## FEATURES

## Space-saving SC70 and SOT-23 packaging

Wide bandwidth: 8 MHz @ 5 V
Low offset voltage: 1.2 mV maximum
Rail-to-rail output swing
2.9 V/us slew rate

Unity gain stable
Single-supply operation: 2.7 V to 12 V

## APPLICATIONS

Portable communications
Microphone amplifiers
Portable phones
Sensor interface
Active filters
PCMCIA cards
ASIC input drivers
Wearable computers
Battery-powered devices
Voltage reference buffers
Personal digital assistants

## PIN CONFIGURATIONS



Figure 2. 5-Lead SC70 and SOT-23 (KS and RJ Suffixes)


Figure 3. 8-Lead SOIC and MSOP (R and RM Suffixes)

## GENERAL DESCRIPTION

The AD8519 and AD8529 are rail-to-rail output bipolar amplifiers with a unity gain bandwidth of 8 MHz and a typical voltage offset of less than 1 mV . The AD8519 brings precision and bandwidth to the SC70 and SOT-23 packages. The low supply current makes the AD8519/AD8529 ideal for batterypowered applications. The rail-to-rail output swing of the AD8519/AD8529 is larger than standard video op amps, making them useful in applications that require greater dynamic range than standard video op amps. The $2.9 \mathrm{~V} / \mu \mathrm{s}$ slew rate makes the AD8519/AD8529 a good match for driving ASIC inputs such as voice codecs.

The small SC70 package makes it possible to place the AD8519 next to sensors, reducing external noise pickup.

The AD8519/AD8529 is specified over the extended industrial $\left(-40^{\circ} \mathrm{C}\right.$ to $\left.+125^{\circ} \mathrm{C}\right)$ temperature range. The AD8519 is available in 5-lead SC70 and 5-lead SOT-23 packages, and an 8-lead SOIC surface-mount package. The AD8529 is available in 8 -lead SOIC and 8-lead MSOP packages.

Rev. D

## AD8519/AD8529

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## SPECIFICATIONS

## ELECTRICAL CHARACTERISTICS

$\mathrm{V}_{\mathrm{s}}=5.0 \mathrm{~V}, \mathrm{~V}-=0 \mathrm{~V}, \mathrm{~V}_{\mathrm{CM}}=2.5 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.
Table 1.

