ALPHA \& OMEGA
SEMICONDUCTOR

## General Description

The AOZ1375DI is a bidirectional current-limited load switch intended for applications that require circuit protections. The device operates from voltages between 3.4 V and 23 V and features two power terminals, VINT and VBUS, which are rated at 28 V Absolute Maximum. When used as source switch, the internal current limiting circuit protects the supply from large load current. The current limit can be set with an external resistor. The back-to-back switch configuration blocks any leakage between VINT and VBUS pins when the device is disabled.

The AOZ1375DI provides over-voltage protection, short-circuit protection and thermal protection function that limit excessive power dissipation. The over-voltage protection threshold is selectable by an external resistor. The internal soft-start circuitry controls inrush current due to highly capacitive loads. The soft-start can be adjusted using an external capacitor. It consumes less than $5 \mu \mathrm{~A}$ in shutdown.

The AOZ1375DI-01 is available in a $3 \mathrm{~mm} \times 3 \mathrm{~mm}$ DFN-12L package which can operate over $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ temperature range.

## Features

- $17.8 \mathrm{~m} \Omega$ typical ON resistance
- 3.4 V to 23 V operating input voltage
- VINT and VBUS are both rated 28 V
- Bidirectional operation
- Reverse blocking to completely isolate VINT and VBUS when disabled
- Programmable current limit
- Short-circuit protection
- Selectable over-voltage protection
- Programmable soft-start
- Under-voltage lockout
- Over-voltage lockout
- Thermal shutdown protection
- $\pm 4 \mathrm{kV}$ HBM ESD rating
- $\pm 8 \mathrm{kV}$ HBM ESD rating for VBUS and VINT
- DFN3x3-12L package
- UL 2367: file no. E495859
- IEC 62368-1: file no. E326264.


## Applications

- Thunderbolt/USB Type-C PD power switch
- Notebook/desktop
- Monitors
- Docking station/dongles



## Typical Application



## Ordering Information

| Part Number | Fault Recovery | Temperature Range | Package | Environmental |
| :---: | :---: | :---: | :---: | :---: |
| AOZ1375DI-01 | Auto-Restart | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | $3 \mathrm{~mm} \times 3 \mathrm{~mm}$ DFN-12L | RoHS |
| AOZ1375DI-02 | Latch-Off | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | $3 \mathrm{~mm} \times 3 \mathrm{~mm}$ DFN-12L | RoHS |

AOS products are offered in packages with Pb-free plating and compliant to RoHS standards.
Please visit www.aosmd.com/media/AOSGreenPolicy.pdf for additional information.
Greep product

Pin Configuration


## Pin Description

| Pin Number | Pin Name | Pin Function |
| :---: | :---: | :--- |
| 1,2 | VBUS | Adapter supply input or output to periphery. Connect to VBUS Connector. |
| 3 | POVP | Programmable over voltage protection. Connect a resistor R R OVP from POVP to GND. |
| 4 | FLTB | Fault Indicator, Open Drain output. Active Low when fault condition occurs. |
| 5 | EN | Enable Input. |
| 6 | GND | Ground. |
| 7 | SS | Soft-start pin. Connect a capacitor C SS from SS to GND to set the soft-start time. |
| 8 | ILIM | Current limit set pin. Connect a resistor R RIM from ILIM to GND to set the switch current limit. |
| 9 | CSP | Current sense positive input, connect to a 10m $\Omega$ for accurate current sensing. Short to VINT <br> if current limit is not required. |
| 10 | CSN | Current sense negative input, connect to a 10m $\Omega$ for accurate current sensing. Short to VINT <br> if current limit is not required. |
| 11,12 | VINT | Connect to internal power source or load. <br> EXP |
| Exposed Thermal Pad. Connect to GND. Solder to a metal surface directly underneath the <br> EXP and connect to PCB ground on multiple layers through vias. For best thermal <br> performance make the ground copper pads as large as possible and connect to EXP with <br> multiple vias. |  |  |

Absolute Maximum Ratings ${ }^{(1)}$
Exceeding the Absolute Maximum ratings may damage the device.

