## 600 mA 6 MHz Synchronous Step-down DCIDC Converter

NO. EA-318-171106

## OUTLINE

The RP508K is a low supply current PWM/VFM step-down DC/DC converter with synchronous rectifier featuring $600 \mathrm{~mA}^{(1)}$ output current. Internally, a single converter consists of an oscillator, a reference voltage unit, an error amplifier, a switching control circuit, a mode control circuit, a soft-start circuit, an under-voltage lockout (UVLO) circuit, an over current protection circuit, a thermal shutdown circuit and switching transistors. By the adoption of the synchronous rectification circuit with built-in switching transistors, the RP508K works as efficient step-down DC/DC converter, without connecting external diodes. Using synchronous rectification not only increases circuit performance but also allows a design to reduce parts count.
Power controlling method can be selected from forced PWM control type or PWM/VFM auto switching control type by inputting a signal to the MODE pin. In low output current, forced PWM control switches at fixed frequency rate in order to reduce noise. Likewise, in low output current, PWM/VFM auto switching control automatically switches from PWM mode to VFM mode in order to achieve high efficiency.
Output voltage is internally fixed type which allows output voltages that range from 0.8 V to 3.3 V in 0.1 V step. The output voltage accuracy is as high as $\pm 1.5 \%$ or $\pm 18 \mathrm{mV}$.
Protection circuits included in the RP508K are over current protection circuit and thermal shutdown circuit. Over current protection circuit supervises the inductor peak current in each switching cycle, and if the current exceeds the Lx current limit (ILxLIm), it turns off P-channel Tr. Thermal shutdown circuit detects overheating of the converter if the output pin is shorted to the ground pin (GND) etc. and stops the converter operation to protect it from damage if the junction temperature exceeds the specified temperature.
The RP508K is offered in a small and thin 6-pin DFN(PLP)1212-6F package which achieves the smallest possible footprint solution on boards where area is limited.
For an input capacitor ( $\mathrm{C}_{\mathrm{IN}}$ ) and an output capacitor (Cout), the smaller sized 0402/1005 (inch/mm) capacitor can be used. For an inductor (L), the smaller sized 0603/1608 or 1005/2012 (inch/mm) inductor can be used.

## FEATURES




- Supply Current (IDD2) ............................................. Typ. $15 \mu \mathrm{~A}$ (VFM Mode with No-Ioad)
- Standby Current (Istandby) ..................................................... $0 \mu \mathrm{~A}$
- Output Voltage Temperature Coefficient ( $\Delta$ Vout/Ta) $\cdots \cdots$... Typ. $\pm 100 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$
- Oscillator Frequency (fosc)................................................... 6.0 MHz
- Maximum Duty Cycle (Maxduty) ..................................... 100\%
- Built-in Driver ON Resistance (Ronp, Ronn) $\ldots \ldots \ldots \ldots \ldots$........... Typ. Pch. $0.33 \Omega$, Nch. $0.24 \Omega\left(\mathrm{~V}_{\mathrm{IN}}=3.6 \mathrm{~V}\right)$
- UVLO Detector Threshold (VuvLoo1) .......................... Typ. 2.0 V
- Soft-start Time (tstart) .............................................................. $90 \mu \mathrm{~s}$

[^0]
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- Lx Current Limit Circuit (Ilxlim)

Typ. 1.1 A


- Package ......................................................... DFN(PLP)1212-6F


## APPLICATIONS

- Cellular Phones
- Smartphones
- Digital Still Camera
- Notebook PCs, PDA's
- Li-ion Battery-used Equipment


## SELECTION GUIDE

The set output voltage and the auto discharge ${ }^{(1)}$ function are user-selectable options.

## Selection Guide

| Product Name | Package | Quantity per Reel | Pb Free | Halogen Free |
| :---: | :---: | :---: | :---: | :---: |
| RP508Kxx1\$-TR | DFN(PLP)1212-6F | $5,000 \mathrm{pcs}$ | Yes | Yes |

xx : Specify the set output voltage $\left(\mathrm{V}_{\mathrm{SET}}\right)$ within the range of $0.8 \mathrm{~V}(08)$ to $3.3 \mathrm{~V}(33)$ in 0.1 V steps ${ }^{(2)}$.

If the set output voltage includes the 3rd digit, indicate the digit of 0.01 .
(1.05 V, 1.25 V, 1.35 V)

Ex. If the set output voltage is 1.05 V : RP508K101\$5
If the set output voltage is 1.25 V : RP508K121\$5
If the set output voltage is 1.35 V : RP508K131\$5
\$: Specify the auto-discharge option.
A: Fixed output voltage type
B: Fixed output voltage type, auto-discharge function in shutdown mode

[^1]
## BLOCK DIAGRAM



RP508Kxx1B Block Diagram

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## PIN DESCRIPTION



DFN(PLP)1212-6F Pin Configurations
Pin Description

| Pin No. | Symbol | Pin Description |
| :---: | :---: | :--- |
| 1 | VOUT | Output Pin |
| 2 | MODE | Mode Control Pin <br> ("H" forced PWM control, "L" PWM/VFM auto switching control) |
| 3 | CE | Chip Enable Pin ("H" active) |
| 4 | VIN | Input Pin |
| 5 | LX | LX Switching Pin |
| 6 | GND | Ground Pin |

## ABSOLUTE MAXIMUM RATINGS

| Symbol | Item | Rating | Unit |
| :---: | :---: | :---: | :---: |
| VIN | Vin Input Voltage | -0.3 to 6.5 | V |
| VLx | Lx Pin Voltage | -0.3 to VIN +0.3 | V |
| $V_{\text {ce }}$ | CE Pin Input Voltage | -0.3 to 6.5 | V |
| $V_{\text {mode }}$ | MODE Pin Input Voltage | -0.3 to 6.5 | V |
| Vout | Vout Pin Voltage | -0.3 to 6.5 | V |
| Itx | Lx Pin Output Current | 1300 | mA |
| PD | Power Dissipation ${ }^{(1)}$ (JEDEC STD 51-7 Test Land Pattern ) | 666 | mW |
| Tj | Junction Temperature Range | -40 to 125 | ${ }^{\circ} \mathrm{C}$ |
| Tstg | Storage Temperature Range | -55 to 125 | ${ }^{\circ} \mathrm{C}$ |

## ABSOLUTE MAXIMUM RATINGS

Electronic and mechanical stress momentarily exceeded absolute maximum ratings may cause the permanent damages and may degrade the life time and safety for both device and system using the device in the field. The functional operation at or over these absolute maximum ratings are not assured.

RECOMMENDED OPERATING CONDITIONS

| Symbol | Item | Rating | Unit |
| :---: | :--- | :---: | :---: |
| Vin | Input Voltage | 2.3 to 5.5 | V |
| Ta | Operating Temperature Range | -40 to 85 | ${ }^{\circ} \mathrm{C}$ |

## RECOMMENDED OPERATING CONDITIONS

All of electronic equipment should be designed that the mounted semiconductor devices operate within the recommended operating conditions. The semiconductor devices cannot operate normally over the recommended operating conditions, even if when they are used over such conditions by momentary electronic noise or surge. And the semiconductor devices may receive serious damage when they continue to operate over the recommended operating conditions.

