common applications for I to V conversion include photodiode circuits where the amplifier converts a current emitted by a diode placed at the negative input terminal into an output voltage.
The low input bias current, wide bandwidth, and low noise of the ADA4610-1/ADA4610-2/ADA4610-4 make them excellent choices for various photodiode applications, including fax machines, fiber optic controls, motion sensors, and barcode readers.

The circuit shown in Figure 59 uses a silicon diode with zero bias voltage. This setup is a photovoltaic mode, which uses many large photodiodes. This configuration limits the overall noise and is suitable for instrumentation applications.


Figure 59. Equivalent Preamplifier Photodiode Circuit
A larger signal bandwidth can be attained at the expense of additional output noise. The total input capacitance ( $\mathrm{C}_{\mathrm{T}}$ ) consists of the sum of the diode capacitance (typically 30 pF to 40 pF ) and the amplifier input capacitance ( $<10 \mathrm{pF}$ ), which includes external parasitic capacitance. $\mathrm{C}_{\mathrm{T}}$ creates a zero in the frequency response that can lead to an unstable system. To ensure stability and optimize the bandwidth of the signal, place a capacitor in the feedback loop of the circuit shown in Figure 59. The capacitor creates a pole and yields a bandwidth with a corner frequency of

$$
1 /\left(2 \pi\left(R_{F} C_{F}\right)\right)
$$

where:
$R_{F}$ is the feedback resistor.
$C_{F}$ is the feedback capacitor

## ADA4610-1/ADA4610-2/ADA4610-4

Determine the $\mathrm{R}_{\mathrm{F}}$ value by the following ratio:

## $V / I_{D}$

where:
$V$ is the desired output voltage of the op amp.
$I_{D}$ is the diode current.
For example, if $\mathrm{I}_{\mathrm{D}}$ is $100 \mu \mathrm{~A}$ and a 10 V output voltage is needed, $\mathrm{R}_{\mathrm{F}}$ must be $100 \mathrm{k} \Omega$. The resistance of the photodiode $\left(R_{D}\right)$ is a junction resistance (see Figure 59).

A typical value for $R_{D}$ is $1000 \mathrm{M} \Omega$. Because $\mathrm{R}_{\mathrm{D}} \gg \mathrm{R}_{\mathrm{F}}$, the circuit behavior is not impacted by the effect of the junction resistance. The maximum signal bandwidth ( $\mathrm{f}_{\mathrm{MAX}}$ ) is

$$
f_{M A X}=\sqrt{\frac{f t}{2 \pi R_{F} C_{T}}}
$$

where $f t$ is the unity-gain frequency of the op amp.

## Calculate $\mathrm{C}_{\mathrm{F}}$ by

$$
C_{F}=\sqrt{\frac{C_{T}}{2 \pi R_{F} f t}}
$$

where $f t$ is the unity-gain frequency of the op amp, and achieves a phase margin, $\varphi_{M}$, of approximately $45^{\circ}$.

Increase the $C_{F}$ value to obtain a higher phase margin. Setting $C_{F}$ to twice the previous value yields approximately $\varphi_{M}=65^{\circ}$ and a maximal flat frequency response, but it reduces the maximum signal bandwidth by $50 \%$.
Using the previous parameters with a $\mathrm{C}_{\mathrm{F}} \approx 7 \mathrm{pF}$, the signal bandwidth is approximately 250 kHz .

## COMPARATOR OPERATION

Although op amps are quite different from comparators, occasionally an unused section of a dual or a quad op amp can be used as a comparator; however, this is not recommended for rail-to-rail output op amps. For rail-to-rail output op amps, the output stage is generally a ratioed current mirror with bipolar or MOSFET transistors. With the device operating in open-loop mode, the second stage increases the current drive to the ratioed mirror to close the loop. However, the second stage cannot close the loop, which results in an increase in supply current. With the ADA4610-1/ADA4610-2/ADA4610-4 op amps configured as comparators, the supply current can be significantly higher (see Figure 60 for the supply current vs. the supply voltage for the ADA4610-4). Configuring an unused section as a voltage follower with the noninverting input connected to a voltage within the input voltage range is recommended. The ADA4610-1/ADA4610-2/ ADA4610-4 have a unique output stage design that reduces the excess supply current but does not entirely eliminate this effect when the op amp is operating in open-loop mode.


