# Dual 1A, 1.25MHz Synchronous Step-Down Converter

### **General Description**

The RT8075 is a high efficiency Pulse-Width-Modulated (PWM) dual step-down DC/DC converter. Capable of delivering up to 1A output current over a wide input voltage range from 2.5V to 5.5V, the RT8075 is ideally suited for portable electronic devices that are powered from 1-cell Li-ion battery or from other power sources such as cellular phones, PDAs, PC WLAN card and hand-held devices.

Three operating modes are available including : PWM mode, Low Dropout Mode and shut-down mode. The Internal synchronous rectifier with low R<sub>DS(ON)</sub> dramatically reduces conduction loss at PWM mode. No external Schottky diode is required in practical application. The RT8075 enters Low Dropout mode when normal PWM cannot provide regulated output voltage by continuously turning on the upper P-MOSFET. The RT8075 enters shutdown mode and consumes less than 0.1µA when the EN pin is pulled low.

The switching ripple is easily smoothed-out by small package filtering elements due to the fixed operating frequency of 1.25MHz. The RT8075 is available in the WDFN-10L 3x3 package.

## **Pin Configurations**

(TOP VIEW)

EN1 11 FB1 22 VIN2 23 GND 41 LX2 51 UID LX1 GND 41 LX2 M S UID LX1 S GND VIN S UID LX1 S GND VIN S UID LX1 S GND VIN S UID LX1 S GND VIN S UID LX1 S UID LX1 S GND VIN S UID LX1 S UID LX1
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WDFN-10L 3x3

## **Marking Information**

**RT8075GQW** 

38=YM DNN

38= : Product Code YMDNN : Date Code

### Features

- 2.5V to 5.5V Input Range
- 1A Output Current
- 1.25MHz Fixed Frequency PWM Operation
- 95% Efficiency
- No Schottky Diode Required
- 0.6V Reference Allows Low Output Voltage
- Low Dropout Operation : 100% Duty Cycle
- Small 10-Lead WDFN Package
- RoHS Compliant and Halogen Free

### Applications

- Portable Instruments
- Microprocessors and DSP Core Supplies
- Cellular Phones
- Wireless and DSL Modems
- PC Cards

# **Ordering Information**

### RT8075

#### Package Type QW: WDFN-10L 3x3 (W-Type)

Lead Plating System

- G : Green (Halogen Free and Pb Free)
- Z: ECO (Ecological Element with Halogen Free and Pb free)

Note :

Richtek products are :

- RoHS compliant and compatible with the current requirements of IPC/JEDEC J-STD-020.
- Suitable for use in SnPb or Pb-free soldering processes.

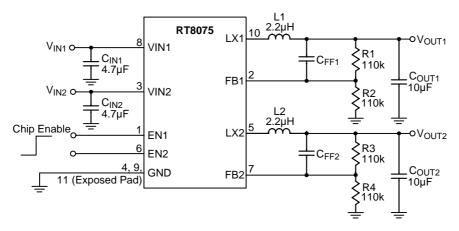
#### **RT8075ZQW**



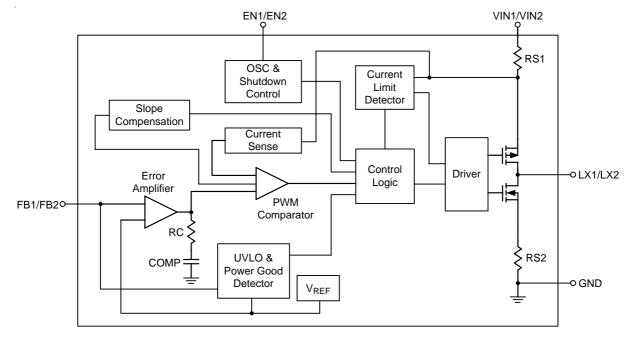
38 : Product Code YMDNN : Date Code



# **Typical Application Circuit**



# **Function Block Diagram**



# **Functional Pin Description**

Pin No.	Pin Name	Pin Function		
1	EN1	Chip Enable of Channel 1 (Active High).		
2	FB1	Feedback Input of Channel 1.		
3	VIN2	Power Supply Input of Channel 2.		
5	LX2	Switching Node of Channel 2.		
6	EN2	Chip Enable of Channel 2 (Active High).		
7	FB2	Feedback Input of Channel 2.		
8	VIN1	Power Supply Input of Channel 1.		
10	LX1	Switching Node of Channel 1.		
4, 9, 11 (Exposed Pad)	d Pad) GND Ground. The exposed pad must be soldered to a large PCB and connected to GND for maximum power dissipation.			

