

# MIC2176-1/-2/-3



## Wide Input Voltage, Synchronous Buck Controllers Featuring Adaptive On-Time Control

### Hyper Speed Control™ Family

### General Description

The Micrel MIC2176-1/-2/-3 is a family of constant-frequency, synchronous buck controllers featuring a unique digitally modified adaptive ON-time control architecture. The MIC2176 family operates over an input supply range of 4.5V to 75V and can be used to supply up to 15A of output current. The output voltage is adjustable down to 0.8V with a guaranteed accuracy of  $\pm 1\%$ , and the device operates at a constant switching frequency of 100kHz, 200kHz, and 300kHz.

Micrel's Hyper Speed Control™ architecture allows for ultra-fast transient response while reducing the output capacitance and also makes (High  $V_{IN}$ )/(Low  $V_{OUT}$ ) operation possible. This digitally modified adaptive  $t_{ON}$  ripple control architecture combines the advantages of fixed-frequency operation and fast transient response in a single device.

The MIC2176 offers a full suite of protection features to ensure protection of the IC during fault conditions. These include undervoltage lockout to ensure proper operation under power-sag conditions, internal soft-start to reduce inrush current, fold-back current limit, "hiccup" mode short-circuit protection and thermal shutdown.

All support documentation can be found on Micrel's web site at: [www.micrel.com](http://www.micrel.com).

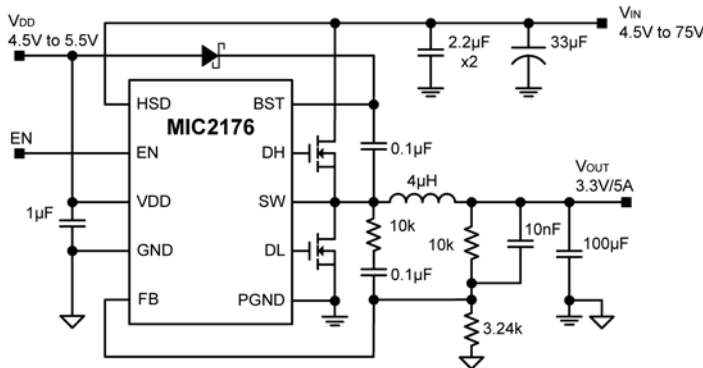
### Features

- Hyper Speed Control™ architecture enables
  - High delta V operation ( $V_{IN} = 75V$  and  $V_{OUT} = 1.2V$ )
  - Small output capacitance
- 4.5V to 75V input voltage
- Output down to 0.8V with  $\pm 1\%$  accuracy
- Any Capacitor™ Stable
  - Zero-ESR to high-ESR output capacitance
- 100kHz/200kHz/300kHz switching frequency
- Internal compensation
- 6ms Internal soft-start
- Foldback current limit and "hiccup" mode short-circuit protection
- Thermal shutdown
- Supports safe start-up into a pre-biased output
- $-40^{\circ}C$  to  $+125^{\circ}C$  junction temperature range
- Available in 10-pin MSOP package

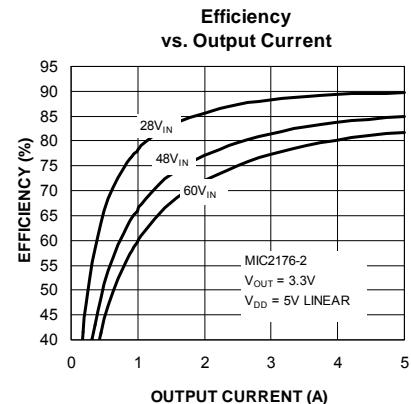
### Applications

- Distributed power systems
- Networking/Telecom Infrastructure
- Printers, scanners, graphic cards and video cards

### Typical Application



MIC2176-2 Adjustable Output 200kHz Buck Converter



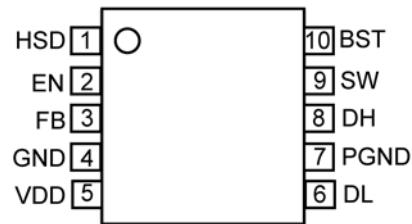
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## Ordering Information