Figure 60. Supply Current ( $l_{\text {sy }}$ ) vs. Supply Voltage $\left(V_{s y}\right)$ for the ADA4610-4 Only

## LONG-TERM DRIFT

The stability of a precision signal path over its lifetime or between calibration procedures is dependent on the long-term stability of the analog components in the path, such as op amps, references, and data converters. To help system designers predict the long-term drift of circuits that use the ADA4610-1/ ADA4610-2/ADA4610-4, Analog Devices measured the offset voltage of multiple units for 10,000 hours (more than 13 months) using a high precision measurement system, including an ultrastable oil bath. To replicate real-world system performance, the devices under test (DUTs) were soldered onto an FR4 PCB using a standard reflow profile (as defined in the JEDEC J-STD020D standard), as opposed to testing them in sockets. This manner of testing is important because expansion and contraction of the PCB can apply stress to the integrated circuit (IC) package and contribute to shifts in the offset voltage.
The ADA4610-1/ADA4610-2/ADA4610-4 have extremely low long-term drift, as shown in Figure 61. The red, blue, and green traces show sample units. Note that the ADA4610-1/ADA4610-2/ ADA4610-4 (B-grade) have a mean drift over 10,000 hours of approximately $5 \mu \mathrm{~V}$, or less than $2 \%$ of their maximum specified offset voltage of $400 \mu \mathrm{~V}$ at room temperature.


Figure 61. Measured Long-Term Drift of the ADA4610-1/ADA4610-2/ ADA4610-4 Offset Voltage over 10,000 Hours

## TEMPERATURE HYSTERESIS

In addition to stability over time as described in the Long-Term Drift section, it is useful to know the temperature hysteresis, that is, the stability vs. cycling of temperature. Hysteresis is an important parameter because it tells the system designer how closely the signal returns to its starting amplitude after the ambient temperature changes and subsequent return to room temperature. Figure 62 shows the change in input offset voltage as the temperature cycles three times from room temperature to $+125^{\circ} \mathrm{C}$ to $-40^{\circ} \mathrm{C}$ and back to room temperature. The dotted line is an initial preconditioning cycle to eliminate the original temperature-induced offset shift from exposure to production solder reflow temperatures. In the three full cycles, the offset hysteresis is typically only $8 \mu \mathrm{~V}$, or $1 \%$ of its $800 \mu \mathrm{~V}$ maximum offset voltage over the full operating temperature range. The histogram in Figure 63 shows that the hysteresis is larger when the device is cycled through only a half cycle, from room temperature to $125^{\circ} \mathrm{C}$ and back to room temperature.


Figure 62. Change in Offset Voltage over Three Full Temperature Cycles


Figure 63. Histogram Showing the Temperature Hysteresis of the Offset Voltage over Three Full Cycles and over Three Half Cycles

## OUTLINE DIMENSIONS



COMPLIANT TO JEDEC STANDARDS MS-012-AA
CONTROLLING DIMENSIONS ARE IN MILLIMETERS; INCH DIMENSIONS (IN PARENTHESES) ARE ROUNDED-OFF MILLIMETER EQUIVALENTS FOR REFERENCE ONLY AND ARE NOT APPROPRIATE FOR USE IN DESIGN.

Figure 64. 8-Lead Standard Small Outline Package [SOIC_N] Narrow Body
( $R-8$ )
Dimensions shown in millimeters and (inches)


Figure 65. 8-Lead Mini Small Outline Package [MSOP]
(RM-8)
Dimensions shown in millimeters


Figure 66. 5-Lead Small Outline Transistor Package [SOT-23] (RJ-5)
Dimensions shown in millimeters


Figure 67. 8-Lead Lead Frame Chip Scale Package [LFCSP]
$3 \mathrm{~mm} \times 3 \mathrm{~mm}$ Body and 0.75 mm Package Height (CP-8-11)
Dimensions shown in millimeters


COMPLIANT TO JEDEC STANDARDS MS-012-AB CONTROLLING DIMENSIONS ARE IN MILLIMETERS; INCH DIMENSIONS (IN PARENTHESES) ARE ROUNDED-OFF MILLIMETER EQUIVALENTS FOR REFERENCE ONLY AND ARE NOT APPROPRIATE FOR USE IN DESIGN.

