## Step-up DCIDC Converter with Shutdown Function

No. EA-284-180511

## OUTLINE

The R1204x is a low supply current PWM step-up DC/DC converter. Internally, a single IC consists of an NMOS FET, an oscillator, a PWM comparator, a voltage reference unit, an error amplifier, a current limit circuit, an under voltage lockout circuit (UVLO), an over-voltage protection circuit (OVP), a soft-start circuit, a maximum duty cycle limit circuit, and a thermal shutdown protection circuit. By simply using an inductor, a resistor, capacitors and a diode as external components, a high-efficiency step-up DC/DC converter can be easily configured. As protection functions, the IC contains a thermal shutdown protection circuit, a current limit circuit, an OVP circuit, and an UVLO circuit. A thermal shutdown circuit detects overheating of the ICs and stops the operation to protect it from damage. A current limit circuit limits the peak current of Lx, and an OVP circuit detects the over voltage of output, and an UVLO circuit detects the low input voltage.
The R1204x provides the R1204xxxA/D/G/H versions, which are optimized for serial driving of white LEDs with constant current, and the R1204xxxB/C/E/F versions, which are optimized for constant voltage driving. Among the R1204xxxB/C/E/F versions, only the R1204xxxC/F versions are equipped with PWM/VFM auto-switching controls. The LED current can be determined by the value of current setting resistor. The brightness of the LEDs can be quickly adjusted by applying a PWM signal ( 200 Hz to 300 kHz ) to the CE pin. The R1204x is available in DFN(PLP)1820-6 and TSOT-23-6 packages.

## FEATURES

- Input Voltage Range.........................................2.3 V to 5.5 V
- Supply Current .................................................Typ. $800 \mu \mathrm{~A}$
- Standby Current Max. $5 \mu \mathrm{~A}$
- Feedback Voltage ........................................... $0.2 \mathrm{~V} \pm 10 \mathrm{mV}$ (R1204xxxxA/D) $0.4 \mathrm{~V} \pm 10 \mathrm{mV}(\mathrm{R} 1204 \mathrm{xxxxG} / \mathrm{H})$
- $\quad \mathrm{V} \pm 15 \mathrm{mV}$ (R1204xxxxB/C/E/F)
- Lx Current Limit Function..................................Min. 700 mA
- Over Voltage Protection ................................... $23 \mathrm{~V}, 33 \mathrm{~V}, 42 \mathrm{~V}( \pm 1.5 \mathrm{~V})$
- Oscillator Frequency ........................................Typ. 1.0 MHz (R1204xxxxA/B/C/G)

Typ. 750 kHz (R1204xxxxD/E/F/H)

- Maximum Duty Cycle ........................................Min. 91\% (R1204xxxxA/B/C/G)

Min. 92\% (R1204xxxxD/E/F/H)

- FET ON Resistance ..........................................Typ. $0.8 \Omega$
- UVLO Function
- Thermal Protection Function
- LED Dimming Control for R1204xxxxA/D ..........by external PWM signal ( 200 Hz to 300 kHz frequency)
- Packages ..........................................................DFN(PLP)1820-6, TSOT-23-6
- Recommended Bypass Capacitor .................... 1.0 $\mu \mathrm{F}$


## APPLICATIONS

- Constant voltage power source for hand-held equipment
- OLED power supply for hand-held equipment
- White LED driver for hand-held equipment


## R1204x

No. EA-284-180511

## SELECTION GUIDE

The package type, the OVP detector threshold, the feedback voltage and the PWM//VFM auto-switching control are user- selectable options as described below.

## Selection Guide

| Product Name | Package | Quantity per Reel | Pb Free | Halogen Free |
| :--- | :---: | :---: | :---: | :---: |
| R1204Kxy2z-TR | DFN(PLP)1820-6 | 5,000 pcs | Yes | Yes |
| R1204Nxy3z-TR-FE | TSOT-23-6 | $3,000 \mathrm{pcs}$ | Yes | Yes |

x: OVP Detector Threshold
1: 23 V
2: 33 V
3: 42 V
y : Current Limit
1: Typ. 900 mA
z: Feedback Voltage, Oscillator Frequency, PWM/VFM Auto-Switching Control

| $\mathbf{z}$ | Feedback Voltage | Oscillator Frequency | PWM/VFM <br> Auto-Switching Control |
| :---: | :---: | :---: | :---: |
| A | Typ. 0.2 V |  | No |
| B | Typ. 1 V |  | No |
| C | Typ. 1 V |  | Yes |
| D | Typ. 0.2 V |  | No |
| E | Typ. 1 V | Typ. 750 kHz | No |
| F | Typ. 1 V |  | Yes |
| G | Typ. 0.4 V |  | No |
| H |  |  | Typ. 1 MHz |