| Parameter | Rating |
| :--- | ---: |
| VINT, VBUS, CSP, CSN, to GND | -0.3 V to +28 V |
| VINT-CSP, VINT-CSN, CSP-CSN | -0.3 V to +0.3 V |
| EN, ILIM, SS, FLTB, POVP to GND | -0.3 V to +6 V |
| Junction Temperature $\left(\mathrm{T}_{\mathrm{J}}\right)$ | $+150^{\circ} \mathrm{C}$ |
| Storage Temperature ( $\left.\mathrm{T}_{\mathrm{S}}\right)$ | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| ESD Rating HBM All Pins ${ }^{(1)}$ | $\pm 4 \mathrm{kV}$ |
| ESD Rating HBM VBUS/VINT | $\pm 8 \mathrm{kV}$ |

## Note:

1. Devices are inherently ESD sensitive, handling precautions are required. Human body model is a 100 pF capacitor discharging through a $1.5 \mathrm{k} \Omega$ resistor.

## Recommended Operating Conditions

The device is not guaranteed to operate beyond the Maximum Recommended Operating Conditions.

| Parameter | Rating |
| :--- | ---: |
| Supply Voltage (VINT, VBUS) | 3.4 V to 23 V |
| EN, FLTB | 0 V to 5.5 V |
| POVP | 0 V to 3 V |
| DC Switch Current (ISW) | 0 A to 8 A |
| Peak Switch Current (ISW_PK) for $10 \mathrm{~ms} @$ <br> $2 \% ~ D u t y ~ C y c l e ~$ | 20 A |
| Ambient Temperature $\left(\mathrm{T}_{\mathrm{A}}\right)$ | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| Package Thermal Resistance <br> DFN3x3-12L $\left(\Theta_{\mathrm{JA}}\right)$ | $50^{\circ} \mathrm{C} / \mathrm{W}$ |

## Electrical Characteristics

$T_{A}=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{IN}}=20 \mathrm{~V}$, unless otherwise specified.

| Symbol | Parameter | Conditions | Min | Typ | Max | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\text {VINT }}$ | Input Supply Voltage | VINT is input and VBUS is output | 3.4 |  | 23 | V |
| $\mathrm{V}_{\text {VBUS }}$ |  | VBUS is input and VINT is output | 3.4 |  | 23 |  |
| $\mathrm{V}_{\text {UVLO }}$ | Under-voltage Lockout Threshold | VIN rising, VBUS is output | 3.0 |  | 3.35 | V |
|  |  | VBUS rising, VINT is output | 3.0 |  | 3.35 |  |
| VUVLO_HYS | Under-voltage Lockout Hysteresis | VINT falling, VBUS is output |  | 0.25 |  | V |
|  |  | VBUS falling, VINT is output |  | 0.25 |  |  |
| VoVLo_VINT Vovlo_vbus | Over-voltage Lockout Threshold | $\mathrm{R}_{\text {OVP }}=20 \mathrm{k} \Omega, 1 \%$ | 23.0 | 24.0 | 25.0 | V |
|  |  | $\mathrm{R}_{\text {OVP }}=75 \mathrm{k} \Omega, 1 \%$ | 16.8 | 17.4 | 18.0 |  |
|  |  | $R_{\text {OVP }}=137 \mathrm{k} \Omega, 1 \%$ | 10.0 | 10.4 | 10.8 |  |
|  |  | $\mathrm{R}_{\text {OVP }}=301 \mathrm{k} \Omega, 1 \%$ | 6.2 | 6.4 | 6.6 |  |
| V ${ }_{\text {OVLO_HYS }}$ | Over-voltage Lockout Hysteresis | VINT and VBUS |  | 300 |  | mV |
| $\mathrm{t}_{\text {D_OVP }}$ | Over-voltage Turn-off Delay | VINT and VBUS |  | 1 |  | $\mu \mathrm{s}$ |
| IVINT_ON | Input Quiescent Current | VINT $=20 \mathrm{~V}, \mathrm{IVBUS}=0 \mathrm{~A}, \mathrm{EN}=5 \mathrm{~V}$ |  | 550 |  | $\mu \mathrm{A}$ |
| $\mathrm{I}_{\text {VBUS_ON }}$ |  | VBUS $=20 \mathrm{~V}, \mathrm{IVINT}=0 \mathrm{~A}, \mathrm{EN}=5 \mathrm{~V}$ |  |  |  |  |
| $\mathrm{I}_{\text {VINT_OFF }}$ | Input Shutdown Current | VINT $=20 \mathrm{~V}$, VBUS $=$ Float, EN $=0 \mathrm{~V}$ |  | 2 | 5 | $\mu \mathrm{A}$ |
| IVBUS_OFF | Output Leakage Current | VBUS $=20 \mathrm{~V}, \mathrm{VINT}=$ Float, $\mathrm{EN}=0 \mathrm{~V}$ |  | 2 | 5 |  |
| $\mathrm{R}_{\text {ON }}$ | Switch On Resistance | $\mathrm{VINT}=20 \mathrm{~V}, \mathrm{I}_{\mathrm{VBUS}}=1 \mathrm{~A}, \mathrm{R}_{\text {LIM }}=30 \mathrm{k} \Omega$ |  | 17.8 |  | $\mathrm{m} \Omega$ |
|  |  | $\mathrm{VINT}=5 \mathrm{~V}, \mathrm{I}_{\mathrm{VBUS}}=1 \mathrm{~A}, \mathrm{R}_{\text {LIM }}=30 \mathrm{k} \Omega$ |  | 18.2 |  |  |