Part Number	Output Voltage	Switching Frequency	Junction Temperature Range	Package	Lead Finish
MIC2176-1YMM	Adjustable	100kHz	-40°C to +125°C	10-pin MSOP	Pb-Free
MIC2176-2YMM	Adjustable	200kHz	-40°C to +125°C	10-pin MSOP	Pb-Free
MIC2176-3YMM	Adjustable	300kHz	-40°C to +125°C	10-pin MSOP	Pb-Free

## Pin Configuration



10-Pin MSOP (MM)

## Pin Description

Pin Number	Pin Name	Pin Function
1	HSD	High-Side MOSFET Drain Connection (Input): The HSD pin is the input of the adaptive On-time control circuitry. A 0.1 $\mu$ F ceramic capacitor between the HSD pin and the power ground (PGND) is required and must be placed as close as possible to the IC.
2	EN	Enable (Input): A logic level control of the output. The EN pin is CMOS compatible. Logic high or floating = enable, logic low = shutdown. In the off state, the $V_{DD}$ supply current of the device is reduced (typically 0.7mA). Do not connect the EN pin to the HSD pin.
3	FB	Feedback (Input): Input to the transconductance amplifier of the control loop. The FB pin is regulated to 0.8V. A resistor divider connecting the feedback to the output is used to adjust the desired output voltage.
4	GND	Signal ground. GND is the ground path for the device bias voltage $V_{DD}$ and the control circuitry. The loop for the signal ground should be separate from the power ground (PGND) loop.
5	VDD	$V_{DD}$ Bias (Input): Power to the internal reference and control sections of the MIC2176. The $V_{DD}$ operating voltage range is from 4.5V to 5.5V. A 1 $\mu$ F ceramic capacitor from the VDD pin to the PGND pin must be placed next to the IC.
6	DL	Low-Side Drive (output): High-current driver output for external low-side MOSFET. The DL driving voltage swings from ground to $V_{DD}$ .
7	PGND	Power Ground. PGND is the ground path for the buck converter power stage. The PGND pin connects to the sources of low-side N-Channel external MOSFETs, the negative terminals of input capacitors, and the negative terminals of output capacitors. The loop for the power ground should be as small as possible and separate from the Signal ground (GND) loop.
8	DH	High-Side Drive (output): High-current driver output for external high-side MOSFET. The DH driving voltage is floating on the switch node voltage ( $V_{SW}$ ). Adding a small resistor between DH pin and the gate of the high-side N-channel MOSFETs can slow down the turn-on and turn-off time of the MOSFETs.

**Pin Description (Continued)**

Pin Number	Pin Name	Pin Function
9	SW	Switch Node and Current-Sense input (Input): High current output driver return. The SW pin connects directly to the switch node. Due to the high-speed switching on this pin, the SW pin should be routed away from sensitive nodes. The SW pin also senses the current by monitoring the voltage across the low-side MOSFET during OFF time. In order to sense the current accurately, connect the low-side MOSFET drain to the SW pin using a Kelvin connection.
10	BST	Boost (Output): Bootstrapped voltage to the high-side N-channel internal MOSFET driver. A Schottky diode is connected between the VDD pin and the BST pin. A boost capacitor of 0.1 $\mu$ F is connected between the BST pin and the SW pin. Adding a small resistor in series with the BST pin can slow down the turn-on time of high-side N-Channel MOSFETs.