# Absolute Maximum Ratings (Note 1)

Supply Input Voltage VIN1, VIN2	–0.3V to 6.5V
• LX1, LX2 Pin Voltage	0.3V to (V <sub>IN</sub> + 0.3V)
Other Pins Voltage	–0.3V to 6.5V
• Power Dissipation, $P_D @ T_A = 25^{\circ}C$	
WDFN-10L 3x3	1.471W
Package Thermal Resistance (Note 2)	
WDFN-10L 3x3, θ <sub>JA</sub>	68°C/W
WDFN-10L 3x3, 0JC	7.8°C/W
• Lead Temperature (Soldering, 10 sec.)	260°C
Junction Temperature	150°C
Storage Temperature Range	–65°C to 150°C
ESD Susceptibility (Note 3)	
HBM (Human Body Mode)	2kV
MM (Machine Mode)	200V

# Recommended Operating Conditions (Note 4)

Supply Input Voltage 2.5V to 5.5	šν
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### **Electrical Characteristics**

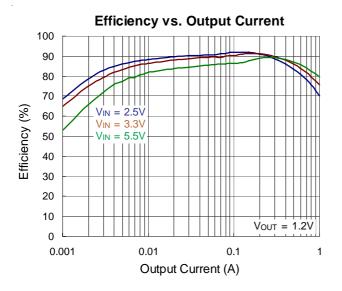
 $(V_{IN} = 3.6V, T_A = 25^{\circ}C$  unless otherwise specified)

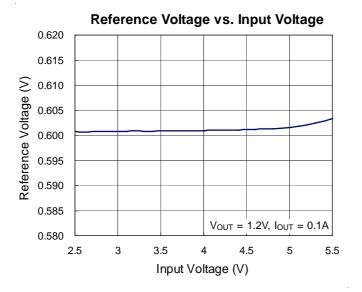
Parameter	Symbol	Test Conditions	Min	Тур	Max	Unit	
Input Voltage Range	V <sub>IN</sub>		2.5		5.5	V	
Reference Voltage	V <sub>REF</sub>		0.588	0.6	0.612	V	
Quiescent Current	lq	$I_{OUT} = 0$ mA, $V_{FB} = V_{REF} + 5\%$		70		μΑ	
Shutdown Current	I <sub>SHDN</sub>			0.1	1	μA	
Under Voltage		V <sub>IN</sub> Rising		2.1		V	
Lockout Threshold	UVLO	Hysteresis		0.18			
Oscillator Frequency	f <sub>OSC</sub>	V <sub>IN</sub> = 3.6V, I <sub>OUT</sub> = 300mA	1	1.25	1.5	MHz	
EN1 High-Level Input Voltage	V <sub>EN_H</sub>	V <sub>IN</sub> = 2.5V to 5.5V	1.5		V <sub>IN</sub>	V	
EN1 Low-Level Input Voltage	V <sub>EN_L</sub>	V <sub>IN</sub> = 2.5V to 5.5V			0.4	V	
Thermal Shutdown Temperature	T <sub>SD</sub>			160		°C	
Peak Current Limit	I <sub>LIM</sub>	V <sub>IN</sub> = 2.5V to 5.5 V	1.2	1.5	2.1	А	
Switch On Resistance, High	R <sub>DS(ON)_P</sub>	I <sub>OUT</sub> = 200mA, V <sub>IN</sub> = 3.6V		0.25		Ω	
Switch On Resistance, Low	R <sub>DS(ON)_N</sub>	I <sub>OUT</sub> = 200mA, V <sub>IN</sub> = 3.6V		0.26		Ω	
Output Line Regulation		V <sub>IN</sub> = 2.5V to 5.5V (Note 5)		0.04	0.4	%/V	
Output Load Regulation		50mA < I <sub>LOAD</sub> < 1A (Note 5)		0.5		%	