## Electrical Characteristics (Continued)

$T_{A}=25^{\circ} \mathrm{C}, \mathrm{V}_{I N}=20 \mathrm{~V}$, unless otherwise specified.

| Symbol | Parameter | Conditions | Min | Typ | Max | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $I_{\text {Limit }}$ | Current Limit ${ }^{(2)}$ | $\begin{aligned} & \mathrm{R}_{\mathrm{LIM}}=68 \mathrm{k} \Omega(1 \% \text { Tolerance }) \\ & \mathrm{R}_{\text {SENSE }}=10 \mathrm{~m} \Omega(1 \% \text { Tolerance }) \end{aligned}$ | 2.0 | 2.35 | 2.7 | A |
|  |  | $\begin{aligned} & \mathrm{R}_{\mathrm{LIM}}=47 \mathrm{k} \Omega(1 \% \text { Tolerance }) \\ & \mathrm{R}_{\mathrm{SENSE}}=10 \mathrm{~m} \Omega(1 \% \text { Tolerance }) \end{aligned}$ | 3.0 | 3.4 | 3.8 |  |
|  |  | $\begin{aligned} & \mathrm{R}_{\mathrm{LIM}}=30 \mathrm{k} \Omega(1 \% \text { Tolerance }) \\ & \mathrm{R}_{\text {SENSE }}=10 \mathrm{~m} \Omega(1 \% \text { Tolerance }) \end{aligned}$ | 5.0 | 5.3 | 5.6 |  |
| $\mathrm{V}_{\text {EN_H }}$ | Enable Input High Voltage |  | 1.4 |  |  | V |
| $\mathrm{V}_{\text {EN_L }}$ | Enable Input Low Voltage |  |  |  | 0.6 | V |
| $\mathrm{I}_{\text {EN_BIAS }}$ | Enable Input Bias Current | $\mathrm{EN}=1.8 \mathrm{~V}$ |  | 4 | 10 | $\mu \mathrm{A}$ |
| $V_{\text {FLTB_LO }}$ | Fault Pull-down Voltage | $\mathrm{I}_{\text {SINK }}=3 \mathrm{~mA}$ |  |  | 0.3 | V |
| $t_{\text {D_ON }}$ | Turn-On Delay Time EN to VBUS ( $10 \%$ of VINT) | EN to $10 \%$ of VINT, VINT $=20 \mathrm{~V}$, CVBUS $=68 \mu \mathrm{~F}, \mathrm{CSS}=1 \mathrm{nF}$ |  | 1600 |  | $\mu \mathrm{s}$ |
| $\mathrm{t}_{\mathrm{ON}}$ | Turn-On Rise Time VBUS from 10\% to $90 \%$ | VBUS rising from $10 \%$ to $90 \%$ of VINT, VINT $=20 \mathrm{~V}, \mathrm{C}_{\mathrm{VB}}=68 \mu \mathrm{~F}$, $\mathrm{C}_{\mathrm{SS}}=1 \mathrm{nF}$ |  | 400 |  | $\mu \mathrm{s}$ |
| $V_{\text {SCP }}$ | Short-Circuit Protection | VINT - VBUS when VINT $=20 \mathrm{~V}$ |  | 5 |  | V |
| $\mathrm{T}_{\text {SD }}$ | Thermal Shutdown Threshold |  |  | 140 |  | ${ }^{\circ} \mathrm{C}$ |
| $\mathrm{T}_{\text {SD_HYS }}$ | Thermal Shutdown Hysteresis |  |  | 35 |  | ${ }^{\circ} \mathrm{C}$ |
| $\mathrm{t}_{\mathrm{OCP}}$ | Over Current Response Time | Over current to switch disabled |  | 1 |  | ms |
| $\mathrm{t}_{\text {D_FLTB }}$ | FLTB Delay | The time of occurrence of over current to FLTB going low |  | 500 |  | $\mu \mathrm{s}$ |
| $t_{\text {REC }}$ | FLTB Recover Time | Fault is removed |  | 64 |  | ms |