## BLOCK DIAGRAMS



## R1204x

No. EA-284-180511


## PIN DESCRIPTIONS




TSOT-23-6 Pin Configuration

DFN(PLP)1820-6 Pin Description

| Pin No | Symbol | Description |
| :---: | :---: | :--- |
| 1 | Vout | Output Pin |
| 2 | Lx $^{2}$ | Switching Pin, Open Drain Output |
| 3 | GND | Ground Pin |
| 4 | VIN | Input Pin |
| 5 | CE | Chip Enable Pin, Active-high |
| 6 | $V_{\text {FB }}$ | Feedback Pin |

The exposed tab is substrate level (GND). It is recommended that the exposed tab be connected to the ground plane on the board or otherwise be left open.

TSOT-23-6 Pin Description

| Pin No | Symbol | Description |
| :---: | :---: | :--- |
| 1 | Lx | Switching Pin, Open Drain Output |
| 2 | GND | Ground Pin |
| 3 | $V_{\text {FB }}$ | Feedback Pin |
| 4 | CE | Chip Enable Pin, Active-high |
| 5 | Vout | Output Pin |
| 6 | $V_{I N}$ | Input Pin |

No. EA-284-180511

## ABSOLUTE MAXIMUM RATINGS

| Absolute Maximum Ratings |  |  |  |  | (GND = 0 V ) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Symbol | Parameter |  |  | Rating | Unit |
| VIN | VIN Pin Voltage |  |  | -0.3 to 6.5 | V |
| $V_{\text {ce }}$ | CE Pin Voltage |  |  | -0.3 to 6.5 | V |
| $\mathrm{V}_{\mathrm{FB}}$ | $\mathrm{V}_{\mathrm{FB}}$ Pin Voltage |  |  | -0.3 to 6.5 | V |
| Vout | Vout Pin Voltage |  |  | -0.3 to 48 | V |
| VLx | Lx Pin Voltage |  |  | -0.3 to 48 | V |
| ILX | Lx Pin Current |  |  | 1200 | mA |
| Pd | Power Dissipation ${ }^{(1)}$ | DFN(PLP)1820-6 | JEDEC STD. 51-7 | 2200 | mW |
|  |  | TSOT-23-6 | Standard Test <br> Land Pattern | 460 |  |
| Tj | Junction Temperature Range |  |  | -40 to 125 | ${ }^{\circ} \mathrm{C}$ |
| Tstg | Storage Temperature Range |  |  | -55 to 125 | ${ }^{\circ} \mathrm{C}$ |

## ABSOLUTE MAXIMUM RATINGS

Electronic and mechanical stress momentarily exceeded absolute maximum ratings may cause the permanent damages and may degrade the lifetime and safety for both device and system using the device in the field. The functional operation at or over these absolute maximum ratings is not assured.

## RECOMMENDED OPERATING CONDITIONS

Recommended Operating Conditions

| Symbol | Parameter | Rating | Unit |
| :---: | :--- | :---: | :---: |
| $\mathrm{V}_{\text {IN }}$ | Input Voltage | 2.3 to 5.5 | V |
| Ta | Operating Temperature Range | -40 to 85 | ${ }^{\circ} \mathrm{C}$ |

## RECOMMENDED OPERATING CONDITIONS

All of electronic equipment should be designed that the mounted semiconductor devices operate within the recommended operating conditions. The semiconductor devices cannot operate normally over the recommended operating conditions, even if when they are used over such ratings by momentary electronic noise or surge. And the semiconductor devices may receive serious damage when they continue to operate over the recommended operating conditions.

[^0]
## ELECTRICAL CHARACTERISTICS



All test items listed under Electrical Characteristics are done under the pulse load condition $\left(\mathrm{Tj} \approx \mathrm{Ta}=25^{\circ} \mathrm{C}\right)$.

## R1204x

No. EA-284-180511

## THEORY OF OPERATION

## Operation of Step-Up DC/DC Converter and Output Current

<Basic Circuit>


## <Current through L>



There are two operation modes of the step-up PWM control-DC/DC converter. That is the continuous mode and discontinuous mode by the continuousness inductor.
When the transistor turns ON, the voltage of inductor L becomes equal to VIN voltage. The increase value of inductor current (i1) will be
$\Delta \mathrm{i} 1=\mathrm{V}_{\mathrm{IN}} \times$ ton $/ \mathrm{L}$
Formula 1

As the step-up circuit, during the OFF time (when the transistor turns OFF) the voltage is continually supply from the power supply. The decrease value of inductor current (i2) will be
$\Delta \mathrm{i} 2=\left(\mathrm{V}_{\text {out }}-\mathrm{V}_{\text {IN }}\right) \times$ topen $/ \mathrm{L}$
Formula 2

At the PWM control-method, the inductor current become continuously when topen = toff, the DC/DC converter operate as the continuous mode.