**Absolute Maximum Ratings<sup>(1, 2)</sup>**

$V_{HSD}$ to PGND	-0.3V to +76V
$V_{DD}$ to PGND	-0.3V to +6V
$V_{SW}$ to PGND	-0.3V to ( $V_{HSD} + 0.3V$ )
$V_{BST}$ to $V_{SW}$	-0.3V to 6V
$V_{BST}$ to PGND	-0.3V to 82V
$V_{EN}$ to PGND	-0.3V to ( $V_{DD} + 0.3V$ )
$V_{FB}$ to PGND	-0.3V to ( $V_{DD} + 0.3V$ )
PGND to GND	-0.3V to +0.3V
Junction Temperature	+150°C
Storage Temperature ( $T_S$ )	-65°C to +150°C
Lead Temperature (soldering, 10sec)	260°C

**Operating Ratings<sup>(3)</sup>**

Supply Voltage ( $V_{HSD}$ )	4.5V to 75V
Bias Voltage ( $V_{DD}$ )	4.5V to 5.5V
Enable Input ( $V_{EN}$ )	0V to $V_{DD}$
Junction Temperature ( $T_J$ )	-40°C to +125°C
Junction Thermal Resistance	
MSOP ( $\theta_{JA}$ )	130.5°C/W
Continuous Power Dissipation (derate 5.6mW/°C above 70°C)	
( $T_A = 70^\circ\text{C}$ )	421mW
ESD (Human Body Mode)	1.5kV

**Electrical Characteristics<sup>(4)</sup>**

$V_{IN} = V_{HSD} = 48V$ ,  $V_{DD} = 5V$ ;  $V_{BST} - V_{SW} = 5V$ ;  $T_A = 25^\circ\text{C}$ , unless noted. **Bold** values indicate  $-40^\circ\text{C} \leq T_J \leq +125^\circ\text{C}$ .

Parameter	Condition	Min.	Typ.	Max.	Units
<b>Power Supply Input</b>					
HSD Voltage Range ( $V_{HSD}$ ) <sup>(5)</sup>		<b>4.5</b>		<b>75</b>	V
<b><math>V_{DD}</math> Bias Voltage</b>					
Operating Bias Voltage ( $V_{DD}$ )		<b>4.5</b>	5	<b>5.5</b>	V
Undervoltage Lockout Trip Level	$V_{DD}$ Rising	<b>3.2</b>	3.85	<b>4.45</b>	V
UVLO Hysteresis			370		mV
Quiescent Supply Current	$V_{FB} = 1.5V$		1.4	<b>3</b>	mA
Shutdown Supply Current	SW = unconnected, $V_{EN} = 0V$		0.7	<b>2</b>	mA
<b>Reference</b>					
Feedback Reference Voltage	$0^\circ\text{C} \leq T_J \leq 85^\circ\text{C}$ ( $\pm 1.0\%$ )	<b>0.792</b>	0.8	<b>0.808</b>	V
	$-40^\circ\text{C} \leq T_J \leq 125^\circ\text{C}$ ( $\pm 1.5\%$ )	<b>0.788</b>	0.8	<b>0.812</b>	
FB Bias Current	$V_{FB} = 0.8V$		5	<b>500</b>	nA
<b>Enable Control</b>					
EN Logic Level High	$4.5V < V_{DD} < 5.5V$	<b>1.2</b>	0.85		V
EN Logic Level Low	$4.5V < V_{DD} < 5.5V$		0.78	<b>0.4</b>	V
EN Bias Current	$V_{EN} = 0V$		50	<b>100</b>	$\mu\text{A}$
<b>Oscillator</b>					
Switching Frequency <sup>(6)</sup>	MIC2176-1	<b>75</b>	100	<b>125</b>	kHz
	MIC2176-2	<b>150</b>	200	<b>250</b>	
	MIC2176-3	<b>225</b>	300	<b>375</b>	
Maximum Duty Cycle <sup>(7)</sup>	MIC2176-1, $V_{FB} = 0V$ , HSD=4V, $V_O = 3.3V$		96		%
	MIC2176-2, $V_{FB} = 0V$ , HSD=4V, $V_O = 3.3V$		93		
	MIC2176-3, $V_{FB} = 0V$ , HSD=4V, $V_O = 3.3V$		89		
Minimum Duty Cycle	$V_{FB} > 0.8V$		0		%
Minimum Off-Time			360		ns
Minimum On-Time			60		ns

## Electrical Characteristics<sup>(4)</sup> (Continued)

$V_{IN} = V_{HSD} = 48V$ ,  $V_{DD} = 5V$ ;  $V_{BST} - V_{SW} = 5V$ ;  $T_A = 25^\circ C$ , unless noted. **Bold** values indicate  $-40^\circ C \leq T_J \leq +125^\circ C$ .