## Note:

2. Configured such that VINT is input and VBUS is output.

## Functional Block Diagram



Timing Diagrams


Figure 1. Turn-on Delay and Turn-on Time


Figure 2. OVP Delay and Recovery Time for VINT OVP (AOZ1375DI-01) Same response for VBUS OVP with VINT and VBUS exchange


Figure 3. OCP and FLTB Time

## Typical Characteristics

$\mathrm{C}_{\mathrm{IN}}=20 \mu \mathrm{~F}, \mathrm{C}_{\mathrm{OUT}}=120 \mu \mathrm{~F}, \mathrm{R}_{\mathrm{LOAD}}=100 \Omega, \mathrm{C}_{\mathrm{SS}}=5.6 \mathrm{nF}, \mathrm{POVP}=0 \mathrm{~V}$, unless otherwise specified.


VINT OVP Operation
with $R_{\text {OVP }}=20 \mathrm{k} \Omega$



400 $\mu \mathrm{s} / \mathrm{div}$
Turn-Off by EN
(VINT $=5 \mathrm{~V}$ )


VINT OVP Operation
with $\mathrm{R}_{\mathrm{OVP}}=301 \mathrm{k} \Omega$


## Typical Characteristics (Continued)

$\mathrm{C}_{\mathrm{IN}}=20 \mu \mathrm{~F}, \mathrm{C}_{\mathrm{OUT}}=120 \mu \mathrm{~F}, \mathrm{R}_{\mathrm{LOAD}}=100 \Omega, \mathrm{C}_{\mathrm{SS}}=5.6 \mathrm{nF}, \mathrm{POVP}=0 \mathrm{~V}$, unless otherwise specified.


## Typical Characteristics

$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise specified.


Figure 4. VINT Quiescent Current vs. VINT Voltage


Figure 6. VINT Shutdown Current vs. VINT Voltage


Figure 8. VINT Quiescent Current vs. Temperature (VINT = 20V)


Figure 5. VBUS Quiescent Current vs. VBUS Voltage


Figure 7. VBUS Shutdown Current vs. VBUS Voltage


Figure 9. VBUS Quiescent Current vs. Temperature (VBUS = 20V)

## Typical Characteristics (Continued)

$T_{A}=25^{\circ} \mathrm{C}$, unless otherwise specified.


Figure 10. VINT Shutdown Current vs. Temperature (VINT = 20V)


Figure 12. Enable Input Low Voltage vs. Temperature


Figure 14. UVLO Rise Voltage (VINT) vs. Temperature


Figure 11. VBUS Shutdown Current vs. Temperature (VBUS = 20V)


Figure 13. Enable Input High Voltage vs. Temperature


Figure 15. UVLO Rise Voltage (VBUS) vs. Temperature

## Typical Characteristics (Continued)

$T_{A}=25^{\circ} \mathrm{C}$, unless otherwise specified.