In the continuous mode, the variation of current of i1 and i2 is same at regular condition.
$V_{\text {IN }} \times$ ton $/ L=\left(\right.$ Vout $\left.-V_{\text {IN }}\right) \times$ toff $/ L$
Formula 3

The duty at continuous mode will be
duty $(\%)=$ ton $/($ ton + toff $)=\left(\right.$ VOUT $\left.-\mathrm{V}_{\text {IN }}\right) / \mathrm{V}_{\text {OUT }}$ Formula 4

The average of inductor current at $\mathrm{tf}=$ toff will be
$\mathrm{IL}($ Ave. $)=\mathrm{V}_{\mathrm{IN}} \times \operatorname{ton} /(2 \times \mathrm{L})$ Formula 5

If the input voltage $=$ output voltage, the lout will be
lout $=\mathrm{V}_{\text {IN } 2} \times$ ton $/\left(2 \times \mathrm{L} \times \mathrm{V}_{\text {OUT }}\right)$
Formula 6

If the lout value is large than above the calculated value (Formula 6), it will become the continuous mode, at this status, the peak current (llmax) of inductor will be

```
ILmax = lout }\times\mp@subsup{\textrm{V}}{\mathrm{ OUt }}{}/\mp@subsup{\textrm{V}}{\mathrm{ IN }}{}+\mp@subsup{\textrm{V}}{\mathrm{ IN }}{}\times\mathrm{ ton / ( }2\times\textrm{L}
```

$\qquad$

``` Formula 7
ILmax \(=\) lout \(\times\) Vout \(/ \mathrm{V}\) IN \(+\mathrm{V}_{\text {IN }} \times \mathrm{T} \times(\) Vout -VIN\() /(2 \times \mathrm{L} \times\) Vout \()\) Formula 8
```

The peak current value is larger than the lout value. In case of this, selecting the condition of the input and the output and the external components by considering of Ilmax value.
The explanation above is based on the ideal calculation, and the loss caused by LX switch and the external components are not included.
The actual maximum output current will be between $50 \%$ and $80 \%$ by the above calculations. Especially, when the IL is large or $\mathrm{V}_{\mathbb{I N}}$ is low, the loss of $\mathrm{V}_{\mathbb{I}}$ is generated with on resistance of the switch. Moreover, it is necessary to consider Vf of the diode (approximately 0.8 V ) about Vout.

## R1204x

No. EA-284-180511

## PWM/VFM Auto-Switching Control (R1204xxxxC/F)

In low output current, the IC automatically switches to high-efficiency VFM mode. The minimum Onduty (Don_min) of VFM mode is set to approximately $30 \%$ and is fixed inside the IC. If the difference between the voltages of the input and the output is small, or the Onduty in continuous mode (Don_con) becomes lower than Don_min, the IC will not shift to PWM mode but will stay with VFM mode instead even in high output current, as a result, the ripple current will be increased. Don_min should be $70 \%$ or more $\left(\mathrm{V}_{\text {SET }}>\mathrm{V}_{\text {IN }} \times 3.33\right.$ ).

## Soft-Start Function

## (R1204xxxxA/D/G/H)

Unless otherwise Vout is beyond the threshold (Vf x number of LED lights), current will not flow through LEDs, as a result, $\mathrm{V}_{\mathrm{FB}}$ voltage will not increase. The IC increases Vout by controlling the output of error amplifier to " H " and turning the Lx switch on and off for a certain period of time (until the current flow). At the mean time, the inrush current is controlled by gradually increasing the current limit. If Vout is over the threshold (the current flows), the IC controls the soft-start function by gradually increasing the reference voltage of error amplifier.

## (R1204xxxxB/C/E/F)

The IC controls the soft-start function by gradually increasing the reference voltage of error amplifier. Soft-start begins when the output voltage of error amplifier is 0 V and ends when it reaches the constant voltage.

## Current Limit Function

If the peak current of inductor (llmax) exceeds the current limit, current limit function turns the driver off and turns it on in every switching cycle to continually monitor the driver current.

## Under Voltage Lock Out Function (UVLO)

UVLO function stops DC/DC operation and prevents malfunction when the supply voltage falls below the UVLO detector threshold.

## Over Voltage Protection Circuit (OVP)

OVP circuit monitors the Vout pin voltage and if it reaches the OVP voltage it will stop oscillation. When the Vout pin voltage decreases it will restart oscillation, but if the cause of the excess Vout pin voltage is not removed the OVP circuit will operate repeatedly so as to restrict the Vout pin voltage.