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## ELECTRICAL CHARACTERISTICS

| RP508K Electrical Characteristics |  |  |  |  |  | $\left(\mathrm{Ta}=25^{\circ} \mathrm{C}\right)$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Symbol | Item | Conditions |  | Min. | Typ. | Max. | Unit |
| Vout | Output Voltage | $\mathrm{V}_{\mathrm{IN}}=\mathrm{V}_{\mathrm{CE}}=3.6 \mathrm{~V}$ | $\mathrm{V}_{\text {SET }} \geq 1.2 \mathrm{~V}$ | x0.985 |  | x1.015 | V |
|  |  |  | $\mathrm{V}_{\text {SET }}<1.2 \mathrm{~V}$ | -0.018 |  | +0.018 | V |
| fosc | Oscillator Frequency | $\begin{aligned} & V_{I N}=V_{C E}=3.6 \mathrm{~V}\left(V_{\text {SET }} \leq 2.6 \mathrm{~V}\right), \\ & V_{I N}=V_{C E}=V_{S E T}+1 \mathrm{~V}\left(V_{\text {SET }}>2.6 \mathrm{~V}\right) \end{aligned}$ |  | 5.4 | 6.0 | 6.6 | MHz |
| IdD1 | Supply Current 1 | $\begin{aligned} & \mathrm{V}_{\text {IN }}=\mathrm{V}_{\text {CE }}=5.5 \mathrm{~V}, \\ & \mathrm{~V}_{\text {OUT }}=\mathrm{V}_{\text {SET }} \times 0.8 \end{aligned}$ |  |  | 1000 | 1300 | $\mu \mathrm{A}$ |
| IDD2 | Supply Current 2 | $\begin{aligned} & V_{\text {IN }}=V_{\text {CE }}=V_{\text {OUT }} \\ & =5.5 \mathrm{~V} \end{aligned}$ | $\mathrm{V}_{\text {mode }}=0 \mathrm{~V}$ |  | 15 | 25 | $\mu \mathrm{A}$ |
|  |  |  | $\mathrm{V}_{\text {Mode }}=5.5 \mathrm{~V}$ |  | 1000 | 1300 | $\mu \mathrm{A}$ |
| Istandby | Standby Current | $\mathrm{V}_{\text {IN }}=5.5 \mathrm{~V}, \mathrm{~V}_{\text {CE }}=0 \mathrm{~V}$ |  |  | 0 | 5 | $\mu \mathrm{A}$ |
| Iceh | CE "H" Input Current | $\mathrm{V}_{\text {IN }}=\mathrm{V}_{\text {CE }}=5.5 \mathrm{~V}$ |  | -1 | 0 | 1 | $\mu \mathrm{A}$ |
| Icel | CE "L" Input Current | $\mathrm{V}_{\text {IN }}=5.5 \mathrm{~V}, \mathrm{~V}_{\text {CE }}=0 \mathrm{~V}$ |  | -1 | 0 | 1 | $\mu \mathrm{A}$ |
| $\mathrm{Imodeh}^{\text {l }}$ | Mode "H" Input Current | $\mathrm{V}_{\text {IN }}=\mathrm{V}_{\text {MOde }}=5.5 \mathrm{~V}, \mathrm{~V}_{\text {ce }}=0 \mathrm{~V}$ |  | -1 | 0 | 1 | $\mu \mathrm{A}$ |
| Imodel | Mode "L" Input Current | $\mathrm{V}_{\mathrm{IN}}=5.5 \mathrm{~V}, \mathrm{~V}_{\text {Ce }}=\mathrm{V}_{\text {MOde }}=0 \mathrm{~V}$ |  | -1 | 0 | 1 | $\mu \mathrm{A}$ |
| Ivouth | Vout "H" Input Current ${ }^{(1)}$ | $\mathrm{V}_{\text {In }}=\mathrm{V}_{\text {out }}=5.5 \mathrm{~V}, \mathrm{~V}_{\text {ce }}=0 \mathrm{~V}$ |  | -1 | 0 | 1 | $\mu \mathrm{A}$ |
| Ivoutl | Vout "L" Input Current | $\mathrm{V}_{\text {IN }}=5.5 \mathrm{~V}, \mathrm{~V}_{\text {CE }}=\mathrm{V}_{\text {OUt }}=0 \mathrm{~V}$ |  | -1 | 0 | 1 | $\mu \mathrm{A}$ |
| Rlow | On Resistance for Auto Discharge ${ }^{(2)}$ | $\mathrm{V}_{\text {IN }}=3.6 \mathrm{~V}, \mathrm{~V}_{\text {CE }}=0 \mathrm{~V}$ |  |  | 30 |  | $\Omega$ |
| ILXLEAKH | Lx Leakage Current "H" | $\mathrm{V}_{\mathrm{IN}}=\mathrm{V}_{\mathrm{LX}}=5.5 \mathrm{~V}, \mathrm{~V}_{\text {CE }}=0 \mathrm{~V}$ |  | -1 | 0 | 5 | $\mu \mathrm{A}$ |
| ILXLEAKL | Lx Leakage Current "L" | $\mathrm{V}_{\mathrm{IN}}=5.5 \mathrm{~V}, \mathrm{~V}_{\text {CE }}=\mathrm{V}_{\text {LX }}=0 \mathrm{~V}$ |  | -5 | 0 | 1 | $\mu \mathrm{A}$ |
| $\mathrm{V}_{\text {ceh }}$ | CE "H" Input Voltage | $\mathrm{V}_{\text {IN }}=5.5 \mathrm{~V}$ |  | 1.0 |  |  | V |
| $\mathrm{V}_{\text {cel }}$ | CE "L" Input Voltage | $\mathrm{V}_{\text {IN }}=2.3 \mathrm{~V}$ |  |  |  | 0.4 | V |
| Vmodeh | Mode "H" Input Voltage | $\mathrm{V}_{\mathrm{IN}}=\mathrm{V}_{\text {Ce }}=5.5 \mathrm{~V}$ |  | 1.0 |  |  | V |
| Vmodel | Mode "L" Input Voltage | $\mathrm{V}_{\text {IN }}=\mathrm{V}_{\text {CE }}=2.3 \mathrm{~V}$ |  |  |  | 0.4 | V |
| Ronp | On Resistance of Pch Tr. | $\mathrm{V}_{\mathrm{IN}}=3.6 \mathrm{~V}, \mathrm{ILX}^{\text {L }}=-100 \mathrm{~mA}$ |  |  | 0.33 |  | $\Omega$ |
| Ronn | On Resistance of Nch Tr. | $\mathrm{V}_{\mathrm{IN}}=3.6 \mathrm{~V}, \mathrm{lLX}=-100 \mathrm{~mA}$ |  |  | 0.24 |  | $\Omega$ |
| Maxduty | Maximum Duty Cycle | Soft-start Time is between the rising edge of CE pin and $V_{\text {out }} \geq V_{\text {SET }} \times 0.9$. |  | 100 |  |  | \% |
| tstart | Soft-start Time |  |  |  | 90 | 150 | $\mu \mathrm{S}$ |
| IlxLim | Lx Current Limit |  |  | 900 | 1100 |  | mA |
| Vuvloi | UVLO Detector Threshold | $\mathrm{V}_{\text {In }}=\mathrm{V}_{\text {ce }}$ |  | 1.9 | 2.0 | 2.1 | V |
| Vuvloz | UVLO Released Voltage | $\mathrm{V}_{\text {IN }}=\mathrm{V}_{\text {CE }}$ |  | 2.0 | 2.1 | 2.2 | V |
| T TSD | Thermal Shutdown Temperature | Junction Temperature |  |  | 140 |  | ${ }^{\circ} \mathrm{C}$ |
| TTSR | Thermal Shutdown Released Temperature | Junction Temperature |  |  | 100 |  | ${ }^{\circ} \mathrm{C}$ |

All test items listed under ELECTRICAL CHARACTERISTICS are done under the pulse load condition ( $\mathrm{Tj} \approx \mathrm{Ta}=25^{\circ} \mathrm{C}$ ) except Output Voltage Temperature Coefficient.
(1) RP508Kxx1A only
${ }^{(2)}$ RP508Kxx1B only

## THEORY OF OPERATION

## Fast Frequency and Fast Response



* Ripple is added and easy to detect and stabilize the system.