| Parameter | Symbol | Conditions | Min | Typ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| INPUT CHARACTERISTICS |  |  |  |  |  |  |
| Offset Voltage | Vos | AD8519AKS, AD8519ART |  | 600 | 1100 | $\mu \mathrm{V}$ |
|  |  | $-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C}$ |  | 800 | 1300 | $\mu \mathrm{V}$ |
|  |  | AD8519AR (R-8), AD8529 |  | 600 | 1000 | $\mu \mathrm{V}$ |
|  |  | $-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C}$ |  |  | 1100 | $\mu \mathrm{V}$ |
| Input Bias Current | $\mathrm{I}_{\mathrm{B}}$ |  |  |  | 300 | nA |
|  |  | $-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C}$ |  |  | 400 | nA |
| Input Offset Current | los |  |  |  | $\pm 50$ | nA |
|  |  | $-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C}$ |  |  | $\pm 100$ | nA |
| Input Voltage Range | Vcm |  | 0 |  | 4 | V |
| Common-Mode Rejection Ratio | CMRR | $0 \mathrm{~V} \leq \mathrm{V}_{\text {СМ }} \leq 4.0 \mathrm{~V},-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C}$ | 63 | 100 |  | dB |
| Large Signal Voltage Gain | Avo | $\mathrm{R}_{\mathrm{L}}=2 \mathrm{k} \Omega, 0.5 \mathrm{~V}<\mathrm{V}_{\text {out }}<4.5 \mathrm{~V}$ |  | 30 |  | $\mathrm{V} / \mathrm{mV}$ |
|  |  | $\mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega, 0.5 \mathrm{~V}<\mathrm{V}_{\text {Out }}<4.5 \mathrm{~V}$ | 50 | 100 |  | $\mathrm{V} / \mathrm{mV}$ |
|  |  | $\mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega,-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C}$ | 30 |  |  | $\mathrm{V} / \mathrm{mV}$ |
| Offset Voltage Drift | $\Delta \mathrm{V}_{\text {os }} / \Delta \mathrm{T}$ |  |  | 2 |  | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| Bias Current Drift | $\Delta l_{B} / \Delta T$ |  |  | 500 |  | $\mathrm{pA} /{ }^{\circ} \mathrm{C}$ |
| OUTPUT CHARACTERISTICS |  |  |  |  |  |  |
| Output Voltage Swing High | V ${ }_{\text {OH }}$ | $\mathrm{I}_{\mathrm{L}}=250 \mu \mathrm{~A}$ |  |  |  |  |
|  |  | $-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C}$ | 4.90 |  |  | V |
|  |  | $\mathrm{L}=5 \mathrm{~mA}$ | 4.80 |  |  | V |
| Output Voltage Swing Low | Vol | $\mathrm{L}_{\mathrm{L}}=250 \mu \mathrm{~A}$ |  |  |  |  |
|  |  | $-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C}$ |  |  | 80 | mV |
|  |  | $\mathrm{L}_{\mathrm{L}}=5 \mathrm{~mA}$ |  |  | 200 | mV |
| Short-Circuit Current | Isc | Short to ground, instantaneous |  | $\pm 70$ |  | mA |
| Maximum Output Current | lout |  |  | $\pm 25$ |  | mA |
| POWER SUPPLY |  |  |  |  |  |  |
| Power Supply Rejection Ratio | PSRR | $\mathrm{V}_{\mathrm{s}}=2.7 \mathrm{~V}$ to 7 V |  | 110 |  | dB |
|  |  | $-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C}$ |  | 80 |  | dB |
| Supply Current/Amplifier | l SY | $\mathrm{V}_{\text {OUT }}=2.5 \mathrm{~V}$ |  | 600 | 1200 | $\mu \mathrm{A}$ |
|  |  | $-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C}$ |  |  | 1400 |  |
| DYNAMIC PERFORMANCE |  |  |  |  |  |  |
| Slew Rate | SR | $1 \mathrm{~V}<\mathrm{V}_{\text {Out }}<4 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega$ |  | 2.9 |  | V/ $/ \mathrm{s}$ |
| Settling Time | $\mathrm{ts}_{5}$ | To 0.01\% |  | 1200 |  |  |
| Gain Bandwidth Product | GBP |  |  | 8 |  | MHz |
| Phase Margin | $\Phi_{\mathrm{m}}$ |  |  | 60 |  | Degrees |
| NOISE PERFORMANCE |  |  |  |  |  |  |
| Voltage Noise | $\mathrm{e}_{\mathrm{n}} \mathrm{p}$-p | 0.1 Hz to 10 Hz |  | 0.5 |  | $\mu \mathrm{V}$ p-p |
| Voltage Noise Density | $\mathrm{e}_{\mathrm{n}}$ | $\mathrm{f}=1 \mathrm{kHz}$ |  | 10 |  | $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ |
| Current Noise Density | $\mathrm{i}_{n}$ | $\mathrm{f}=1 \mathrm{kHz}$ |  | 0.4 |  | $\mathrm{pA} / \sqrt{ } \mathrm{Hz}$ |

## AD8519/AD8529

$\mathrm{V}_{\mathrm{S}}=3.0 \mathrm{~V}, \mathrm{~V}-=0 \mathrm{~V}, \mathrm{~V}_{\mathrm{CM}}=1.5 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.

Table 2.

$\mathrm{V}_{\mathrm{S}}=2.7 \mathrm{~V}, \mathrm{~V}-=0 \mathrm{~V}, \mathrm{~V}_{\mathrm{CM}}=1.35 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.

Table 3.