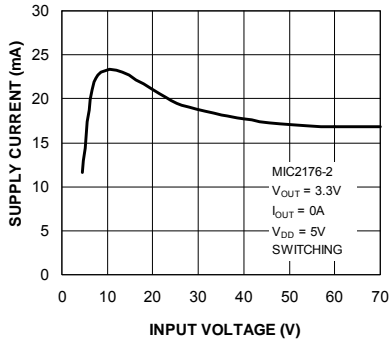
Parameter	Condition	Min.	Typ.	Max.	Units
<b>Soft Start</b>					
Soft-Start time			6		ms
<b>Short Circuit Protection</b>					
Current-Limit Threshold	$V_{FB} = 0.8V$	<b>103</b>	130	<b>162</b>	mV
Short-Circuit Threshold	$V_{FB} = 0V$	<b>19</b>	48	<b>77</b>	mV
<b>FET Drivers</b>					
DH, DL Output Low Voltage	$I_{SINK} = 10mA$			<b>0.1</b>	V
DH, DL Output High Voltage	$I_{SOURCE} = 10mA$	$V_{DD} - 0.1V$ Or $V_{BST} - 0.1V$			V
DH On-Resistance, High State			2.1	<b>3.3</b>	$\Omega$
DH On-Resistance, Low State			1.8	<b>3.3</b>	$\Omega$
DL On-Resistance, High State			1.8	<b>3.3</b>	$\Omega$
DL On-Resistance, Low State			1.2	<b>2.3</b>	$\Omega$
SW Leakage Current	$V_{SW} = 48V$ , $V_{DD} = 5V$ , $V_{BST} = 53V$			<b>55</b>	$\mu A$
HSD Leakage Current	$V_{SW} = 48V$ , $V_{DD} = 5V$ , $V_{BST} = 53V$			<b>55</b>	$\mu A$
<b>Thermal Protection</b>					
Over-Temperature Shutdown	$T_J$ Rising		160		$^\circ C$
Over-Temperature Shutdown Hysteresis			25		$^\circ C$

### Notes:

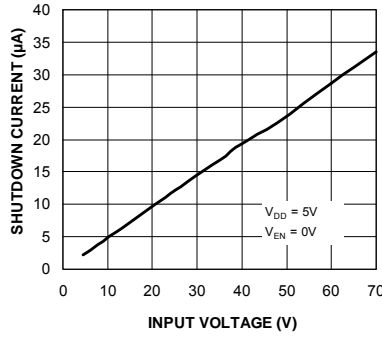
1. Exceeding the absolute maximum rating may damage the device.
2. Devices are ESD sensitive. Handling precautions recommended. Human body model, 1.5k $\Omega$  in series with 100pF.
3. The device is not guaranteed to function outside operating range.
4. Specification for packaged product only.
5. The application is fully functional at low  $V_{DD}$  (supply of the control section) if the external MOSFETs have enough low voltage  $V_{TH}$ .
6. Measured in test mode.
7. The maximum duty-cycle is limited by the fixed mandatory off-time  $t_{OFF}$  of typically 360ns.

# Typical Characteristics

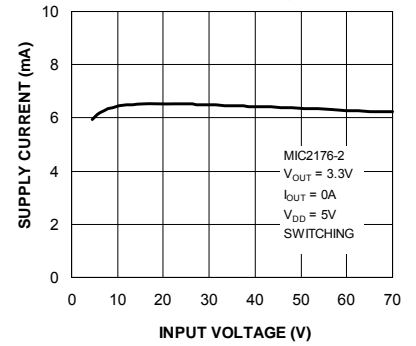
**V<sub>IN</sub> Operating Supply Current vs. Input Voltage**