Figure 16. UVLO Hysteresis Voltage (VINT) vs. Temperature


Figure 18. VINT OVP vs. Temperature


Figure 17. UVLO Hysteresis Voltage (VBUS) vs. Temperature


Figure 19. VBUS OVP vs. Temperature

## Detailed Description

AOZ1375D is a high-side load switch with adjustable soft- start, over current limit, over-voltage, over temperature and short-circuit protections. It is capable of operating from 3.4 V to 23 V and rated up to 5 A .

AOZ1375DI can be operated as bidirectional switch. As a source switch it can pass power from VINT to the VBUS. As a sink switch, it can pass supply from VBUS to VINT. The devices automatically select power from either VINT or VBUS whichever is higher.

The power switch consists of 2 back-to-back connected N -channel MOSFETs. When switch is enabled, the overall resistance between VINT and VBUS is only $17.8 \mathrm{~m} \Omega$ in typical condition, minimizing power lose and thermal dissipation. The back-to-back configuration of switches completely isolates between VINT and VBUS when turned off, preventing leakage between the two pins.

## Enable

The EN pin is the ON/OFF control for the power switch. The device is enabled when EN pin is high and device is not in UVLO lockout state. The EN pin must be driven to a logic high or logic low state to guarantee operation. While disabled, the AOZ1375DI only draws about $2 \mu \mathrm{~A}$ supply current.

## Input Under-Voltage Lockout (UVLO)

The internal circuitry of AOZ1375DI is powered from either VBUS or VINT. The under-voltage lockout (UVLO) circuit of AOZ1375DI monitors the voltage at both pins and only allows the power switches to turn on when VINT or VBUS is higher than 3.4 V . If both pins are below 3.4 V , the device is in under-voltage lockout state.

## Programmable Over-Voltage Protection (OVP)

The voltages at both VINT and VBUS pins are constantly monitored once the device is enabled. In case voltage on either pin exceeds the programmed threshold, over-voltage protection is activated:

1) If the power switch is on, it will be turned off immediately to isolate VINT from VBUS;
2) OVP will prevent power switch to be turned on if it is in off state.

In either case FLTB pin is pulled low to report the fault condition.

An external resistor $\mathrm{R}_{\mathrm{ovp}}$ connected between POVP and GND pins sets the over-voltage protection threshold. An internal $8 \mu \mathrm{~A}$ current source biases POVP pin. The voltage drop across resistor $\mathrm{R}_{\mathrm{Ovp}}$ is detected by comparators that sets the OVP threshold based on the table below:

Table 1. OVP Setting by External Resistor

| $\mathbf{R}_{\text {OVP }}$ Resistor Value (1\%) | OVP Threshold |
| :---: | :---: |
| $\leq 20 \mathrm{~K}$ | 24 V |
| 75 K | 17.4 V |
| 137 K | 10.4 V |
| $\geq 301 \mathrm{~K}$ | 6.4 V |

## Programmable Over-Current Protection (OCP)

AOZ1375DI implemented current limit to ensure that the current through the switch does not exceed the programmed value. The current passes through the switch is sensed using external sense resistor $\mathrm{R}_{\text {SENSE }}$. Current limit is programmed by an external resistor $\mathrm{R}_{\text {LIM }}$ connected between ILIM and GND. If over-load occur, the internal circuitry will limit the output current based on the value of $\mathrm{R}_{\text {LIM }}$.

The current limit threshold can be calculated according to equation below for $\mathrm{R}_{\text {SENSE }}=10 \mathrm{~m} \Omega$ :

$$
\text { Current Limit }=\frac{160}{\left(R_{\text {LIM }}\right)(k \Omega)}(A)
$$

For example, for 3.4 A current limit, a $47 \mathrm{k} \Omega$ RLIM should be selected.


Figure 20. Current Limit Vs $\mathrm{R}_{\mathrm{LIM}}$
The current limit threshold should be within 1 A to 6 A . Current limit accuracy or functionality is not guaranteed beyond this range. $1 \%$ resistors are recommended for both $\mathrm{R}_{\text {SENSE }}$ and $\mathrm{R}_{\text {LIM. }}$.