There are the following advantages when it operates at fast frequency ( 6 MHz ).

- Inductance value can be reduced.
- The fluctuation of energy in one cycle is fast and small, as a result, the capacitance value of Cout can be also reduced.
- Small LC value reduced the feedback delay, then response frequency band can be wide and transient response is much improved compared with conventional line-up.


## Maximum Frequency ( 6 MHz ) Lock



* The frequency goes faster and faster without this.


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Switching frequency in order to become reference frequency ( 6 MHz ), delay time is included the output voltage feedback loop and locked the frequency ( 6 MHz ).

## Frequency Control for Minimum On/Off Time

Minimum on/off time/Minimum off time is set. (But $100 \%$ duty is available.) In the 6 MHz , based on the calculation of input/ output relation, on/off time can be calculated, and if it is not satisfy the minimum on time / minimum off time, the reference frequency must be reduced and switching frequency is reduced.

## (Ex.) Min On Time (40 ns)

(1) $\mathrm{V}_{\text {IN }}=3.6 \mathrm{~V}$ Vout $=1.0 \mathrm{~V}$
$1 / 6 \mathrm{MHz} \times 1.0 \mathrm{~V} / 3.6 \mathrm{~V} \approx 46 \mathrm{~ns}>\operatorname{Min}$ On Time (= 40 ns )
$\rightarrow 6 \mathrm{MHz}$ Switching OK
(2) $\mathrm{V}_{\text {IN }}=5.5 \mathrm{~V}$ Vout $=1.0 \mathrm{~V}$
$1 / 6 \mathrm{MHz} \times 1.0 \mathrm{~V} / 5.5 \mathrm{~V} \approx 30 \mathrm{~ns}<\operatorname{Min}$ On Time ( $=40 \mathrm{~ns}$ )
$\rightarrow$ It must be slow down from 6 MHz

LX Waveform


Cycle time becomes long in order to satisfy Min. on time. It is suitable with keeping the duty.

## (Ex.) Min Off Time (40 ns)

(1) $\mathrm{V}_{\text {IN }}=5.0 \mathrm{~V}$ Vout $=3.3 \mathrm{~V}$
$1 / 6 \mathrm{MHz} \times(1-3.3 \mathrm{~V} / 5.0 \mathrm{~V}) \approx 57 \mathrm{~ns}>$ Min Off Time $(=$ 40 ns )
$\rightarrow 6 \mathrm{MHz}$ Switching OK
(2) $\mathrm{V}_{\text {IN }}=4.2 \mathrm{~V}$ Vout $=3.3 \mathrm{~V}$
$1 / 6 \mathrm{MHz} \times(1-3.3 \mathrm{~V} / 4.2 \mathrm{~V}) \approx 36 \mathrm{~ns}<\operatorname{Min}$ Off Time $(=$ $40 \mathrm{~ns})$
$\rightarrow$ It must be slow down from 6 MHz

LX Waveform


Cycle time becomes long in order to satisfy Min. off time. It is suitable with keeping the duty.

## Operation of Step-Down DCIDC Converter and Output Current

The step-down DC/DC converter charges energy in the inductor when $L_{x}$ Tr. turns "ON", and discharges the energy from the inductor when $\mathrm{Lx} \operatorname{Tr}$. turns "OFF" and operates with less energy loss, so that a lower output voltage ( $\mathrm{V}_{\text {out }}$ ) than the input voltage ( $\mathrm{V}_{\text {IN }}$ ) can be obtained.
The operation of the step-down DC/DC converter is explained in the following figures.


Figure 1. Basic Circuit


Figure 2. Inductor Current ( $\mathrm{I}_{\mathrm{L}}$ ) flowing through Inductor

Step1. P-channel Tr. turns "ON" and the inductor current ( $\mathrm{IL}=\mathrm{i} 1$ ) flows, L is charged with energy. At this moment, i1 increases from the minimum inductor current (lımin), which is 0 A , and reaches the maximum inductor current (lıMAX) in proportion to the on-time period (ton) of P-channel Tr.
Step2. When P-channel Tr. turns "OFF", L tries to maintain $I_{L}$ at $l_{\text {Lmax, }}$ so $L$ turns $N$-channel Tr. "ON" and the inductor current ( $\mathrm{l}=\mathrm{i} 2$ ) flows into L .
Step3. i2 decreases gradually and reaches Ilmin after the open-time period (topen) of N -channel Tr., and then N -channel Tr. turns "OFF". This is called discontinuous current mode.
As the output current (lout) increases, the off-time period (toff) of P-channel Tr. runs out before IL reaches ILmin. The next cycle starts, and P-channel Tr. turns "ON" and N-channel Tr. turns "OFF", which means IL starts increasing from ILmin. This is called continuous current mode.

In the case of PWM mode, Vout is maintained by controlling ton. During the PWM mode, the oscillator frequency (fosc) is constantly maintained.

As shown in Figure 2., when the step-down DC/DC operation is constant, Ilmin and Ilmax during ton of P-channel Tr . is same as the P -channel Tr. during toff.

The current differential between $\mathrm{I}_{\mathrm{Lmax}}$ and $\mathrm{I}_{\text {Lmin }}$ is described as $\Delta \mathrm{I}$.

However,
$\mathrm{T}=1 / \mathrm{fosc}=$ ton + toff
Duty (\%) $=$ ton $/ \mathrm{T} \times 100=$ ton $\times$ fosc $\times 100$
topen $\leq$ toff
In Equation 1, "Vout $\times$ topen / L" shows the amount of current change in "OFF" state. Also, " $\left.\mathrm{V}_{\mathrm{IN}}-\mathrm{V}_{\text {out }}\right) \times$ ton / L" shows the amount of current change at "ON" state.

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## Discontinuous Mode and Continuous Mode

As illustrated in Figure 3. when lout is relatively small, topen < toff. In this case, the energy charged into L during ton will be completely discharged during toff, as a result, ILMIN $=0$. This is called discontinuous mode. When lout is gradually increased, eventually topen = toff and when lout is increased further, eventually llmin > 0 . This is called continuous mode.


Figure 3. Discontinuous Mode


Figure 4. Continuous Mode

In the continuous mode, the solution of Equation 1 is described as tonc.
$\qquad$
tonc $=T \times V_{\text {out }} / V_{\text {IN }}$

When ton < tonc, it indicates discontinuous mode, and when ton $\geq$ tonc, it indicates continuous mode.