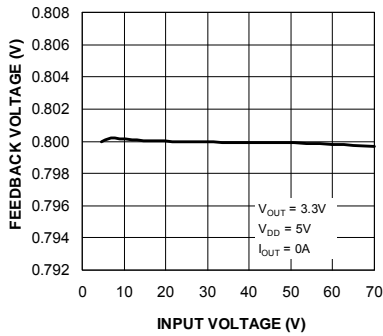
**V<sub>IN</sub> Shutdown Current vs. Input Voltage**



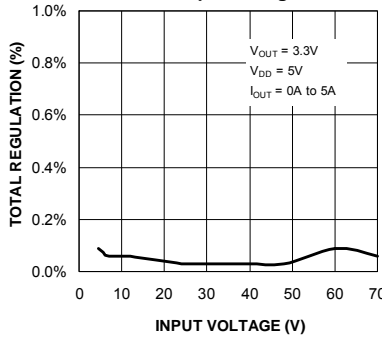
**V<sub>DD</sub> Operating Supply Current vs. Input Voltage**



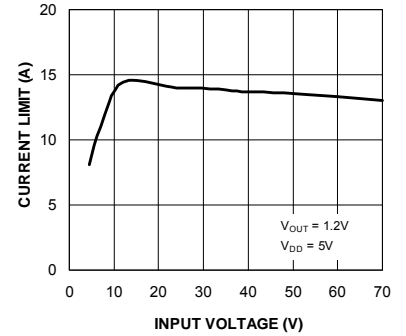
**Feedback Voltage vs. Input Voltage**



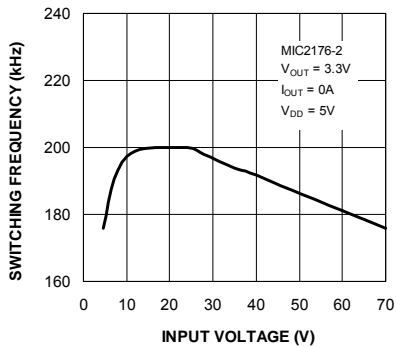
**Total Regulation vs. Input Voltage**



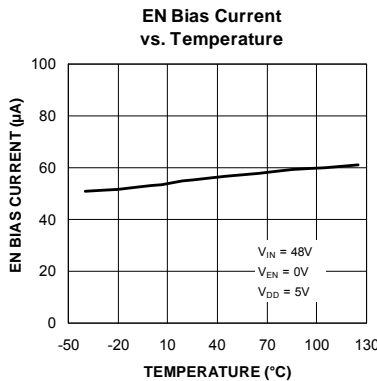