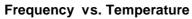
# **RT8075**

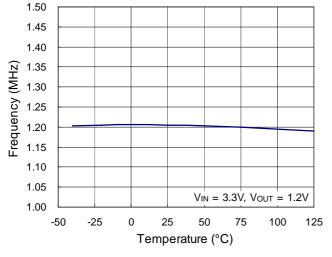
- **Note 1.** Stresses listed as the above "Absolute Maximum Ratings" may cause permanent damage to the device. These are for stress ratings. Functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may remain possibility to affect device reliability.
- Note 2.  $\theta_{JA}$  is measured in the natural convection at  $T_A = 25^{\circ}C$  on a high effective thermal conductivity four-layer test board of JEDEC 51-7 thermal measurement standard. The case point of  $\theta_{JC}$  is on the exposed pad of the package.
- Note 3. Devices are ESD sensitive. Handling precaution is recommended.
- Note 4. The device is not guaranteed to function outside its operating conditions.
- Note 5. Guarantee by design.

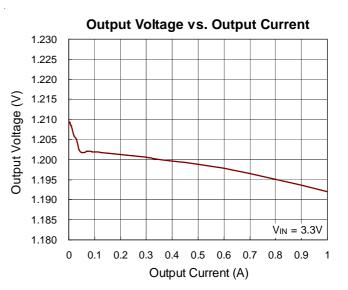
# **Typical Operating Characteristics**



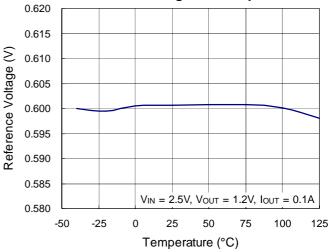




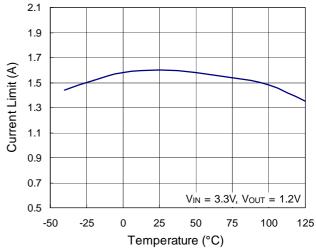




**Reference Voltage vs. Temperature** 

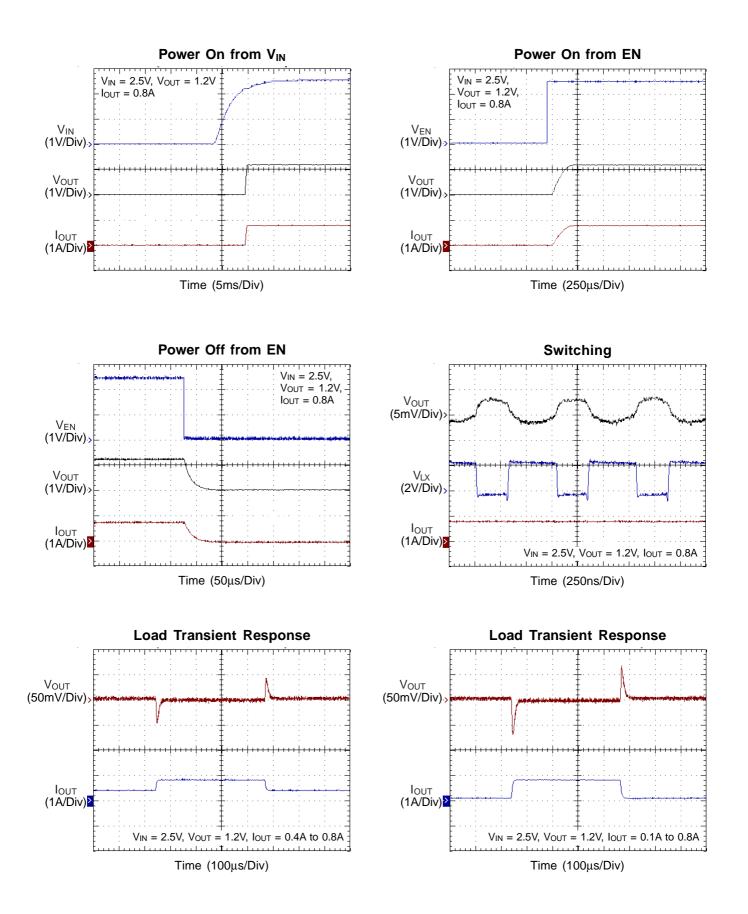


**Current Limit vs. Temperature** 



# **RT8075**





### **Applications Information**

The basic RT8075 application circuit is shown in Typical Application Circuit. External component selection is determined by the maximum load current and begins with the selection of the inductor value and operating frequency followed by  $C_{\text{IN}}$  and  $C_{\text{OUT}}$ .

#### **Inductor Selection**

For a given input and output voltage, the inductor value and operating frequency determine the ripple current. The ripple current  $\Delta I_L$  increases with higher  $V_{IN}$  and decreases with higher inductance.

$$\Delta I_{L} = \left[\frac{V_{OUT}}{f x L}\right] x \left[1 - \frac{V_{OUT}}{V_{IN}}\right]$$

Having a lower ripple current reduces the ESR losses in the output capacitors and the output voltage ripple. Highest efficiency operation is achieved at low frequency with small ripple current. This, however, requires a large inductor.

A reasonable starting point for selecting the ripple current is  $\Delta I_L = 0.4(I_{MAX})$ . The largest ripple current occurs at the highest V<sub>IN</sub>. To guarantee that the ripple current stays below a specified maximum, the inductor value should be chosen according to the following equation :