## Forced PWM Mode

By setting the MODE pin to "H", the RP508K switches on/off at the fixed frequency to reduce noise even under the light load. When IOUT is $\Delta I L / 2$ or less, ILMIN becomes less than 0 . That is, the accumulated electricity in CL is discharged through the IC side at IL increase period from ILMIN to "O" during ton and at IL decrease period from " 0 " to ILMIN during toff.


## Forced PWM Mode

## VFM MODE

By setting the MODE pin to " L ", in low output current, the IC automatically switches into VFM mode in order to achieve high efficiency. In VFM mode, a value of ton is determined by VIN and VOUT.


VFM Mode

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## Timing Chart

## 1. Soft-Start Time

## Starting-up with CE Pin

The IC starts to operate when the CE pin voltage ( $\mathrm{V}_{\mathrm{CE}}$ ) exceeds the threshold voltage. The threshold voltage is preset between CE " H " input voltage ( V сен ) and CE "L" input voltage ( $\mathrm{V}_{\text {CEL }}$ ).
After the start-up of the IC, soft-start circuit starts to operate. Then, after a certain period of time, the reference voltage ( $V_{R E F}$ ) in the IC gradually increases up to the specified value.


Soft-start time starts when soft-start circuit is activated, and ends when the reference voltage reaches the specified voltage. Soft start time is not always equal to the turn-on speed of the step-down DC/DC converter. Note that the turn-on speed could be affected by the power supply capacity, the output current, the inductance value and the Cout value.

## Starting-up with Power Supply

After the power-on, when $\mathrm{V}_{\text {IN }}$ exceeds the UVLO released voltage (VuvLoz), the IC starts to operate. Then, softstart circuit starts to operate and after a certain period of time, $V_{\text {Ref }}$ gradually increases up to the specified value. Soft-start time starts when soft-start circuit is activated, and ends when $V_{\text {REF }}$ reaches the specified voltage.


Note that the turn-on speed of Vout could be affected by the power supply capacity, the output current, the inductance value, the Cout value and the turn-on speed of $\mathrm{V}_{\mathrm{IN}}$ determined by $\mathrm{C}_{\text {IN }}$.

## 2. Under Voltage Lockout (UVLO) Circuit

If Vin becomes lower than VSET, the step-down DC/DC converter stops the switching operation and ON duty becomes $100 \%$, and then Vout gradually drops according to Vin.
If the VIN becomes lower than the UVLO detector threshold (VuvLoi), the UVLO circuit starts to operate, Vref stops, and P-channel and N-channel built-in switch transistors turn "OFF". As a result, Vout drops according to the Cout capacitance value and the load.
To restart the operation, Vin needs to be higher than Vuvloz. The timing chart below shows the voltage shifts of $V_{\text {REF }}, V_{L x}$ and $V_{\text {out }}$ when $V_{\text {IN }}$ value is varied.


Falling edge (operating) and rising edge (releasing) waveforms of Vout could be affected by the initial voltage of Cout and the output current of Vout.

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## 3. Over Current Protection Circuit

Over current protection circuit supervises the inductor peak current (the peak current flowing through Pchannel Tr.) in each switching cycle. If the current exceeds the Lx current limit (ILxlim) of 1100 mA (Typ.), Pchannel Tr . is turned off.

Ilxııм could be easily affected by self-heating or ambient environment. If the $\mathrm{V}_{\mathrm{in}}$ drops dramatically or becomes unstable due to short-circuit, protection operation could be affected.


## APPLICATION INFORMATION

## Typical Application



RP508K Typical Application

Recommended Components

| Symbol | Size | Type | Manufacturer |
| :---: | :---: | :---: | :---: |
| CIN | $2.2 \mu \mathrm{~F}$ | Ceramic | C1005JB0J225K (TDK) |
|  | $4.7 \mu \mathrm{~F}$ | Ceramic | C1005JB0J475K (TDK) |
| Cout | $4.7 \mu \mathrm{~F}$ | Ceramic | C1005JB0J475K (TDK) |
| L | $0.47 \mu \mathrm{H}(0.5 \mu \mathrm{H})$ | Inductor | MIPSZ2012D0R5 (FDK) |
|  |  |  | MDT1608CHR47N (TOKO) |
|  | $1.0 \mu \mathrm{H}$ | Inductor | MIPSZ2012D1R0 (FDK) |
|  |  |  | MDT1608CH1R0N (TOKO) |

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## Cautions in Selecting External Components

- Ensure the $\mathrm{V}_{\mathrm{IN}}$ and GND lines are sufficiently robust. A large switching current flows through the GND lines, the VDD line, the Vout line, an inductor, and Lx. If their impedance is too high, noise pickup or unstable operation may result. Set the external components as close as possible to the IC and minimize the wiring between the components and the IC, especially between a capacitor ( $\mathrm{C}_{\mathrm{IN}}$ ) and the VIN pin. The wiring between $V_{\text {оut }}$ and load and between $L$ and $V_{\text {оut s should be separated. }}$
- Choose a low ESR ceramic capacitor. The capacitance of $\mathrm{C}_{\mathrm{I}}$ should be more than or equal to $2.2 \mu \mathrm{~F}$. The capacitance of a capacitor (Cout) should be between $4.7 \mu \mathrm{~F}$ to $10 \mu \mathrm{~F}$.
- The Inductance value should be set within the range of $0.47 \mu \mathrm{H}$ to $1.0 \mu \mathrm{H}$. However, the inductance value is limited by output voltage. Refer to the table below. The phase compensation of this IC is designed according to the Cout and $L$ values. Choose an inductor that has small DC resistance, has enough allowable current and is hard to cause magnetic saturation. If the inductance value of an inductor is extremely small, the peak current of $L x$ may increase. The increased $L x$ peak current reaches " $L x$ limit current" to trigger over current protection circuit even if the load current is less than 600 mA .

Set Output Voltage Range vs. Inductance Range

| Set Output Voltage (V) | Input Voltage (V) | Inductance |  |
| :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\text {SET }}$ | $V_{\text {IN }}$ | $\mathrm{L}=0.47 \mu \mathrm{H}$ | $L=1.0 \mu \mathrm{H}$ |
| 0.8 to 1.2 | up to 5.5 | Recommended | Acceptable |
| 1.3 to 1.5 | up to 4.5 | Recommended | Acceptable |
|  | 4.5 to 5.5 | Acceptable | Recommended |
| 1.6 to 2.6 | up to 3.6 | Recommended | Acceptable |
|  | up to 4.5 | Acceptable | Recommended |
|  | 4.5 to 5.5 | - | Recommended |
| 2.7 to 3.3 | up to 4.5 | Recommended | Acceptable |
|  | 4.5 to 5.5 | - | Recommended |

- Over current protection circuit may be affected by self-heating or power dissipation environment.
- The performance of power source circuits using this IC largely depends on the peripheral circuits. When selecting the peripheral components, consider the conditions of use. Do not allow each component, PCB pattern and the IC to exceed their respected rated values (voltage, current and power) when designing the peripheral circuits.


## Output Current and Selection of External Components

The following equations explain the relationship between output current and peripheral components used in the diagrams in TYPICAL APPLICATIONS.