Figure 68. 14-Lead Standard Small Outline Package [SOIC_N]
Narrow Body
(R-14)
Dimensions shown in millimeters and (inches)


COMPLIANT TO JEDEC STANDARDS MO-220-WGGC.
Figure 69. 16-Lead Lead Frame Chip Scale Package [LFCSP]
$4 \mathrm{~mm} \times 4 \mathrm{~mm}$ Body and 0.75 mm Package Height (CP-16-23)
Dimensions shown in millimeters

## ORDERING GUIDE

| Model ${ }^{1}$ | Temperature Range | Package Description | Package Option | Marking Code |
| :---: | :---: | :---: | :---: | :---: |
| ADA4610-1ARZ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead Standard Small Outline Package [SOIC_N] | R-8 |  |
| ADA4610-1ARZ-R7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead Standard Small Outline Package [SOIC_N] | R-8 |  |
| ADA4610-1ARZ-RL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead Standard Small Outline Package [SOIC_N] | R-8 |  |
| ADA4610-1BRZ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead Standard Small Outline Package [SOIC_N] | R-8 |  |
| ADA4610-1BRZ-R7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead Standard Small Outline Package [SOIC_N] | R-8 |  |
| ADA4610-1BRZ-RL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead Standard Small Outline Package [SOIC_N] | R-8 |  |
| ADA4610-1ARJZ-R2 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 5-Lead Small Outline Transistor Package [SOT-23] | RJ-5 | A37 |
| ADA4610-1ARJZ-R7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 5-Lead Small Outline Transistor Package [SOT-23] | RJ-5 | A37 |
| ADA4610-1ARJZ-RL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 5-Lead Small Outline Transistor Package [SOT-23] | RJ-5 | A37 |
| ADA4610-2ACPZ-R7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead Lead Frame Chip Scale Package [LFCSP] | CP-8-11 | A2U |
| ADA4610-2ACPZ-RL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead Lead Frame Chip Scale Package [LFCSP] | CP-8-11 | A2U |
| ADA4610-2ARMZ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead Mini Small Outline Package [MSOP] | RM-8 | A2U |
| ADA4610-2ARMZ-R7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead Mini Small Outline Package [MSOP] | RM-8 | A2U |
| ADA4610-2ARMZ-RL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead Mini Small Outline Package [MSOP] | RM-8 | A2U |
| ADA4610-2ARZ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead Standard Small Outline Package [SOIC_N] | R-8 |  |
| ADA4610-2ARZ-R7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead Standard Small Outline Package [SOIC_N] | R-8 |  |
| ADA4610-2ARZ-RL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead Standard Small Outline Package [SOIC_N] | R-8 |  |
| ADA4610-2BRZ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead Standard Small Outline Package [SOIC_N] | R-8 |  |
| ADA4610-2BRZ-R7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead Standard Small Outline Package [SOIC_N] | R-8 |  |
| ADA4610-2BRZ-RL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead Standard Small Outline Package [SOIC_N] | R-8 |  |
| ADA4610-4ARZ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 14-Lead Standard Small Outline Package [SOIC_N] | R-14 |  |
| ADA4610-4ARZ-R7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 14-Lead Standard Small Outline Package [SOIC_N] | R-14 |  |
| ADA4610-4ARZ-RL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 14-Lead Standard Small Outline Package [SOIC_N] | R-14 |  |
| ADA4610-4ACPZ-R7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 16-Lead Lead Frame Chip Scale Package [LFCSP] | CP-16-23 |  |
| ADA4610-4ACPZ-RL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 16-Lead Lead Frame Chip Scale Package [LFCSP] | CP-16-23 |  |


[^0]:    ${ }^{1}$ Guaranteed by design and characterization.