## Thermal Shutdown Function

If the junction temperature exceeds the thermal shutdown temperature, thermal shutdown function turns the driver off. If the junction temperature becomes lower than the thermal shutdown released temperature, the thermal shutdown function resets the IC to restart the operation.

## APPLICATION INFORMATION

## R1204xxxxA/D/G/H Typical Applications



Figure 1.

Figure 3.



Figure 2.


Figure 4.

## R1204xxxxB/C/E/F Typical Applications



Figure 5.


Figure 6.

## R1204x

No. EA-284-180511

## Selection of Inductor

Peak current of inductor (lımax) in normal mode when the efficiency is $80 \%$ can be calculated by the following formula.


- When starting up the IC or when adjusting the brightness of LEDs, a large transient current may flow into an inductor (L1).
- Ilmax should be equal or smaller than the current limit of the IC
- When deciding the rated current of inductor, Ilmax should be considered.
- It is recommended that L 1 with $10 \mu \mathrm{H}$ to $22 \mu \mathrm{H}$ be used.

Table 1. Peak Current Values for $\mathrm{V}_{\mathrm{IN}}$, $\mathrm{V}_{\text {out, }}$ lout, and L1

| ViN $^{(V)}$ | Vout (V) | lout (mA) | $\mathbf{L 1}(\boldsymbol{\mu H})$ | ILMAX (mA) |
| :---: | :---: | :---: | :---: | :---: |
| 3 | 21 | 20 | 10 | 280 |
| 3 | 21 | 20 | 22 | 225 |
| 3 | 30 | 20 | 10 | 365 |
| 3 | 30 | 20 | 22 | 305 |

Table 2. Recommended Inductors

| L1 ( $\mu \mathrm{H}$ ) | Parts No. | Rated Current (mA) | Size (mm) | Versions |
| :---: | :---: | :---: | :---: | :---: |
| 10 | VLS252010ET-100M | 550 | $2.5 \times 2.0 \times 1.0$ | R1204xxxxA/B/C/G |
| 10 | VLF302512MT-100M | 620 | $3.0 \times 2.5 \times 1.2$ |  |
| 10 | VLF403212MT-100M | 900 | $4.0 \times 3.2 \times 1.2$ |  |
| 22 | VLF302512MT-220M | 430 | $3.0 \times 2.5 \times 1.2$ | R1204xxxxD/E/F/H |
| 22 | VLF403212MT-220M | 540 | $4.0 \times 3.2 \times 1.2$ |  |
| 22 | VLF504012MT-220M | 800 | $5.0 \times 4.0 \times 1.2$ |  |

## Selection of Capacitor

- Place a $1 \mu \mathrm{~F}$ or more bypass capacitor (C1) as close as possible to the $\mathrm{V}_{\mathrm{IN}}$ and GND pins


## [R1204xxxxA/D/G/H]

- Place a $1 \mu \mathrm{~F}$ or more output capacitor (C2) as close as possible to the Vout and GND pins.
- In the case of operating the inductor using a separated power supply from the IC, place a $1 \mu \mathrm{~F}$ or more bypass capacitor (C3) as close as possible to Vinductor and the GND pin.
- Note the Vout that depends on LED used, and select the rating of Vout or more.


## [R1204xxxxB/C/E/F]

- Place $1 \mu \mathrm{~F}$ to $10 \mu \mathrm{~F} \mathrm{C} 2$ as close as possible to the Vout and GND pins.
- In the case of operating the inductor using a separated power supply from the IC, place a $1 \mu \mathrm{~F}$ or more bypass capacitor (C4) as close as possible to Vinductor and the GND pin.


## SBD (Schottky Barrier Diode) Selection

- Choose a diode that has low $\mathrm{V}_{\mathrm{F}}$, low reverse current $\mathrm{I}_{\mathrm{R}}$, and low capacitance.
- SBD is an ideal type of diode for R 1204 x since it has low $\mathrm{V}_{\mathrm{F}}$, low reverse current $\mathrm{I}_{\mathrm{R}}$, and low capacitance.

Table 3. Recommended Components for R1204xxxxA/D/G/H

| Symbol | Rated Voltage (V) | Parts No. |
| :---: | :---: | :---: |
| D1 | 60 | CRS12 |
| C1 | 6.3 | CM105B105K06 |
| C2 | 50 | C2012X5R1H105K |
|  |  | C2012X5R1H225K |
| C3 (Option: Figure 4) | Select by the input voltage | (R1204xxxxG/H: ILED $>22 \mathrm{~mA})$ |

Table 4. Recommended Components for R1204xxxxB/C/E/F

| Symbol | Rated Voltage (V) | Parts No. |
| :---: | :---: | :---: |
| D1 | 60 | CRS12 |
| C1 | 6.3 | CM105B105K06 |
| C2 | 16 | C2012X5R1C475K |
|  | 25 | C2012X5R1E105K |
|  | 50 | C2012X5R1H105K |
| C4 (Option: Figure 6) | Select by the input voltage | $1 \mu \mathrm{~F}$ or more |