Ripple Current P-P value is described as $I_{R P}$, ON resistance of P-channel Tr. is described as Ronp, ON resistance of N -channel Tr . is described as Ronn, and DC resistor of the inductor is described as RL.

First, when P-channel Tr. Is "ON", the following equation is satisfied.

$$
V_{I N}=V_{\text {OUT }}+\left(R_{\text {ONP }}+R_{L}\right) \times \text { lout }+L \times I_{R P} / \text { ton } .
$$

Equation 3

Second, when P-channel Tr. is "OFF" (N-channel Tr. Is "ON"), the following equation is satisfied.
$\mathrm{L} \times \mathrm{I}_{\mathrm{RP}} /$ toff $=\mathrm{R}_{\text {ONN }} \times$ lout $+\mathrm{V}_{\text {OUT }}+\mathrm{R}_{\mathrm{L}} \times$ lout
Equation 4

Put Equation 4 into Equation 3 to solve ON duty of P-channel Tr. (Don $=$ ton / (toff + ton $)$ ):

$$
\text { Don }=(\text { Vout }+ \text { Ronn } \times \text { lout }+ \text { RL } \times \text { lout }) /(\text { Vin }+ \text { Ronn } \times \text { lout }- \text { Ronp } \times \text { lout }) \ldots \ldots . . . . . . . . . \text { Equation } 5
$$

Ripple Current is described as follows:

$$
I_{\text {RP }}=\left(V_{\text {IN }}-V_{\text {OUT }}-R_{\text {ONP }} \times \text { lout }-R_{\mathrm{L}} \times \text { Iout }\right) \times \text { DoN } / \text { fosc } / L
$$

Peak current that flows through $L$, and $L \times \operatorname{Tr}$. is described as follows:

$$
I_{\text {LXMAX }}=\mathrm{I}_{\mathrm{OUT}}+\mathrm{I}_{\mathrm{RP}} / 2
$$

Consider Ilxmax when setting conditions of input and output, as well as selecting the external components. The above calculation formulas are based on the ideal operation of the Ics in continuous mode.

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## TECHNICAL NOTES

The performance of power source circuits using this IC largely depends on the peripheral circuits. When selecting the peripheral components, consider the conditions of use. Do not allow each component, PCB pattern and the IC to exceed their respected rated values (voltage, current and power) when designing the peripheral circuits.

- Ensure the $\mathrm{V}_{\mathrm{IN}}$ and GND lines are sufficiently robust. A large switching current flows through the GND lines, the $V_{D D}$ line, the Vout line, an inductor, and $L_{x}$. If their impedance is too high, noise pickup or unstable operation may result. Set the external components as close as possible to the IC and minimize the wiring between the components and the IC, especially between a capacitor ( $\mathrm{C}_{\mathrm{I}}$ ) and the VIn pin. The



## Reference PCB Layout



## TYPICAL CHARACTERISTICS

Note: Typical Characteristics are intended to be used as reference data; they are not guaranteed. 01) Output Voltage vs. Output Current

RP508K081x, Vout = 0.8 V
MODE = "L" PWM/VFM auto switching control


RP508K101x, Vout $=1.0 \mathrm{~V}$
MODE = "L" PWM/VFM auto switching control


RP508K121x, Vout $=1.2 \mathrm{~V}$
MODE = "L" PWM/VFM auto switching control


RP508K081x, Vout $=0.8 \mathrm{~V}$
MODE = "H" forced PWM control


RP508K101x, Vout $=1.0 \mathrm{~V}$
MODE = "H" forced PWM control


RP508K121x, Vout $=1.2 \mathrm{~V}$
MODE = "H" forced PWM control


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RP508K181x, Vout $=1.8 \mathrm{~V}$
MODE = "L" PWM/VFM auto switching control


RP508K331x, Vout $=3.3 \mathrm{~V}$
MODE = "L" PWM/VFM auto switching control

02) Output Voltage vs. Input Voltage

RP508K081x, Vout $=0.8 \mathrm{~V}$
MODE = "H" forced PWM control


RP508K181x, $\mathrm{V}_{\text {оut }}=1.8 \mathrm{~V}$
MODE = " H " forced PWM control


RP508K331x, Vout $=3.3 \mathrm{~V}$
MODE = "H" forced PWM control


RP508K101x, Vout $=1.0 \mathrm{~V}$
MODE = "H" forced PWM control


RP508K121x, Vout $=1.2 \mathrm{~V}$
MODE = "H" forced PWM control


RP508K331x, Vout $=3.3 \mathrm{~V}$
MODE = "H" forced PWM control

03) Output Voltage vs. Temperature


RP508K181x, Vout $=1.8 \mathrm{~V}$
MODE $=$ " H " forced PWM control


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## 04) Efficiency vs. Output Current

RP508K081x, Vout $=0.8 \mathrm{~V}$
L = MIPSZ2012D0R5 (2012size_0.5 $\mu \mathrm{H}$ )


RP508K121x, Vout $=1.2 \mathrm{~V}$
L = MIPSZ2012D0R5 (2012size_0.5 $\mu \mathrm{H}$ )


RP508K331x, Vout $=3.3 \mathrm{~V}$
L = MIPSZ2012D1R0 (2012size_1.0 $\mu \mathrm{H}$ )


RP508K101x, Vout $=1.0 \mathrm{~V}$
L = MIPSZ2012D0R5 (2012size_0.5 $\mu \mathrm{H}$ )


RP508K181x, Vout $=1.8 \mathrm{~V}$
L = MIPSZ2012D0R5 (2012size_0.5 $\mu \mathrm{H}$ )


RP508K081x, Vout $=0.8 \mathrm{~V}$
L = MDT1608CHR47N (1608size_0.47 $\mu \mathrm{H}$ )


RP508K121x, Vout $=1.2 \mathrm{~V}$
L = MDT1608CHR47N (1608size_0.47 $\mu \mathrm{H}$ )


RP508K331x, Vоut $=3.3 \mathrm{~V}$
L = MDT1608CH1R0N (1608size_1.0 $\mu \mathrm{H}$ )


Output Current $\mathrm{I}_{\text {Out }}(\mathrm{mA})$

RP508K101x, Vout $=1.0 \mathrm{~V}$
L = MDT1608CHR47N (1608size_0.47 $\mu \mathrm{H}$ )


RP508K181x, Vout $=1.8 \mathrm{~V}$
L = MDT1608CHR47N (1608size_0.47 $\mu \mathrm{H}$ )

05) Supply Current vs. Temperature RP508K181x, Vout $=1.8 \mathrm{~V}\left(\mathrm{~V}_{\text {IN }}=5.5 \mathrm{~V}\right)$ MODE = "L" PWM/VFM auto switching control
$\mathrm{V} \mathrm{in}_{\mathrm{n}}=5.5 \mathrm{~V}$


## 07) Output Voltage Waveform

RP508K081x, Vout $=0.8 \mathrm{~V}\left(\mathrm{~V}_{\text {in }}=3.6 \mathrm{~V}\right)$
MODE $=$ "L" PWM/VFM auto switching control


RP508K121x, Vout $=1.2 \mathrm{~V}(\mathrm{~V}$ IN $=3.6 \mathrm{~V})$
MODE = "L" PWM/VFM auto switching control

06) Supply Current vs. Input Voltage RP508K181x, Vout $=1.8 \mathrm{~V}$
MODE = "L" PWM/VFM auto switching control