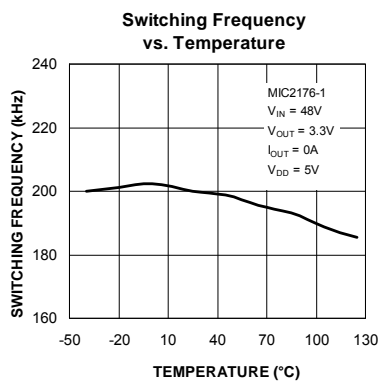
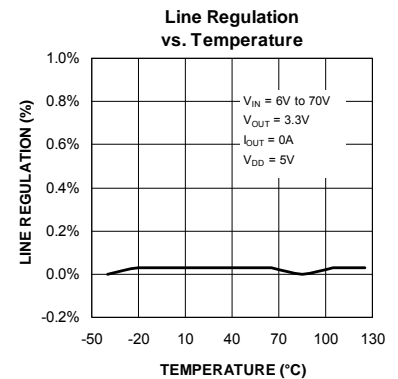
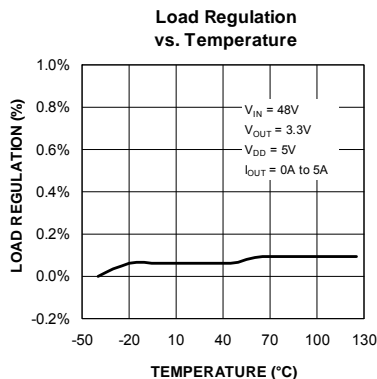
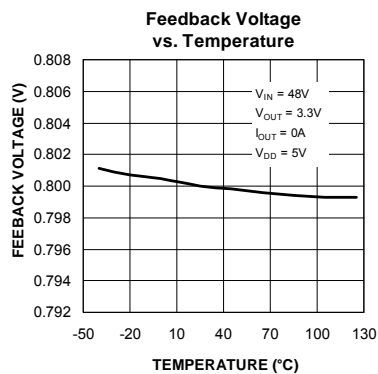
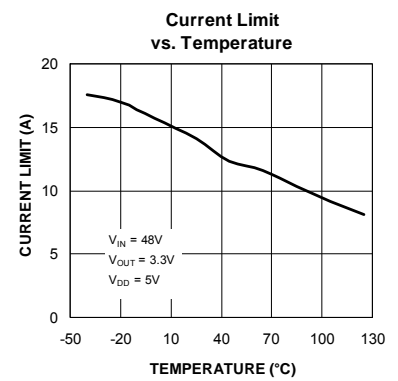
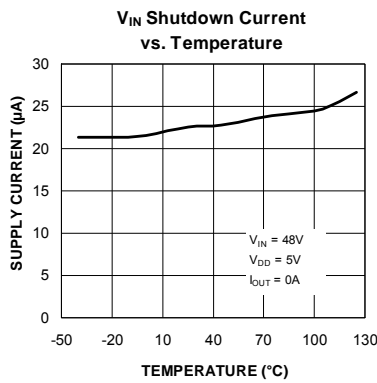
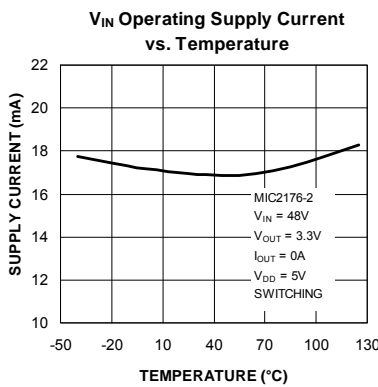
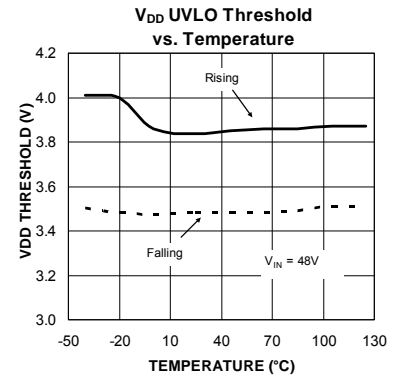
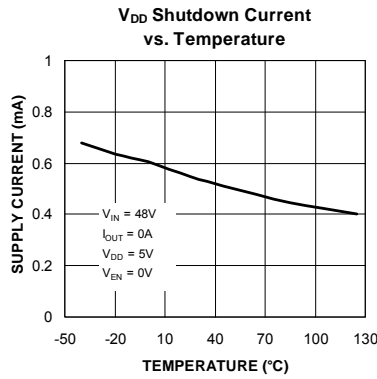
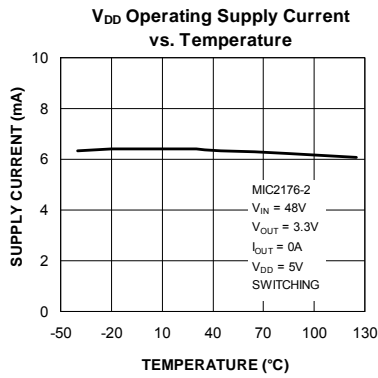
**Current Limit vs. Input Voltage**