| Parameter | Symbol | Conditions | Min | Typ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| INPUT CHARACTERISTICS <br> Offset Voltage <br> Input Bias Current <br> Input Offset Current <br> Input Voltage Range <br> Common-Mode Rejection Ratio Large Signal Voltage Gain | Vos <br> $I_{B}$ <br> los <br> Vcm <br> CMRR <br> Avo | AD8519AKS, AD8519ART $-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C}$ <br> AD8519AR (R-8), AD8529 $-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C}$ $\begin{aligned} & 0 \mathrm{~V} \leq \mathrm{V}_{\mathrm{CM}} \leq 1.7 \mathrm{~V},-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C} \\ & \mathrm{R}_{\mathrm{L}}=2 \mathrm{k} \Omega, 0.5 \mathrm{~V}<\mathrm{V}_{\text {OUT }}<2.2 \mathrm{~V} \\ & \mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega \end{aligned}$ | 0 <br> 55 <br> 20 | $\begin{aligned} & 700 \\ & 900 \\ & 700 \\ & \\ & \\ & 75 \\ & 20 \\ & 30 \end{aligned}$ | $\begin{aligned} & 1400 \\ & 1600 \\ & 1200 \\ & 1300 \\ & 300 \\ & \pm 50 \\ & 2 \end{aligned}$ | $\mu \mathrm{V}$ <br> $\mu \mathrm{V}$ <br> $\mu \mathrm{V}$ <br> $\mu \mathrm{V}$ <br> nA <br> nA <br> V <br> dB <br> $\mathrm{V} / \mathrm{mV}$ <br> V/mV |
| OUTPUT CHARACTERISTICS Output Voltage Swing High Output Voltage Swing Low | VoH <br> Vol | $\begin{aligned} & \mathrm{I}_{\mathrm{L}}=250 \mu \mathrm{~A} \\ & \mathrm{I}_{\mathrm{L}}=5 \mathrm{~mA} \\ & \mathrm{I}_{\mathrm{L}}=250 \mu \mathrm{~A} \\ & \mathrm{I}_{\mathrm{L}}=5 \mathrm{~mA} \end{aligned}$ | $\begin{aligned} & 2.60 \\ & 2.50 \end{aligned}$ |  | $\begin{aligned} & 100 \\ & 200 \end{aligned}$ | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~V} \\ & \mathrm{mV} \\ & \mathrm{mV} \end{aligned}$ |
| POWER SUPPLY <br> Power Supply Rejection Ratio <br> Supply Current/Amplifier | PSRR <br> Is | $\begin{aligned} & \mathrm{V}_{\mathrm{S}}=2.5 \mathrm{~V} \text { to } 7 \mathrm{~V} \\ & -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C} \\ & \text { Vout }=1.35 \mathrm{~V} \\ & -40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C} \end{aligned}$ | 60 | $\begin{aligned} & 80 \\ & 600 \end{aligned}$ | $\begin{aligned} & 1100 \\ & 1300 \end{aligned}$ | dB <br> $\mu \mathrm{A}$ <br> $\mu \mathrm{A}$ |
| DYNAMIC PERFORMANCE <br> Slew Rate <br> Settling Time <br> Gain Bandwidth Product Phase Margin | $\begin{aligned} & \mathrm{SR} \\ & \mathrm{t}_{\mathrm{s}} \\ & \mathrm{GBP} \\ & \Phi_{\mathrm{m}} \end{aligned}$ | $\begin{aligned} & \mathrm{RL}=10 \mathrm{k} \Omega \\ & \text { To } 0.01 \% \end{aligned}$ |  | $\begin{aligned} & 1.5 \\ & 2000 \\ & 6 \\ & 55 \end{aligned}$ |  | V/ $\mu \mathrm{s}$ <br> ns <br> MHz <br> Degrees |
| NOISE PERFORMANCE Voltage Noise Density Current Noise Density | $\begin{aligned} & \mathrm{e}_{\mathrm{n}} \\ & \mathrm{i}_{\mathrm{n}} \end{aligned}$ | $\begin{aligned} & f=1 \mathrm{kHz} \\ & \mathrm{f}=1 \mathrm{kHz} \end{aligned}$ |  | $\begin{aligned} & 10 \\ & 0.4 \end{aligned}$ |  | $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ <br> $\mathrm{pA} / \sqrt{ } \mathrm{Hz}$ |

## AD8519/AD8529

$\mathrm{V}_{\mathrm{S}}=5.0 \mathrm{~V}, \mathrm{~V}-=-5 \mathrm{~V}, \mathrm{~V}_{\mathrm{CM}}=0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.
Table 4.