Table 5. Recommended Component Values for R1204xxxxB/C/E/F

| $V_{\text {SET }}(\mathbf{V})$ | $\mathbf{7}<\mathrm{V}_{\text {SET }} \leq \mathbf{1 0}$ | $\mathbf{1 0}<\mathrm{V}_{\text {SET }} \leq \mathbf{2 5}$ | $\mathbf{2 5}<\mathrm{V}_{\text {SET }}$ |
| :---: | :---: | :---: | :---: |
| $\mathrm{R} 1(\mathrm{k} \Omega)$ | 10 | 10 | 10 |
| $R 2(\mathrm{k} \Omega)$ | $\left(\mathrm{V}_{\text {SET }}-1\right) \times \mathrm{R} 1$ | $\left(\mathrm{~V}_{\text {SET }}-1\right) \times \mathrm{R} 1$ | $\left(\mathrm{~V}_{\text {SET }}-1\right) \times \mathrm{R} 1$ |
| $\mathrm{R} 3(\Omega)$ | 0 | 0 | 0 |
| $\mathrm{C} 1(\mu \mathrm{~F})$ | 1.0 | 1.0 | 1.0 |
| $\mathrm{C} 2(\mu \mathrm{~F})$ | 4.7 | $1.0 \times 2$ | 1.0 |
| $\mathrm{C} 3(\mathrm{pF})$ | 10 | 10 | 10 |
| $\mathrm{C} 4(\mu \mathrm{~F})$ | 1.0 | 1.0 | 1.0 |

## R1204x

No. EA-284-180511

## Other External Components Settings

Set a capacitor (C3) between the Vout and $V_{\text {FB }}$ pins to improve the response of DC/DC converter by giving high-frequency voltage feedback. Please note that C3 operation could be different from the theory of operation depending on component layouts and parasitic capacitances.

## Output Voltage Setting (R1204xxxxB/C/E/F)

The relation between the output voltage $\left(\mathrm{V}_{\mathrm{SET}}\right)$ and the resistors $(\mathrm{R} 1, \mathrm{R} 2)$ is calculable by the following formula.
$V_{S E T}=V_{F B} \times(R 1+R 2) / R 1$
The sum of R1 and R2 should be $300 \mathrm{k} \Omega$ or less. Ensure the $\mathrm{V}_{\text {IN }}$ and GND lines are sufficiently robust. If their impedances are too high, noise pickup or unstable operation may result. Set a capacitor (C2) with a suitable voltage resistance (more than 1.5 times of $V_{S E T}$ ) between the $V_{I N}$ and GND pins, and as close as possible to the pins.

## LED Current Setting (R1204xxxxA/D/G/H)

The LED current (lled) when a "H" signal is applied to the CE pin (Duty $=100 \%$ ) can be determined by the value of feedback resistor (R1).
$I_{\text {LED }}=0.2 / R 1(R 1204 x x x x A / D)$
liED $=0.4 / R 1$ (R1204xxxxG/H)

## LED Dimming Control (R1204xxxxA/D/G/H)

The brightness of the LEDs can be adjusted by applying a PWM signal to the CE pin. By inputting "L" voltage for a certain period of time (Typ. 9 ms (R1204xxxxA/G) / 12 ms (R1204xxxxD/H) or more), the IC goes into standby mode and turns off LEDs. ILed can be controlled by the duty of a PWM signal for the CE pin. The relation between the high-duty of the CE pin (Hduty) and ILED is calculatable by the following formula.
$\mathrm{I}_{\text {LED }}=$ Hduty $\times \mathrm{V}_{\mathrm{FB}} / \mathrm{R} 1$

The frequency range of a PWM signal should be set within the range of 200 Hz to 300 kHz . In the case of using a 20 kHz or less PWM signal for dimming the LEDs, the increasing or decreasing of the inductor current (IL) may make noise in the audible band. In this case, a high frequency PWM signal should be used.


Figure 7. Dimming Control by CE Pin

## Low luminance Dimming Accuracy (R1204xxxxG/H)

Low luminance Dimming filtered $\mathrm{V}_{\mathrm{FB}}$ voltage tolerance depends on the offset voltage of the internal DC/DC converter. By this offset voltage, some voltage difference may be generated between $\mathrm{V}_{\mathrm{ref}}$ voltage and $\mathrm{V}_{\mathrm{fb}}$ voltage. Low luminance Dimming Accuracy is shown in Table 5.