RP508K081x, $\mathrm{V}_{\text {OUt }}=0.8 \mathrm{~V}\left(\mathrm{~V}_{\text {IN }}=3.6 \mathrm{~V}\right)$ MODE = " H " forced PWM control


RP508K121x, Vout $=1.2 \mathrm{~V}\left(\mathrm{~V}_{\text {in }}=3.6 \mathrm{~V}\right)$ MODE = H" forced PWM control


RP508K181x, $\mathrm{V}_{\text {out }}=1.8 \mathrm{~V}\left(\mathrm{~V}_{\text {IN }}=3.6 \mathrm{~V}\right)$ MODE $=$ "L" PWM/VFM auto switching control

RP508K181x, $\mathrm{V}_{\text {out }}=1.8 \mathrm{~V}\left(\mathrm{~V}_{\text {IN }}=3.6 \mathrm{~V}\right)$ MODE $=$ " H " forced PWM control

RP508K331x, Vout $=3.3 \mathrm{~V}\left(\mathrm{~V}_{\text {In }}=4.3 \mathrm{~V}\right)$
MODE = "H" forced PWM control


## 08) Frequency vs. Input Voltage

RP508K181x, Vout $=1.8 \mathrm{~V}$
MODE = " H " forced PWM control


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09) Frequency vs. Input Voltage with Various Output Currents

RP508K121x, Vout = 1.2 V
MODE $=$ " $H$ " forced $P W M$ control

10) VFM Frequency vs. Output Current

RP508K121x, Vout $=1.2 \mathrm{~V}$
MODE = "L" PWM/VFM auto switching control

11) Soft-start Time vs. Temperature


RP508K181x, Vout $=1.8 \mathrm{~V}$
MODE $=$ " H " forced PWM control


RP508K181x, Vout $=1.8 \mathrm{~V}$
MODE = "L" PWM/VFM auto switching control


## 12) UVLO Detector Threshold/ Released Voltage vs. Temperature

UVLO Detector Threshold

13) CE Input Voltage vs. Temperature
$\mathrm{CE}=$ " H " Input Voltage $\left(\mathrm{V}_{\mathrm{IN}}=5.5 \mathrm{~V}\right)$

14) $L_{x}$ Current Limit vs. Temperature


UVLO Release Voltage


CE = "H" Input Voltage (Vin = 2.3 V)

15) Standby Current vs. Temperature


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16) Nch Transistor On Resistance vs. Temperature
17) Pch Transistor On Resistance vs. Temperature


18) Load Transient Response (Cout $=4.7 \mu \mathrm{~F}, \mathrm{C} 1005 \mathrm{X} 5 \mathrm{R0J475M}$ )

RP508K081x (Vin $=3.6 \mathrm{~V}$, Vout $=0.8 \mathrm{~V}$ )
L = MIPSZ2012D0R5 (2012size_0.5 $\mu \mathrm{H}$ )
MODE $=$ " H " forced PWM control


RP508K081x (VIN $=3.6 \mathrm{~V}$, $\mathrm{V}_{\text {out }}=0.8 \mathrm{~V}$ )
L = MIPSZ2012D0R5 (2012size_0.5 $\mu \mathrm{H}$ )
MODE = "H" forced PWM control


RP508K081x (Vin $=3.6 \mathrm{~V}$, Vout $=0.8 \mathrm{~V})$ L = MIPSZ2012DOR5 (2012size_0.5 $\mu \mathrm{H}$ ) MODE $=$ " ${ }^{H}$ " forced $P W M$ control


RP508K081x (VIN $=3.6 \mathrm{~V}$, $\mathrm{V}_{\text {out }}=0.8 \mathrm{~V}$ ) L = MIPSZ2012D0R5 (2012size_0.5 $\mu \mathrm{H}$ ) MODE $=$ " ${ }^{H}$ " forced $P W M$ control


RP508K121x ( $\mathrm{V}_{\text {in }}=3.6 \mathrm{~V}$, $\mathrm{V}_{\text {out }}=1.2 \mathrm{~V}$ ) L = MIPSZ2012D0R5 (2012size $0.5 \mu \mathrm{H}$ ) MODE = "H" forced PWM control


RP508K121x ( $\mathrm{V}_{\mathrm{IN}}=3.6 \mathrm{~V}$, $\mathrm{V}_{\text {out }}=1.2 \mathrm{~V}$ ) L = MIPSZ2012D0R5 (2012size_0.5 $\mu \mathrm{H}$ ) MODE = "H" forced PWM control


RP508K181x ( $\mathrm{V}_{\text {IN }}=3.6 \mathrm{~V}$, $\left.\mathrm{V}_{\text {Out }}=1.8 \mathrm{~V}\right)$ L = MIPSZ2012D0R5 (2012size_0.5 $\mu \mathrm{H}$ ) MODE = "H" forced PWM control


RP508K121x ( $\mathrm{V}_{\text {IN }}=3.6 \mathrm{~V}$, $\mathrm{V}_{\text {out }}=1.2 \mathrm{~V}$ )
L = MIPSZ2012D0R5 (2012size_0.5 $\mu \mathrm{H}$ )
MODE = "H" forced PWM control


RP508K121x ( $\mathrm{V}_{\text {IN }}=3.6 \mathrm{~V}$, Vout $=1.2 \mathrm{~V}$ ) L = MIPSZ2012D0R5 (2012size_0.5 $\mu \mathrm{H}$ ) MODE = "H" forced PWM control


RP508K181x ( $\mathrm{V}_{\text {IN }}=3.6 \mathrm{~V}$, $\mathrm{V}_{\text {out }}=1.8 \mathrm{~V}$ ) L = MIPSZ2012D0R5 (2012size_0.5 $\mu \mathrm{H}$ ) MODE = "H" forced PWM control


## RP508K

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RP508K181x ( $\mathrm{V}_{\text {IN }}=3.6 \mathrm{~V}$, Vout $=1.8 \mathrm{~V}$ ) L = MIPSZ2012D0R5 (2012size_0.5 $\mu \mathrm{H}$ )
MODE = "H" forced PWM control


RP508K331x ( $\mathrm{V}_{\text {IN }}=5.0 \mathrm{~V}$, Vout $=3.3 \mathrm{~V}$ ) L = MIPSZ2012D1R0 (2012size_1.0 $\mu \mathrm{H}$ ) MODE = "H" forced PWM control


RP508K331x ( $\mathrm{V}_{\text {IN }}=5.0 \mathrm{~V}$, $\left.\mathrm{V}_{\text {out }}=3.3 \mathrm{~V}\right)$ L = MIPSZ2012D1R0 (2012size_1.0 $\mu \mathrm{H}$ ) MODE = "H" forced PWM control


RP508K181x ( $\mathrm{V}_{\text {IN }}=3.6 \mathrm{~V}$, $\left.\mathrm{V}_{\text {Out }}=1.8 \mathrm{~V}\right)$ L = MIPSZ2012D0R5 (2012size_0.5 $\mu \mathrm{H}$ )
MODE $=$ " $\mathrm{H}^{\prime}$ forced PWM control


RP508K331x ( $\mathrm{V}_{\text {IN }}=5.0 \mathrm{~V}$, $\mathrm{V}_{\text {out }}=3.3 \mathrm{~V}$ )
L = MIPSZ2012D1R0 (2012size_1.0 $\mu \mathrm{H}$ )
MODE = "H" forced PWM control