| Parameter | Symbol | Conditions | Min | Typ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| INPUT CHARACTERISTICS |  |  |  |  |  |  |
| Offset Voltage | Vos | AD8519AKS, AD8519ART |  | 600 | 1100 | $\mu \mathrm{V}$ |
|  |  | $-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C}$ |  | 800 | 1300 | $\mu \mathrm{V}$ |
|  |  | AD8519AR (R-8), AD8529 |  | 600 | 1000 | $\mu \mathrm{V}$ |
|  |  | $-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C}$ |  |  | 1100 | $\mu \mathrm{V}$ |
| Input Bias Current | $\mathrm{I}_{\mathrm{B}}$ | $\mathrm{V}_{\mathrm{cm}}=0 \mathrm{~V}$ |  |  | 300 | nA |
|  |  | $\mathrm{V}_{\text {CM }}=0 \mathrm{~V},-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C}$ |  |  | 400 | nA |
| Input Offset Current | los | $V_{\text {cm }}=0 \mathrm{~V}$ |  |  | $\pm 50$ | nA |
|  |  | $\mathrm{V}_{\text {cM }}=0 \mathrm{~V},-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C}$ |  |  | $\pm 100$ | nA |
| Input Voltage Range | $V_{\text {cm }}$ |  | -5 |  | +4 | V |
| Common-Mode Rejection Ratio | CMRR | $-4.9 \mathrm{~V} \leq \mathrm{V}_{\text {cm }} \leq+4.0 \mathrm{~V}$, |  |  |  |  |
|  |  | $-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C}$ | 70 | 100 |  | dB |
| Large Signal Voltage Gain | Avo | $\mathrm{R}_{\mathrm{L}}=2 \mathrm{k} \Omega$ |  | 30 |  | V/mV |
|  |  | $\mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega$ | 50 | 200 |  | $\mathrm{V} / \mathrm{mV}$ |
|  |  | $-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C}$ | 25 |  |  | $\mathrm{V} / \mathrm{mV}$ |
| Offset Voltage Drift | $\Delta \mathrm{Vos} / \Delta \mathrm{T}$ |  |  | 2 |  | $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ |
| Bias Current Drift | $\Delta I_{B} / \Delta T$ |  |  | 500 |  | $\mathrm{pA} /{ }^{\circ} \mathrm{C}$ |
| OUTPUT CHARACTERISTICS |  |  |  |  |  |  |
| Output Voltage Swing High | Vor | $\mathrm{L}=250 \mu \mathrm{~A}$ |  |  |  |  |
|  |  | $-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C}$ | 4.90 |  |  | V |
|  |  | $\mathrm{L}_{\mathrm{L}}=5 \mathrm{~mA}$ | 4.80 |  |  | V |
| Output Voltage Swing Low | Vol | $\mathrm{L}_{\mathrm{L}}=250 \mu \mathrm{~A}$ |  |  |  |  |
|  |  | $-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C}$ |  |  | -4.90 | V |
|  |  | $\mathrm{L}=5 \mathrm{~mA}$ |  |  | -4.80 | V |
| Short-Circuit Current | Isc | Short to ground, instantaneous |  | $\pm 70$ |  | mA |
| Maximum Output Current | Iout |  |  | $\pm 25$ |  | mA |
| POWER SUPPLY |  |  |  |  |  |  |
| Power Supply Rejection Ratio | PSRR | $\mathrm{V}_{\text {s }}= \pm 1.5 \mathrm{~V}$ to $\pm 6 \mathrm{~V},-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C}$ | 60 | 100 |  | dB |
| Supply Current/Amplifier | ls Y | Vout $=0 \mathrm{~V}$ |  | 600 | 1200 | $\mu \mathrm{A}$ |
|  |  | $-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+125^{\circ} \mathrm{C}$ |  |  | 1400 | $\mu \mathrm{A}$ |
| DYNAMIC PERFORMANCE |  |  |  |  |  |  |
| Slew Rate | SR | $-4 \mathrm{~V}<\mathrm{V}_{\text {OUT }}<+4 \mathrm{~V}, \mathrm{R}_{\mathrm{L}}=10 \mathrm{k} \Omega$ |  | 2.9 |  | V/us |
| Settling Time | ts | To 0.01\% |  | 1000 |  |  |
| Gain Bandwidth Product | GBP |  |  | 8 |  | MHz |
| Phase Margin | $\Phi_{m}$ |  |  | 60 |  | Degrees |
| NOISE PERFORMANCE |  |  |  |  |  |  |
| Voltage Noise Density | $\mathrm{e}_{\mathrm{n}}$ | $\mathrm{f}=1 \mathrm{kHz}$ |  | 10 |  | $\mathrm{nV} / \sqrt{\mathrm{Hz}}$ |
| Current Noise Density | $\mathrm{i}_{\mathrm{n}}$ | $\mathrm{f}=1 \mathrm{kHz}$ |  | 0.4 |  | $\mathrm{pA} / \sqrt{\mathrm{Hz}}$ |