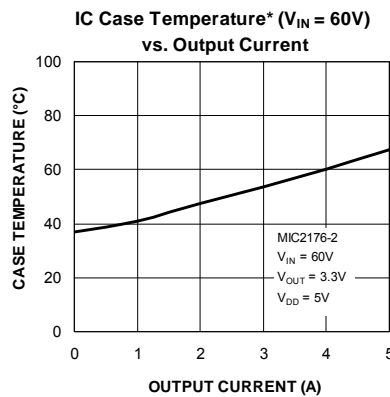
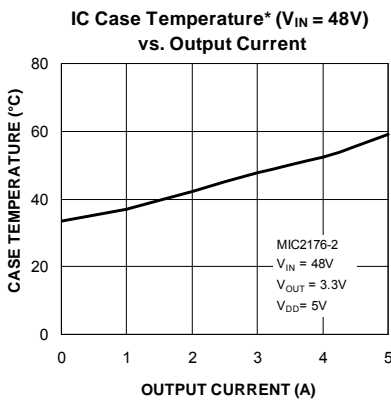
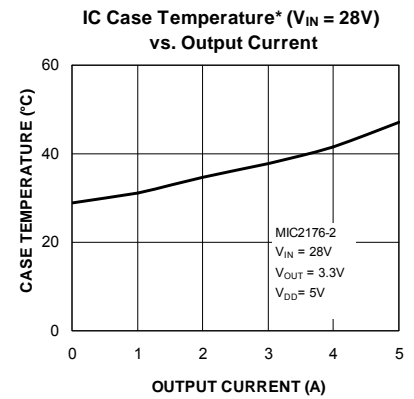
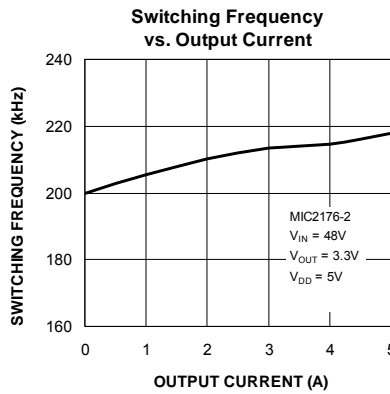
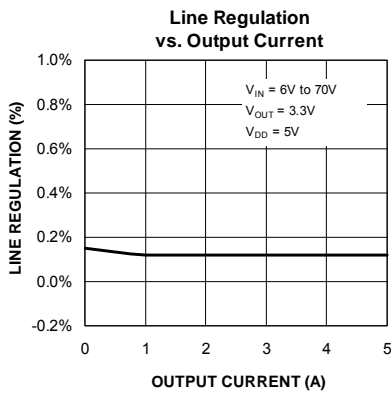
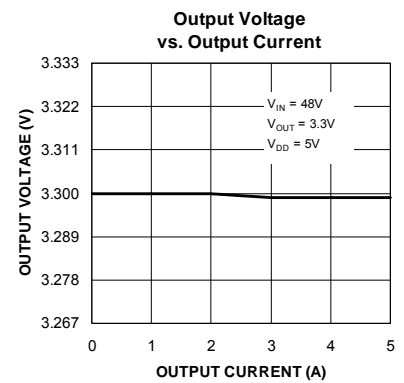
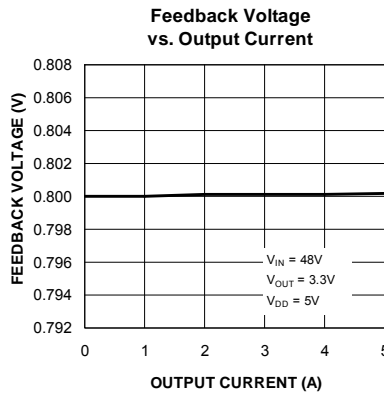
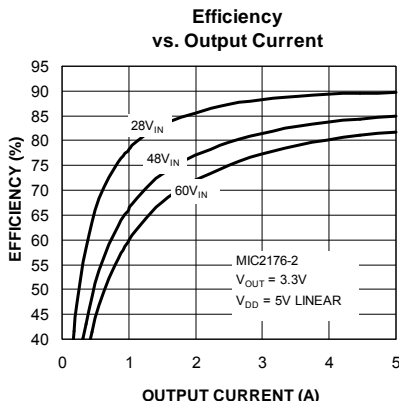
**Switching Frequency vs. Input Voltage**