When AOZ1375DI is under current-limiting, FLTB is pulled low after $500 \mu$ s delay. The load switch will then open if the device is still current-limiting after an additional $500 \mu$ s delay.

There is no current limiting function when configured as sink switch (current flow from VBUS to VINT), but VINT startup rise time is still controlled by the $S S$ pin.

If current limit function is not used, both CSP and CSN pins must be connected to VINT.

## Short-Circuit Protection (SCP)

AOZ1375DI implemented short-circuit protection to quickly turn off the power switch when output is severely overloaded. A comparator monitors the voltage drop between VINT and VBUS when switch is closed. Short-circuit protection is activated when the above voltage difference reaches approximately $75 \%$ of VINT. Short-circuit protection functions in either sourcing or sinking configuration.

Short-circuit protection is not active until soft-start is completed.

## Thermal Shutdown Protection

During current limit or short-circuit, the power switch resistance is increased to limit the load current. This increase device power dissipation dramatically and causes the die temperature to rise. When the die temperature reaches $140^{\circ} \mathrm{C}$ the power switch is turned off. There is a $35^{\circ} \mathrm{C}$ hysteresis. Over-temperature fault is removed when die temperature drops below approximately $105^{\circ} \mathrm{C}$.

## Soft-Start

When EN pin is asserted high, the soft-start control circuitry applies voltage on the gate of the power switch in a manner such that the output voltage is ramped up linearly until it reaches input voltage level. The soft-start can be adjusted by an external capacitor $\mathrm{C}_{\text {ss }}$ connected between SS pin and ground. The soft-start can be approximately set by the following equation:

$$
t_{S S}=\left(\frac{V_{V I N}}{V_{O V P}}\right) \times\left(\left(\frac{C_{S S}}{0.0023}\right)-100\right)
$$

Where, VIN is in volts and $\mathrm{C}_{\mathrm{ss}}$ is in $n F$ and $\mathrm{t}_{\mathrm{ss}}$ is in $\mu \mathrm{s}$. Where VOVP $=24 \mathrm{~V}$. The recommended $\mathrm{C}_{\text {ss }}$ value is $1.0 \mathrm{nF} \sim 1.5 \mathrm{nF}$. The Css should less than 1.5 nF .

The actual soft-start also depends on the output capacitance and current limit setting if in-rush current reaches current-limit level.

## System Startup

The device is enabled when $\mathrm{EN} \geq 1.4 \mathrm{~V}$ and either VBUS or VINT is higher than UVLO threshold. The OVP threshold is first selected by sensing POVP voltage set by ROVP. The
device will then check if fault condition exist. When no fault exists, the power switch is turned on and the output is then ramped up, controlled by the soft-start and current limiting circuitry till it reaches input voltage.

## Fault Protection

AOZ1375D protects its load from the following fault conditions: over-voltage, over-current, short-circuit, and over-temperature.

When device is first enabled, the power switch is off and fault conditions are checked. If voltage at VBUS or VINT is higher than the OVP threshold, or die temperature is higher than thermal shutdown threshold. FLTB pin is pulled low to report to host controller.

After the power switch turned on, device continuously monitors all fault conditions. The switch is turned off when OVP, short-circuit, or over-temperature is detected. FLTB pin is pulled low.

In case of over-current, the device will limit the current pass-through the switch to the value set by RLIM. The switch is turned off if over-current last approximately 1 ms . FLTB pin is pulled low about $500 \mu$ s after OCP is detected.

## Auto-restart or Latch-off

AOZ1375DI-01 (auto-restart version): The device will try to restart 64 ms after the power switch is turned off due to fault protection.

AOZ1375DI-02 (latch-off version): The device keeps off after fault occurs. It can only be re-enabled by either toggle EN pin or recycle the power.