## ABSOLUTE MAXIMUM RATINGS

Table 5.

| Parameter | Rating |
| :--- | :--- |
| Supply Voltage | $\pm 6 \mathrm{~V}$ |
| Input Voltage $^{1}$ | $\pm 6 \mathrm{~V}$ |
| Differential Input Voltage $^{2}$ | $\pm 0.6 \mathrm{~V}$ |
| Storage Temperature Range | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Operating Temperature Range | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |
| Junction Temperature Range | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Lead Temperature Range <br> $\quad$ (Soldering, 60 sec) | $300^{\circ} \mathrm{C}$ |

${ }^{1}$ For supply voltages less than $\pm 6 \mathrm{~V}$, the input voltage is limited to less than or equal to the supply voltage.
${ }^{2}$ For differential input voltages greater than $\pm 0.6 \mathrm{~V}$, the input current should be limited to less than 5 mA to prevent degradation or destruction of the input devices.
Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. This is a stress rating only; functional operation of the device at these or any other conditions above those indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

## THERMAL RESISTANCE

Table 6.

| Package Type |
| :--- |
| 5-Lead SC70 (KS) |
| $\boldsymbol{\theta}_{\mathbf{J A}}{ }^{\mathbf{1}}$ |
| 5-Lead SOT-23 (RJ) |
| 5-Lead SOIC (R) |
| 8-Lead |
| 8-Lead MSOP (RM) |

ESD CAUTION

|  | ESD (electrostatic discharge) sensitive device. <br> Charged devices and circuit boards can discharge <br> without detection. Although this product features <br> patented or proprietary protection circuitry, damage <br> may occur on devices subjected to high energy ESD. <br> Therefore, proper ESD precautions should be taken to <br> avoid performance degradation or loss of functionality. |
| :--- | :--- |

## AD8519/AD8529

TYPICAL PERFORMANCE CHARACTERISTICS


Figure 4. Input Offset Voltage Distribution


Figure 5. Supply Current per Amplifier vs. Supply Voltage


Figure 6. Supply Current per Amplifier vs. Temperature


Figure 7. Input Bias Current vs. Common-Mode Voltage


Figure 8. Common-Mode Rejection vs. Common-Mode Voltage


Figure 9. Open-Loop Gain, Phase vs. Frequency


Figure 10. Closed-Loop Gain vs. Frequency


Figure 11. CMRR vs. Frequency


Figure 12. PSRR vs. Frequency


Figure 13. Overshoot vs. Capacitance Load


Figure 14. Step Size vs. Settling Time


Figure 15. Output Swing vs. Frequency

## AD8519/AD8529



Figure 16. Output Impedance vs. Frequency


Figure 17. Voltage Noise Density


Figure 18. Current Noise Density


Figure 19. 0.1 Hz to 10 Hz Noise


Figure 20. No Phase Reversal


Figure 21. Small Signal Transient Response


Figure 22. Large Signal Transient Response

## AD8519/AD8529

## APPLICATIONS INFORMATION

## MAXIMUM POWER DISSIPATION

The maximum power that can be safely dissipated by the AD8519/AD8529 is limited by the associated rise in junction temperature. The maximum safe junction temperature is $150^{\circ} \mathrm{C}$ for these plastic packages. If this maximum is momentarily exceeded, proper circuit operation is restored as soon as the die temperature is reduced. Operating the product in an overheated condition for an extended period can result in permanent damage to the device.

## PRECISION FULL-WAVE RECTIFIER

Slew rate is probably the most underestimated parameter when designing a precision rectifier. Yet without a good slew rate, large glitches are generated during the period when both diodes are off.