### **Inductor Core Selection**

Once the value for L is known, the type of inductor must be selected. High efficiency converters generally cannot afford the core loss found in low cost powdered iron cores, forcing the use of more expensive ferrite or mollypermalloy cores. Actual core loss is independent of core size for a fixed inductor value but it is very dependent on the inductance selected. As the inductance increases, core losses decrease. Unfortunately, increased inductance requires more turns of wire and therefore copper losses will increase.

Ferrite designs have very low core losses and are preferred at high switching frequencies, so design goals can concentrate on copper loss and preventing saturation. Ferrite core material saturates "hard", which means that inductance collapses abruptly when the peak design current is exceeded. This results in an abrupt increase in inductor ripple current and consequent output voltage ripple. Do not allow the core to saturate!

Different core materials and shapes will change the size/ current and price/current relationship of an inductor.

Toroid or shielded pot cores in ferrite or permalloy materials are small and don't radiate energy but generally cost more than powdered iron core inductors with similar characteristics. The choice of which style inductor to use mainly depends on the price vs size requirements and any radiated field/EMI requirements.

### CIN and COUT Selection

The input capacitance,  $C_{IN}$ , is needed to filter the trapezoidal current at the source of the top MOSFET. To prevent large ripple voltage, a low ESR input capacitor sized for the maximum RMS current should be used. RMS current is given by :

$$I_{RMS} = I_{OUT(MAX)} \frac{V_{OUT}}{V_{IN}} \sqrt{\frac{V_{IN}}{V_{OUT}}} - 1$$

This formula has a maximum at  $V_{IN} = 2V_{OUT}$ , where  $I_{RMS} = I_{OUT}/2$ . This simple worst-case condition is commonly used for design because even significant deviations do not offer much relief. Note that ripple current ratings from capacitor manufacturers are often based on only 2000 hours of life which makes it advisable to further derate the capacitor, or choose a capacitor rated at a higher temperature than required. Several capacitors may also be paralleled to meet size or height requirements in the design.