Table 6. Low luminance Dimming Accuracy for R1204xxxxG/H (R1 = $20 \Omega$ )

| The duty of a PWM signal for the CE pin | Iled Min. | Iled Max. |
| :---: | :---: | :---: |
| $3.5 \%$ (Frequency $=20 \mathrm{kHz}$ to 300 kHz$)$ | $0.01 \mathrm{~mA}^{(2)}$ | $2.1 \mathrm{~mA}^{(2)}$ |

## R1204x

No. EA-284-180511

## TECHNICAL NOTES

## Current Path on PCB

Figure 8 and Figure 9 show flows of current paths of the application circuits when MOSFET is ON and when MOSFET is OFF, respectively.

- Parasitic elements (impedance, inductance or capacitance) in the paths pointed with red arrows in Figure 8 and Figure 9 influence stability of the system and cause noise outbreak. It is recommended that these parasitic elements be minimized.
- In addition, except for the paths of LED load, it is recommended that the all wirings of the current paths be made as short and wide as possible.


Figure 8. MOSFET-ON


Figure 9. MOSFET-OFF

## Layout Guide for PCB

- Place C 1 as close as possible to the $\mathrm{V}_{\mathrm{IN}}$ and GND pins. Also, connect the GND pin to the wider GND plane.
- Make the $L x$ land pattern as small as possible.
- Make the wirings between the Lx pin, the inductor and the diode as short as possible. Also, connect C2 as close as possible to the cathode of the diode.
- Place C2 as close as possible to the GND pin.

PCB Layout
PKG: DFN(PLP)1820-6 pin
R1204Kxx2A/D/G/H


R1204Kxx2B/C/E/F


## R1204x

No. EA-284-180511

PKG: TSOT-23-6 pin
R1204Nxx3A/D/G/H


R1204Nxx3B/C/E/F


## TYPICAL CHARACTERISTICS

1) Efficiency vs. Output Current of R1204xxxxA/D/G/H

Used LED: NICHIA, NSSW208A ( $\mathrm{Vf}=3.0 \mathrm{~V}$ (Led = 20 mA ) )
1-1) Efficiency vs. Output Current with Different Output Voltages, 10 LEDs in Series (Vout $=30 \mathrm{~V}$ (lout = 20 mA ))

R1204xxxxA/G, L = $10 \boldsymbol{\mu H}$ (VLF302512MT-100M)


8 LEDs in Series (Vout $=24 \mathrm{~V}$ (lout $=\mathbf{2 0} \mathrm{mA}$ ))
R1204xxxxA/G, L = $10 \boldsymbol{\mu H}$ (VLF302512MT-100M)


6 LEDs in Series (Vout $=18 \mathrm{~V}$ (lout $=\mathbf{2 0} \mathrm{mA})$ ) R1204xxxxA/G, L = $10 \mu \mathrm{H}$ (VLF302512MT-100M)


R1204xxxxD/H, L = $\mathbf{2 2} \boldsymbol{\mu H}$ (VLF302512MT-220M)


R1204xxxxD/H, L=22 $\boldsymbol{\mu} \mathrm{H}$ (VLF302512MT-220M)


R1204xxxxD/H, L=22 $\boldsymbol{\mu} \mathrm{H}$ (VLF302512MT-220M)


## R1204x

No. EA-284-180511

1-2) Efficiency vs. Output Current with Different Inductors (Vin $=3.6 \mathrm{~V}$ )
10 LEDs in Series (Vout =30 V (lout $=\mathbf{2 0 ~ m A})$ )


R1204xxxxD/H


8 LEDs in Series (Vout = 24 V (lout = 20 mA$)$ )

R1204xxxxA/G


R1204xxxxD/H


1-3) Efficiency vs. Output Current with Different Numbers of LEDs
LEDs in 3 Parallels ( $\mathrm{V}_{\mathrm{IN}}=3.6 \mathrm{~V}$ )

## R1204xxxxA/G, L=10 $\mu \mathrm{H}$ (VLF302512MT-100M)



R1204xxxxD/H, L=22 $\mu \mathrm{H}$ (VLF302512MT-220M)


LEDs in 3 Parallels ( $\mathrm{V}_{\mathrm{in}}=5.0 \mathrm{~V}$ )
R1204xxxxA/G, L = $10 \mu \mathrm{H}$ (VLF302512MT-100M)


R1204xxxxD/H, L = $22 \boldsymbol{\mu H}$ (VLF302512MT-220M)


1-4) Efficiency vs. Output Current with Different Numbers of LEDs
LEDs in 3 Parallels ( $\mathrm{V}_{\mathrm{IN}}=3.6 \mathrm{~V}$, Inductor Voltage $=12.0 \mathrm{~V}$ )

R1204xxxxA/G, L = $10 \boldsymbol{\mu H}$ (VLF302512MT-100M)