The operation of the basic circuit (shown in Figure 23) should be examined before considering the slew rate further. U1 is set up to have two states of operation. D1 and D2 diodes switch the output between the two states. State one is an inverter with a gain of +1 , and state two is a simple unity gain buffer where the output is equal to the value of the virtual ground. The virtual ground is the potential present at the noninverting node of the U1. State one is active when $V_{\text {IN }}$ is larger than the virtual ground. D2 is on in this condition. If $\mathrm{V}_{\text {IN }}$ drops below virtual ground, D2 turns off and D1 turns on. This causes the output of U1 to simply buffer the virtual ground and this configuration is state two. Therefore, the function of U1, which results from these two states of operation, is a half-wave inverter. The U2 function takes the inverted half wave at a gain of two and sums it into the original VIN wave, which outputs a rectified full wave.

$$
V_{\text {OUT }}=V_{I N}-2\left|V_{I N}^{-1}<0\right|
$$

This type of rectifier can be very precise if the following electrical parameters are adhered to:

- All passive components should be of tight tolerance, $1 \%$ for resistors and 5\% for capacitors.
- If the application circuit requires high impedance (that is, direct sensor interface), then an FET amplifier is a better choice than the AD8519.
- An amp such as the AD8519, which has a great slew rate specification, yields the best result because the circuit involves switching.


Figure 23. Precision Full-Wave Rectifier
Switching glitches are caused when D1 and D2 are both momentarily off. This condition occurs every time the input signal is equal to the virtual ground potential. When this condition occurs, the U1 stage is taken out of the Vout equation and $V_{\text {out }}$ is equal to $\mathrm{V}_{\text {IN }} \times \mathrm{R} 5 \times(\mathrm{R} 4 \| \mathrm{R} 1+\mathrm{R} 2+\mathrm{R} 3)$. Note that Node A should be $V_{\text {IN }}$ inverted or virtual ground, but in this condition, Node A is simply tracking Vin. Given a sine wave input centered around virtual ground, glitches are generated at the sharp negative peaks of the rectified sine wave. If the glitches are hard to notice on an oscilloscope, raise the frequency of the sine wave until they become apparent. The size of the glitches is proportional to the input frequency, the diode turn-on potential ( 0.2 V or 0.65 V ), and the slew rate of the op amp.

R6 and R7 are both necessary to limit the amount of bias current related voltage offset. Unfortunately, there is no perfect value for R6 because the impedance at the inverting node is altered as D1 and D2 switch. Therefore, there is also some unresolved bias current related offset. To minimize this offset, use lower value resistors or choose an FET amplifier if the optimized offset is still intolerable.

The AD8519 offers a unique combination of speed vs. power ratio at 2.7 V single supply, small size (SC70 and SOT-23), and low noise that makes it an ideal choice for most high volume and high precision rectifier circuits.

## $10 \times$ MICROPHONE PREAMP MEETS PC99 SPECIFICATIONS

This circuit, while lacking a unique topology, is anything but featureless when an AD8519 is used as the op amp. This preamp gives 20 dB gain over a frequency range of 20 Hz to 20 kHz and is fully PC99 compliant in all parameters including THD + N, dynamic range, frequency range, amplitude range, and crosstalk. Not only does this preamp comply with the PC99 specifications, it far surpasses them. In fact, when the input noise is 120 dB , this preamp has a Vout noise of around 100 dB , which is suitable for most professional 20-bit audio systems. At 120 dB THD +N in unity gain, the AD8519 is suitable for 24-bit professional audio systems. In other words, the AD8519 will not be the limiting performance factor in audio systems despite its small size and low cost.

Slew rate related distortion is not present at the lower voltages because the AD8519 is so fast at $2.1 \mathrm{~V} / \mu \mathrm{s}$. A general rule of thumb for determining the necessary slew rate for an audio system is to take the maximum output voltage range of the device, given the design's power rails, and divide by two. In Figure 24, the power rails are 2.7 V and the output is rail-to-rail. Enter these numbers into the equation: $2.7 / 2=1.35 \mathrm{~V}$, and the minimum ideal slew rate is $1.35 \mathrm{~V} / \mu \mathrm{s}$.

While this data sheet gives only one audio example, many audio circuits are enhanced with the use of the AD8519. Examples include: active audio filters such as bass, treble, and equalizers; PWM filters at the output of audio DACs; buffers and summers for mixing stations; and gain stages for volume control.