The selection of  $C_{OUT}$  is determined by the Effective Series Resistance (ESR) that is required to minimize voltage ripple and load step transients, as well as the amount of bulk capacitance that is necessary to ensure that the control loop is stable. Loop stability can be checked by viewing the load transient response as described in a later section. The output ripple,  $\Delta V_{OUT}$ , is determined by :

$$\Delta V_{OUT} \leq \Delta I_{L} \left[ \text{ESR} + \frac{1}{8 f C_{OUT}} \right]$$

# **RT8075**

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The output ripple is highest at maximum input voltage since  $\Delta I_{L}$  increases with input voltage. Multiple capacitors placed in parallel may be needed to meet the ESR and RMS current handling requirements. Dry tantalum, special polymer, aluminum electrolytic and ceramic capacitors are all available in surface mount packages. Special polymer capacitors offer very low ESR but have lower capacitance density than other types. Tantalum capacitors have the highest capacitance density but it is important to only use types that have been surge tested for use in switching power supplies. Aluminum electrolytic capacitors have significantly higher ESR but can be used in cost-sensitive applications provided that consideration is given to ripple current ratings and long term reliability. Ceramic capacitors have excellent low ESR characteristics but can have a high voltage coefficient and audible piezoelectric effects. The high Q of ceramic capacitors with trace inductance can also lead to significant ringing.

#### **Using Ceramic Input and Output Capacitors**

Higher values, lower cost ceramic capacitors are now becoming available in smaller case sizes. Their high ripple current, high voltage rating and low ESR make them ideal for switching regulator applications. However, care must be taken when these capacitors are used at the input and output. When a ceramic capacitor is used at the input and the power is supplied by a wall adapter through long wires, a load step at the output can induce ringing at the input,  $V_{IN}$ . At best, this ringing can couple to the output and be mistaken as loop instability. At worst, a sudden inrush of current through the long wires can potentially cause a voltage spike at  $V_{IN}$  large enough to damage the part.

### Output Voltage Setting

The resistive divider allows the FB pin to sense a fraction of the output voltage as shown in Figure 1.

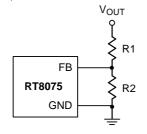


Figure 1. Setting Output Voltage

$$V_{OUT} = V_{REF} \left( 1 + \frac{R1}{R2} \right)$$

where  $V_{REF}$  is the internal reference voltage (0.6V typ.)

#### **Checking Transient Response**

The regulator loop response can be checked by looking at the load transient response. Switching regulators take several cycles to respond to a step in load current. When a load step occurs, V<sub>OUT</sub> immediately shifts by an amount equal to  $\Delta I_{LOAD}$  (ESR), where ESR is the effective series resistance of C<sub>OUT</sub>.  $\Delta I_{LOAD}$  also begins to charge or discharge C<sub>OUT</sub> generating a feedback error signal used by the regulator to return V<sub>OUT</sub> to its steady-state value. During this recovery time, V<sub>OUT</sub> can be monitored for overshoot or ringing that would indicate a stability problem.

#### **Thermal Considerations**

For continuous operation, do not exceed absolute maximum operation junction temperature. The maximum power dissipation depends on the thermal resistance of IC package, PCB layout, the rate of surroundings airflow and temperature difference between junction to ambient. The maximum power dissipation can be calculated by following formula :

 $\mathsf{P}_{\mathsf{D}(\mathsf{MAX})} = \left(\mathsf{T}_{\mathsf{J}(\mathsf{MAX})} - \mathsf{T}_{\mathsf{A}}\right) / \, \theta_{\mathsf{JA}}$ 

Where  $T_{J(MAX)}$  is the maximum operation junction temperature,  $T_A$  is the ambient temperature and the  $\theta_{JA}$  is the junction to ambient thermal resistance.

For recommended operating conditions specification of the RT8075, The maximum junction temperature is 125°C. The junction to ambient thermal resistance  $\theta_{JA}$  is layout dependent. For WDFN-10L 3x3 package, the thermal resistance  $\theta_{JA}$  is 68°C/W on the standard JEDEC 51-7 four layers thermal test board. The maximum power dissipation at  $T_A = 25$ °C can be calculated by following formula :

 $P_{D(MAX)}$  = (125°C - 25°C) / (68°C/W) = 1.471W for WDFN-10L 3x3

The maximum power dissipation depends on operating ambient temperature for fixed  $T_{J(MAX)}$  and thermal resistance  $\theta_{JA}$ . For RT8075 package, the Figure 2 of derating curve allows the designer to see the effect of rising ambient temperature on the maximum power dissipation allowed.