## Input Capacitor Selection

The input capacitor prevents large voltage transients from appearing at the input, and provides the instantaneous current needed each time the switch turns on to charge output capacitors and to limit input voltage drop. It is also to prevent high-frequency noise on the power line from passing through to the output. The input capacitor should be located as close to the pin as possible. A $10 \mu \mathrm{~F}$ ceramic capacitor is recommended. However, higher capacitor values further reduce the transient voltage drop at the input.

## Output Capacitor Selection

The output capacitor has to supply enough current for a large load that it may encounter during system transient. This bulk capacitor must be large enough to supply fast transient load in order to prevent the output from dropping.

There is an upper limit for output capacitor to ensure it can be charged fully during start-up. This upper limit is set by the current limit level and soft-start time.

$$
\text { Output Capacitor }(\text { Max })=\text { Current Limit } *\left(t_{O N} / \text { Input Voltage }\right)
$$

If output capacitor is too large that output voltage can't reach $75 \%$ of the input voltage at the end of soft-start time, short-circuit protection will be triggered.

## Power Dissipation Calculation

Calculate the power dissipation for normal load condition using the following equation:

$$
\text { Power Dissipated }=R_{\text {ON }} \times\left(I_{\text {OUT }}\right)^{2}
$$

The worst case power dissipation occurs when the load current hits the current limit due to over-current or short-circuit fault. The power dissipation under these conditions can be calculated using the following equation:

Power Dissipated $=\mid$ VINT $-V B U S \mid \times$ Current Limit

## Layout Guidelines

Good PCB layout is important for improving the thermal and overall performance of AOZ1375DI. To optimize the switch response time to output short-circuit conditions, keep all traces as short as possible to reduce the effect of unwanted parasitic inductance. Place the input and output bypass capacitors as close as possible to the VINT and VBUS pins. The input and output PCB traces should be as wide as possible for the given PCB space. Use a ground plane to enhance the power dissipation capability of the device. For accuracy current limit during source mode operation, RSENSE signal must be Kelvin connection to CSP and CSN pin. The sense location for RSENSE should be as close to the resistor terminal as possible to reduce the effect of resistance from PCB trace. Figure 21 shows the evaluation board reference layout.


Figure 21. Evaluation Board Layout

## Package Dimensions, DFN3x3-12L



RECOMMENDED LAND PATTERN


NOTE

1. DIMENSIONING AND TOLERANCING CONFORM TO ASME Y14.5M-1994.
2. CONTROLLING DIMENSION IS MILLIMETER. CONVERTED INCH DIMENSIONS ARE NOT NECESSARILY EXACT.
3. DIMENSION b APPLIES TO METALLIZED TERMINAL AND IS MEASURED BETWEEN 0.15 mm . AND 0.30 mm FROM THE TERMINAL TIP. IF THE TERMINAL HAS THE OPTIONAL RADIUS ON THE OTHER END OF THE TERMINAL, THE DIMENSION b SHOULD NOT BE MEASURED IN THAT RADIUS AREA.
4. COPLANARITY ddd APPLIERS TO THE TERMINALS AND ALL OTHER BOTTOM SURFACE METALLIZATION.

Tape and Reel Dimensions, DFN3x3-12L

## Carrier Tape


Reel


| TAPE SIZE | REEL SIZE | M | N | W | W1 | H | K | S | G | R | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 mm | ¢330 | $\begin{gathered} \varnothing 330.00 \\ \pm 0.50 \end{gathered}$ | $\begin{aligned} & \phi 97.00 \\ & \pm 0.10 \end{aligned}$ | $\begin{aligned} & 13.00 \\ & \pm 0.30 \end{aligned}$ | $\begin{aligned} & 17.40 \\ & \pm 1.00 \end{aligned}$ | $\begin{array}{r} \not \subset 13.00 \\ +0.50 \\ -0.20 \\ \hline \end{array}$ | 10.60 | $\begin{gathered} 2.00 \\ \pm 0.50 \end{gathered}$ | - | --- | --- |

## DFN3x3 EP TAPE

## Leader / Trailer \& Orientation

Unit Per Reel: 5000pcs


## Part Marking



| Part Number | Description | Code |
| :---: | :--- | :--- |
| AOZ1375DI-01 | Green Product | AA01 |
| AOZ1375DI-02 | Green Product | AA02 |

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