Figure 24. $10 \times$ Microphone Preamplifier

## TWO-ELEMENT VARYING BRIDGE AMPLIFIER

There are a host of bridge configurations available to designers. For a complete analysis, look at the ubiquitous bridge and its different forms. Refer to the 1992 Amplifier Applications Guide ${ }^{1}$.

Figure 25 is a schematic of a two-element varying bridge. This configuration is commonly found in pressure and flow transducers. With a two-element varying bridge, the signal is $2 \times$ as compared to a single-element varying bridge. The advantages of this type of bridge are gain setting range and single-supply application. Negative characteristics are nonlinear operation and required R matching. Given these sets of conditions, requirements, and characteristics, the AD8519 can be successfully used in this configuration because of its rail-to-rail output and low offset. Perhaps the greatest benefits of the AD8519, when used in the bridge configuration, are the advantages it can bring when placed in a remote bridge sensor. For example, the tiny SC70 and SOT-23 packages reduce the overall sensor size; low power allows for remote powering via batteries or solar cells, high output current drive to drive a long cable; and 2.7 V operation for two-cell operation.


Figure 25. Two-Element Varying Bridge Amplifier

[^0]
## AD8519/AD8529

## OUTLINE DIMENSIONS



COMPLIANT TO JEDEC STANDARDS MS-012-AA
CONTROLLING DIMENSIONS ARE IN MILLIMETERS; INCH DIMENSIONS (IN PARENTHESES) ARE ROUNDED-OFF MILLIMETER EQUIVALENTS FOR REFERENCE ONLY AND ARE NOT APPROPRIATE FOR USE IN DESIGN.

Figure 26. 8-Lead Standard Small Outline Package [SOIC_N] Narrow Body
( $R-8$ )
Dimensions shown in millimeters and (inches)


COMPLIANT TO JEDEC STANDARDS MO-203-AA

Figure 28. 5-Lead Thin Shrink Small Outline Transistor Package [SC70] (KS-5)
Dimensions shown in millimeters


COMPLIANT TO JEDEC STANDARDS MO-187-AA
Figure 27. 8-Lead Mini Small Outline Package [MSOP] (RM-8) Dimensions shown in millimeters


COMPLIANT TO JEDEC STANDARDS MO-178-AA
Figure 29. 5-Lead Small Outline Transistor Package [SOT-23] (RJ-5) Dimensions shown in millimeters

ORDERING GUIDE

| Model | Temperature Range | Package Description | Package Option | Branding Information |
| :---: | :---: | :---: | :---: | :---: |
| AD8519AKS-REEL7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 5-Lead SC70 | KS-5 | A3B |
| AD8519AKSZ-REEL7 ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 5-Lead SC70 | KS-5 | A11 |
| AD8519ART-REEL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 5-Lead SOT-23 | RJ-5 | A3A |
| AD8519ART-REEL7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 5-Lead SOT-23 | RJ-5 | A3A |
| AD8519ARTZ-REEL ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 5-Lead SOT-23 | RJ-5 | A3A\# |
| AD8519ARTZ-REEL7 ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 5-Lead SOT-23 | RJ-5 | A3A\# |
| AD8519AR | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8519AR-REEL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8519AR-REEL7 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8519ARZ ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8519ARZ-REEL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8519ARZ-REEL71 | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8529AR | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8529AR-REEL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8529ARZ ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8529ARZ-REEL ${ }^{1}$ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead SOIC_N | R-8 |  |
| AD8529ARM-REEL | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead MSOP | RM-8 | A5A |
| AD8529ARMZ-REEL¹ | $-40^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ | 8-Lead MSOP | RM-8 | A5A\# |

[^1]
## AD8519/AD8529

## NOTES

# Mouser Electronics 

Authorized Distributor

Click to View Pricing, Inventory, Delivery \& Lifecycle Information:

Analog Devices Inc.:
AD8519AKSZ-REEL7 AD8519ARTZ-REEL7 AD8529ARZ AD8519ARTZ-REEL AD8529ARMZ-REEL AD8529ARZ-
REEL


[^0]:    ${ }^{1}$ Adolfo Garcia and James Wong, Chapter 2, 1992, Amplifier Applications Guide.

[^1]:    ${ }^{1} \mathrm{Z}=$ RoHS compliant part, \# denotes RoHS compliant part may be top or bottom marked.