R1204xxxxD/H, L = $22 \boldsymbol{\mu}$ (VLF302512MT-220M)


LEDs in 6 Parallels ( $\mathrm{V}_{\mathrm{IN}}=3.6 \mathrm{~V}$, Inductor Voltage $=12.0 \mathrm{~V}$ )
R1204xxxxA/G, L = $10 \boldsymbol{\mu}$ (VLF302512MT-100M)


R1204xxxxD/H, L = $22 \boldsymbol{\mu H}$ (VLF302512MT-220M)


## R1204x

No. EA-284-180511
2) Efficiency vs. Output Current of R1204xxxxB/C/E/F

2-1) Efficiency vs. Output Current with Different Output Voltages
$\mathrm{V}_{\mathrm{set}}=31 \mathrm{~V}$
$\mathrm{V}_{\mathrm{IN}}=$ Inductor Voltages

R1204xxxxC, L = $10 \mu \mathrm{H}$ (VLF302512MT-100M)


Different $\mathrm{V}_{\text {IN }}$ / Inductor Voltages ( $\mathrm{V}_{\mathrm{IN}}=3.6 \mathrm{~V}$ )
R1204xxxxC, L = $10 \boldsymbol{\mu H}$ (VLF302512MT-100M)

$V_{\text {SET }}=25 \mathrm{~V}$
$\mathrm{V}_{\mathrm{IN}}=$ Inductor Voltages
R1204xxxxC, L = $10 \boldsymbol{\mu H}$ (VLF302512MT-100M)


R1204xxxxF, L = $22 \boldsymbol{\mu H}$ (VLF302512MT-220M)


R1204xxxxF, L = $22 \boldsymbol{\mu H}$ (VLF302512MT-220M)


R1204xxxxF, L = $22 \boldsymbol{\mu H}$ (VLF302512MT-220M)


Different $\mathrm{V}_{\mathrm{IN}} /$ Inductor Voltages ( $\mathrm{ViN}_{\mathrm{IN}}=3.6 \mathrm{~V}$ )
R1204xxxxC, L = $10 \boldsymbol{\mu}$ (VLF302512MT-100M)

$\mathrm{V}_{\text {set }}=21 \mathrm{~V}$
$\mathrm{V}_{\mathrm{IN}}=$ Inductor Voltage
R1204xxxxC, L = $10 \mu \mathrm{H}$ (VLF302512MT-100M)


Different $\mathrm{V}_{\mathrm{IN}}$ / Inductor Voltages ( $\mathrm{V}_{\mathrm{IN}}=3.6 \mathrm{~V}$ ) R1204xxxxC, L = $10 \boldsymbol{\mu}$ (VLF302512MT-100M)


R1204xxxxF, L = $22 \boldsymbol{\mu H}$ (VLF302512MT-220M)


R1204xxxxF, L = $22 \boldsymbol{\mu H}$ (VLF302512MT-220M)


R1204xxxxF, L = $\mathbf{2 2} \boldsymbol{\mu} \mathrm{H}$ (VLF302512MT-220M)


## R1204x

No. EA-284-180511

2-2) Efficiency vs. Output Current with PWM Control and PWM/VFM Auto-Switching Control $\left(\mathrm{V}_{\mathrm{IN}}=3.6 \mathrm{~V}, \mathrm{~V}_{\text {SET }}=12 \mathrm{~V}\right.$ )

R1204xxxxB/C, L = $10 \boldsymbol{\mu}$ (VLF302512MT-100M)


R1204xxxxE/F, L=22 $\boldsymbol{\mu}$ H (VLF302512MT-220M)


Inductor Voltage = 7.2 V, $\mathrm{V}_{\text {SET }}=25 \mathrm{~V}$
R1204xxxxB/C, L = $10 \mu \mathrm{H}$ (VLF302512MT-100M)

3) Maxduty vs. ILed (R1204xxxxA/D/G/H, 10 LEDs in Series, Vin = 3.6 V )

4) Vout / ILed Ripple of R1204xxxxA/D/G/H When Dimming (10 LEDs in Series, L=10 $\boldsymbol{\mu} \mathrm{H}$ (VLF302512MT-100M))


5) Vout Ripple ( $\mathrm{V}_{\mathrm{IN}}=3.6 \mathrm{~V}$, $\mathrm{V}_{\text {SET }}=21 \mathrm{~V}$, lout $=0 \mathrm{~mA}, \mathrm{~L}=10 \mu \mathrm{H}$ (VLF302512MT-100M) $)$

PWM Control (R1204xxxxB)


VFM Control (R1204xxxxC)