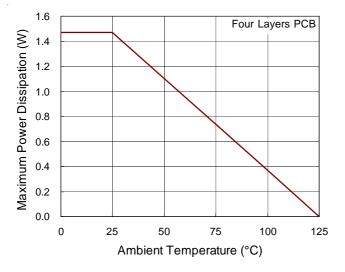
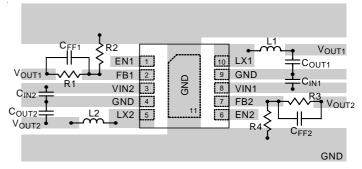


Figure 2. Derating Curves for RT8075 Package

### Layout Considerations

Follow the PCB layout guidelines for optimal performance of RT8075.

- Keep the trace of the main current paths as short and wide as possible.
- Put the input capacitor as close as possible to the device pins (VIN1 / VIN2 and GND).
- LX 1 / LX 2 node is with high frequency voltage swing and should be kept at small area. Keep analog components away from the LX 1 / LX 2 node to prevent stray capacitive noise pick-up.
- Place the feedback components as close as possible to the FB1 / FB2 pins.
- The GND and Exposed Pad must be connected to a strong ground plane for heat sinking and noise protection.





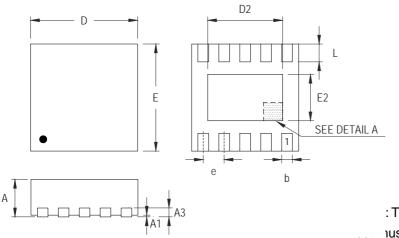
### Table 1. Recommended Inductors

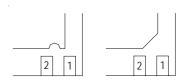
Supplier	Inductance (mH)	Dimensions (mm)	Series	
TAIYO YUDEN	2.2	3.00 x 3.00 x 1.50	NR 3015	
GOTREND	2.2	3.85 x 3.85 x 1.80	GTSD32	
Sumida	2.2	4.50 x 3.20 x 1.55	CDRH2D14	
Sumida	4.7	4.50 x 3.20 x 1.55	CDRH2D14	
TAIYO YUDEN	4.7	3.00 x 3.00 x 1.50	NR 3015	
GOTREND	4.7	3.85 x 3.85 x 1.80	GTSD32	

### Table 2. Recommended Capacitors for $C_{\text{IN}}$ and $C_{\text{OUT}}$

Supplier	Capacitance (mF)	Package	Part Number
TDK	4.7	0603	C1608JB0J475M
MURATA	4.7	0603	GRM188R60J475KE19
TAIYO YUDEN	4.7	0603	JMK107BJ475RA
TAIYO YUDEN	10	0603	JMK107BJ106MA
TDK	10	0805	C2012JB0J106M
MURATA	10	0805	GRM219R60J106ME19
MURATA	10	0805	GRM219R60J106KE19
TAIYO YUDEN	10	0805	JMK212BJ106RD

### **Outline Dimension**





DETAIL A Pin #1 ID and Tie Bar Mark Options

: The configuration of the Pin #1 identifier is optional, nust be located within the zone indicated.

Cumb al	Dimensions	In Millimeters	Dimensions In Inches		
Symbol	Min	Max	Min	Max	
А	0.700	0.800	0.028	0.031	
A1	0.000	0.050	0.000	0.002	
A3	0.175	0.250	0.007	0.010	
b	0.180	0.300	0.007	0.012	
D	2.950	3.050	0.116	0.120	
D2	2.300	2.650	0.091	0.104	
Е	2.950	3.050	0.116	0.120	
E2	1.500	1.750	0.059	0.069	
е	0.500		0.020		
L	0.350	0.450	0.014	0.018	

W-Type 10L DFN 3x3 Package

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