RP508K331x ( $\mathrm{V}_{\text {IN }}=5.0 \mathrm{~V}$, $\mathrm{V}_{\text {out }}=3.3 \mathrm{~V}$ )
L = MIPSZ2012D1R0 (2012size_1.0 $\mu \mathrm{H}$ )
MODE = "H" forced PWM control


Load Transient Response ( $\mathrm{C}_{\text {out }}=4.7 \mu \mathrm{~F}, \mathrm{C} 1005 \mathrm{X} 5 \mathrm{R0J475M}$ )
RP508K081x ( $\mathrm{V}_{\text {IN }}=3.6 \mathrm{~V}$, Vоut $=0.8 \mathrm{~V}$ )
L = MIPSZ2012D0R5 (2012size_0.5 $\mu \mathrm{H}$ )
MODE = "L" PWM/VFM auto switching control


RP508K121x (Vin = 3.6 V, Vout $=1.2 \mathrm{~V}$ )
L = MIPSZ2012DOR5 (2012size_0.5 $\mu \mathrm{H}$ )
MODE = "L" PWM/VFM auto switching control


RP508K181x (VIN $=3.6 \mathrm{~V}$, Vout $=1.8 \mathrm{~V}$ ) L = MIPSZ2012D0R5 (2012size_0.5 $\mu \mathrm{H}$ )
MODE = "L" PWM/VFM auto switching control


RP508K081x (VIN $=3.6 \mathrm{~V}$, Vout $=0.8 \mathrm{~V})$
L = MIPSZ2012D0R5 (2012size_0.5 $\mu \mathrm{H}$ )
MODE = "L" PWM/VFM auto switching control


RP508K121x ( V in $=3.6 \mathrm{~V}$, Vout $=1.2 \mathrm{~V}$ )
L = MIPSZ2012D0R5 (2012size_0.5 $\mu \mathrm{H}$ )
MODE = "L" PWM/VFM auto switching control


RP508K181x ( V In $=3.6 \mathrm{~V}$, Vout $=1.8 \mathrm{~V}$ )
L = MIPSZ2012D0R5 (2012size_0.5 $\mu \mathrm{H}$ )
MODE = "L" PWM/VFM auto switching control


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RP508K331x (VIN $=5.0 \mathrm{~V}$, Vout $=3.3 \mathrm{~V})$
L = MIPSZ2012D1R0 (2012size_1.0 $\mu \mathrm{H}$ )
MODE = "L" PWM/VFM auto switching control

RP508K331x (VIN $=5.0 \mathrm{~V}$, Vоut $=3.3 \mathrm{~V}$ )
L = MIPSZ2012D1R0 (2012size_1.0 $\mu \mathrm{H}$ )
MODE = "L" PWM/VFM auto switching control



Load Transient Response (Cout $=4.7 \mu \mathrm{~F}$, C1005X5R0J475M)

RP508K081x ( $\mathrm{V}_{\text {IN }}=3.6 \mathrm{~V}$, Vout $=0.8 \mathrm{~V}$ )
L = MDT1608CHR47N (1608size_0.47 $\mu \mathrm{H}$ )
MODE = "H" forced PWM control


RP508K081x ( $\mathrm{V}_{\text {IN }}=3.6 \mathrm{~V}$, $\mathrm{V}_{\text {Out }}=0.8 \mathrm{~V}$ )
L = MDT1608CHR47N (1608size_0.47 $\mu \mathrm{H}$ ) MODE = "H" forced PWM control


RP508K081x ( $\mathrm{V}_{\text {IN }}=3.6 \mathrm{~V}$, $\mathrm{V}_{\text {out }}=0.8 \mathrm{~V}$ )
L = MDT1608CHR47N (1608size_0.47 $\mu \mathrm{H}$ )
MODE = "H" forced PWM control


RP508K081x ( $\mathrm{V}_{\text {IN }}=3.6 \mathrm{~V}$, $\mathrm{V}_{\text {out }}=0.8 \mathrm{~V}$ )
L = MDT1608CHR47N (1608size_0.47 $\mu \mathrm{H}$ )
MODE = "H" forced PWM control


RP508K121x (Vin $=3.6 \mathrm{~V}$, $\mathrm{V}_{\text {out }}=1.2 \mathrm{~V}$ ) L = MDT1608CHR47N (1608size_0.47 $\mu \mathrm{H}$ ) MODE = " H " forced PWM control


RP508K121x ( $\mathrm{V}_{\text {IN }}=3.6 \mathrm{~V}$, $\mathrm{V}_{\text {OUt }}=1.2 \mathrm{~V}$ ) L = MDT1608CHR47N (1608size_0.47 $\mu \mathrm{H}$ ) MODE = "H" forced PWM control


RP508K181x ( $\mathrm{V}_{\text {IN }}=3.6 \mathrm{~V}$, $\mathrm{V}_{\text {OUT }}=1.8 \mathrm{~V}$ )
L = MDT1608CHR47N (1608size_0.47 $\mu \mathrm{H}$ )
MODE = "H" forced PWM control


RP508K121x ( $\mathrm{V}_{\text {IN }}=3.6 \mathrm{~V}$, Vоut $=1.2 \mathrm{~V}$ )
L = MDT1608CHR47N (1608size_0.47 $\mu \mathrm{H}$ )
MODE $=$ " H " forced PWM control


RP508K121x ( $\mathrm{V}_{\mathrm{IN}}=3.6 \mathrm{~V}$, $\mathrm{V}_{\text {out }}=1.2 \mathrm{~V}$ )
L = MDT1608CHR47N (1608size_0.47 $\mu \mathrm{H}$ )
MODE = "H" forced PWM control


RP508K181x ( $\mathrm{V}_{\text {IN }}=3.6 \mathrm{~V}$, $\mathrm{V}_{\text {OUT }}=1.8 \mathrm{~V}$ )
L = MDT1608CHR47N (1608size_0.47 $\mu \mathrm{H}$ )
MODE = "H" forced PWM control


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RP508K181x ( $\mathrm{V}_{\text {IN }}=3.6 \mathrm{~V}$, Vout $=1.8 \mathrm{~V}$ )
L = MDT1608CHR47N (1608size_0.47 $\mu \mathrm{H}$ )
MODE = " H " forced PWM control


RP508K331x ( $\mathrm{V}_{\text {IN }}=5.0 \mathrm{~V}$, $\left.\mathrm{V}_{\text {out }}=3.3 \mathrm{~V}\right)$ L = MDT1608CH1R0N(1608size_1.0 $\mu \mathrm{H}$ ) MODE = "H" forced PWM control


RP508K331x ( $\mathrm{V}_{\text {IN }}=5.0 \mathrm{~V}$, Vout $=3.3 \mathrm{~V}$ ) L = MDT1608CH1R0N (1608size_1.0 $\mu \mathrm{H}$ ) MODE = "H" forced PWM control


RP508K181x (Vin $=3.6 \mathrm{~V}$, $\mathrm{V}_{\text {оut }}=1.8 \mathrm{~V}$ )
L = MDT1608CHR47N (1608size_0.47 $\mu \mathrm{H}$ )
MODE $=$ " H " forced PWM control