## R1204x

No. EA-284-180511
6) Load Transient Response
( $\mathrm{V}_{\mathrm{IN}}=3.6 \mathrm{~V}, \mathrm{~V}_{\mathrm{SET}}=25 \mathrm{~V}, \mathrm{~L}=10 \mu \mathrm{H}$ (VLF302512MT-100M), lout $=10 \mathrm{~mA} \Leftrightarrow 30 \mathrm{~mA}, \mathrm{Tr}=\mathrm{Tf}=0.5 \mu \mathrm{~s}$ )

7) Supply Current vs. Ambient Temperature

9) VFB Voltage vs. Ambient Temperature


R1204xxxxF

8) UVLO vs. Ambient Temprature


R1204xxxxG/H


10) Switch ON Resistance vs. Ambient Temperature R1204x3xxx

11) OVP Voltage vs. Ambient Temperature

12) LX Limit Current vs. Ambienet Temperature


## R1204x

No. EA-284-180511
13) Oscillator Frequency vs. Ambiemnt Temperature

R1204xxxxA/B/C/G


R1204xxxxD/E/F/H


The power dissipation of the package is dependent on PCB material, layout, and environmental conditions. The following measurement conditions are based on JEDEC STD. 51-7.

Measurement Conditions

| Item | Measurement Conditions |
| :--- | :--- |
| Environment | Mounting on Board (Wind Velocity $=0 \mathrm{~m} / \mathrm{s}$ ) |
| Board Material | Glass Cloth Epoxy Plastic (Four-Layer Board) |
| Board Dimensions | $76.2 \mathrm{~mm} \times 114.3 \mathrm{~mm} \times 0.8 \mathrm{~mm}$ |
| Copper Ratio | Outer Layer (First Layer): Less than 95\% of 50 mm Square <br> Inner Layers (Second and Third Layers): Approx. 100\% of 50 mm Square <br> Outer Layer (Fourth Layer): Approx. 100\% of 50 mm Square |
| Through-holes | $\phi 0.2 \mathrm{~mm} \times 34$ pcs |

Measurement Result
$\left(\mathrm{Ta}=25^{\circ} \mathrm{C}, \mathrm{Tjmax}=125^{\circ} \mathrm{C}\right)$

| Item | Measurement Result |
| :--- | :---: |
| Power Dissipation | 2200 mW |
| Thermal Resistance $(\theta j \mathrm{ja})$ | $\theta \mathrm{ja}=45^{\circ} \mathrm{C} / \mathrm{W}$ |
| Thermal Characterization Parameter $(\psi j \mathrm{t})$ | $\psi j \mathrm{t}=18^{\circ} \mathrm{C} / \mathrm{W}$ |

Өja: Junction-to-Ambient Thermal Resistance
$\psi j$ t: Junction-to-Top Thermal Characterization Parameter



UNIT: mm

## DFN(PLP)1820-6 Package Dimensions

[^1]The power dissipation of the package is dependent on PCB material, layout, and environmental conditions. The following conditions are used in this measurement.

Measurement Conditions

| Item | Standard Test Land Pattern |
| :--- | :--- |
| Environment | Mounting on Board (Wind Velocity $=0 \mathrm{~m} / \mathrm{s}$ ) |
| Board Material | Glass Cloth Epoxy Plastic (Double-Sided Board) |
| Board Dimensions | $40 \mathrm{~mm} \times 40 \mathrm{~mm} \times 1.6 \mathrm{~mm}$ |
| Copper Ratio | Top Side: Approx. $50 \%$ <br> Bottom Side: Approx. $50 \%$ |
| Through-holes | $\phi 0.5 \mathrm{~mm} \times 44$ pcs |

Measurement Result
$\left(\mathrm{Ta}=25^{\circ} \mathrm{C}, \mathrm{Tjmax}=125^{\circ} \mathrm{C}\right)$

| Item | Standard Test Land Pattern |
| :--- | :---: |
| Power Dissipation | 460 mW |
| Thermal Resistance ( $\theta \mathrm{ja}$ ) | $\theta \mathrm{ja}=217^{\circ} \mathrm{C} / \mathrm{W}$ |
| Thermal Characterization Parameter $(\psi j \mathrm{t})$ | $\psi j \mathrm{j}=40^{\circ} \mathrm{C} / \mathrm{W}$ |

$\theta \mathrm{ja}$ : Junction-to-Ambient Thermal Resistance
$\psi j$ t: Junction-to-Top Thermal Characterization Parameter


Power Dissipation vs. Ambient Temperature


Measurement Board Pattern


UNIT: mm
TSOT-23-6 Package Dimensions

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[^0]:    ${ }^{(1)}$ Refer to POWER DISSIPATION for detailed information

[^1]:    * The tab on the bottom of the package is substrate level (GND). It is recommended that the tab be connected to the ground plane on the board, or otherwise be left floating.