RP508K331x ( $\mathrm{V}_{\text {IN }}=5.0 \mathrm{~V}$, $\left.\mathrm{V}_{\text {Out }}=3.3 \mathrm{~V}\right)$ L = MDT1608CH1R0N (1608size_1.0 $\mu \mathrm{H}$ )
MODE = "H" forced PWM control


RP508K331x ( $\mathrm{V}_{\text {IN }}=5.0 \mathrm{~V}$, $\left.\mathrm{V}_{\text {Out }}=3.3 \mathrm{~V}\right)$ L = MDT1608CH1R0N (1608size_1.0 $\mu \mathrm{H}$ ) MODE = "H" forced PWM control


Load Transient Response ( $\mathrm{C}_{\text {out }}=4.7 \mu \mathrm{~F}, \mathrm{C} 1005 \mathrm{X} 5 \mathrm{R0J475M}$ )

RP508K081x (VIN $=3.6 \mathrm{~V}$, Vout $=0.8 \mathrm{~V}$ )
L = MDT1608CHR47N (1608size_0.47 $\mu \mathrm{H}$ )
MODE = "L" PWM/VFM auto switching control


RP508K121x (Vin = 3.6 V, Vоut $=1.2 \mathrm{~V}$ )
L = MDT1608CHR47N (1608size_0.47 $\mu \mathrm{H}$ )
MODE = "L" PWM/VFM auto switching control


RP508K181x (VIN $=3.6 \mathrm{~V}$, Vout $=1.8 \mathrm{~V}$ ) L = MDT1608CHR47N (1608size_0.47 $\mu \mathrm{H}$ ) MODE = "L" PWM/VFM auto switching control


RP508K081x ( $\mathrm{V}_{\text {IN }}=3.6 \mathrm{~V}$, $\mathrm{V}_{\text {out }}=0.8 \mathrm{~V}$ )
L = MDT1608CHR47N (1608size_0.47 $\mu \mathrm{H}$ )
MODE = "L" PWM/VFM auto switching control


RP508K121x ( $\mathrm{V}_{\text {in }}=3.6 \mathrm{~V}$, Vout $=1.2 \mathrm{~V}$ )
L = MDT1608CHR47N (1608size_0.47 $\mu \mathrm{H}$ )
MODE = "L" PWM/VFM auto switching control


RP508K181x (VIN $=3.6 \mathrm{~V}$, Vout $=1.8 \mathrm{~V}$ )
L = MDT1608CHR47N (1608size_0.47 $\mu \mathrm{H}$ )
MODE = "L" PWM/VFM auto switching control


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RP508K331x ( $\mathrm{V}_{\text {IN }}=5.0 \mathrm{~V}$, $\mathrm{V}_{\text {out }}=3.3 \mathrm{~V}$ )
L = MDT1608CH1R0N (1608size_1.0 $\mu \mathrm{H}$ )
MODE = "L" PWM/VFM auto switching control

19) Mode Switching Waveform

RP508K121x ( $\mathrm{V}_{\text {IN }}=3.6 \mathrm{~V}$, Vout $=1.2 \mathrm{~V}$, lout $\left.=1 \mathrm{~mA}\right)$ MODE = "L" $\rightarrow$ MODE = "H"


RP508K181x $\left(\mathrm{V}_{\mathrm{IN}}=3.6 \mathrm{~V}\right.$, $\mathrm{V}_{\text {OUt }}=1.8 \mathrm{~V}$, lout $\left.=1 \mathrm{~mA}\right)$ MODE = "L" $\rightarrow$ MODE = "H"


RP508K331x ( $\mathrm{V}_{\text {IN }}=5.0 \mathrm{~V}$, $\mathrm{V}_{\text {out }}=3.3 \mathrm{~V}$ )
L = MDT1608CH1R0N (1608size_1.0 $\mu \mathrm{H}$ )
MODE = "L" PWM/VFM auto switching control


RP508K121x $\left(\mathrm{V}_{\text {IN }}=3.6 \mathrm{~V}\right.$, $\mathrm{V}_{\text {OUt }}=1.2 \mathrm{~V}$, I IUT $\left.=1 \mathrm{~mA}\right)$ MODE = "H" $\rightarrow$ MODE = "L"


RP508K181x ( $\mathrm{V}_{\text {IN }}=3.6 \mathrm{~V}$, $\mathrm{V}_{\text {out }}=1.8 \mathrm{~V}$, lout $\left.=1 \mathrm{~mA}\right)$ MODE = "H" $\rightarrow$ MODE = "L"


The power dissipation of the package is dependent on PCB material, layout, and environmental conditions. The following conditions are used in this measurement.

Measurement Conditions

|  | JEDEC STD.51-7 Test Land Pattern |
| :---: | :---: |
| Environment | Mounting on Board (Wind Velocity $=0 \mathrm{~m} / \mathrm{s}$ ) |
| Board Material | Glass Cloth Epoxy Plastic (Four-Layer Board) |
| Board Dimensions | $76.2 \mathrm{~mm} \times 114.3 \mathrm{~mm} \times 1.6 \mathrm{~mm}$ |
| Copper Ratio | Outer Layers (First and Fourth Layers): Less than $10 \%$ of 60 mm Square <br> Inner Layers (Second and Third Layers): $100 \%$ of 74.2 mm Square |
| Through-holes | $\phi 0.85 \mathrm{~mm} \times 44 \mathrm{pcs}$ |

Measurement Result
$\left(\mathrm{Ta}=25^{\circ} \mathrm{C}, \mathrm{Tjmax}=125^{\circ} \mathrm{C}\right)$

|  | JEDEC STD.51-7 Test Land Pattern |
| :---: | :---: |
| Power Dissipation | 666 mW |
| Thermal Resistance | $\theta \mathrm{ja}=\left(125-25^{\circ} \mathrm{C}\right) / 0.666 \mathrm{~W}=150^{\circ} \mathrm{C} / \mathrm{W}$ |
|  | $\theta \mathrm{jc}=28^{\circ} \mathrm{C} / \mathrm{W}$ |



Power Dissipation vs. Ambient Temperature
IC Mount Area (mm)
Measurement Board Pattern


DFN(PLP)1212-6F Package Dimensions (Unit: mm)

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# Mouser Electronics 

Authorized Distributor

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## Ricoh Electronics:

> RP508K181A-TR RP508K101B-TR RP508K121A-TR RP508K181B-TR RP508K121B-TR RP508K331B-TR

RP508K241A-TR RP508K301B-TR RP508K281B-TR RP508K131B5-TR RP508K281A-TR RP508K321B-TR
RP508K141A-TR RP508K151B-TR RP508K191A-TR RP508K201B-TR RP508K211B5-TR RP508K331A-TR
RP508K221A-TR RP508K251A-TR RP508K251B-TR RP508K261A-TR RP508K301A-TR RP508K311B-TR
RP508K131B-TR RP508K191B-TR RP508K111B-TR


[^0]:    ${ }^{(1)}$ This is an approximate value. The output current is dependent on conditions and external components.

[^1]:    (1) Auto-discharge function quickly lowers the output voltage to 0 V , when the chip enable signal is switched from the active mode to the standby mode, by releasing the electrical charge accumulated in the external capacitor.
    (2) 0.05 V step is also available as a custom code.

[^2]:    ${ }^{(1)}$ Refer to POWER DISSIPATION for detailed information.