# Typical Characteristics (Continued)



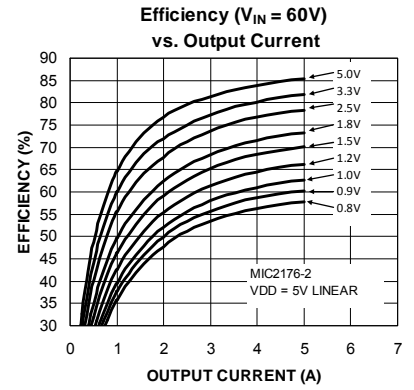
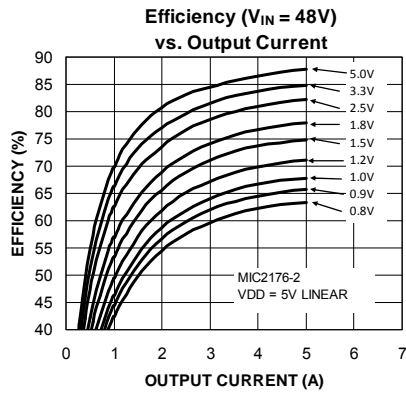
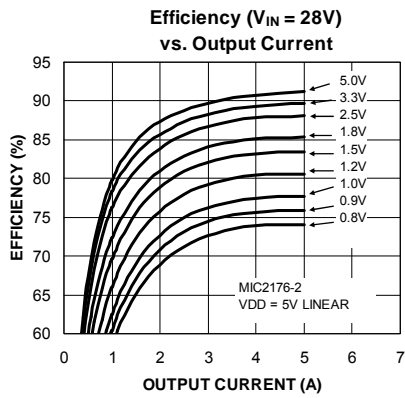
## Typical Characteristics (Continued)



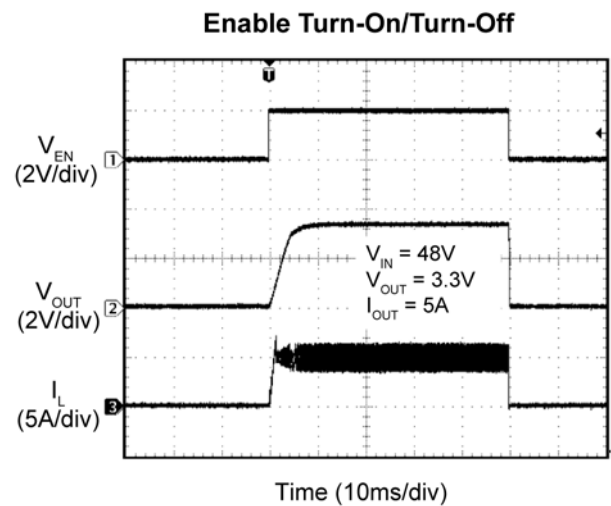
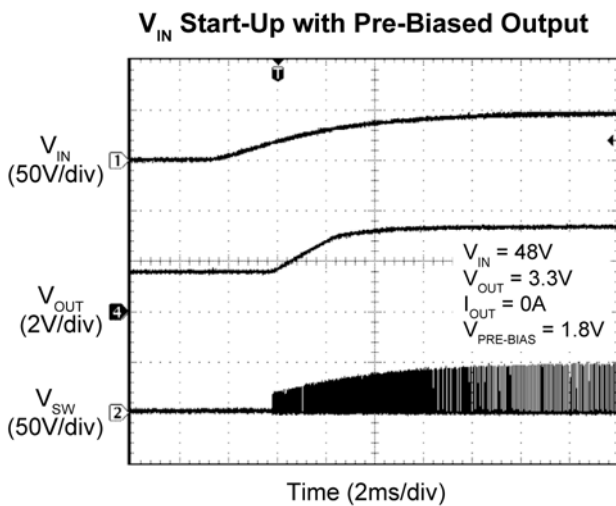
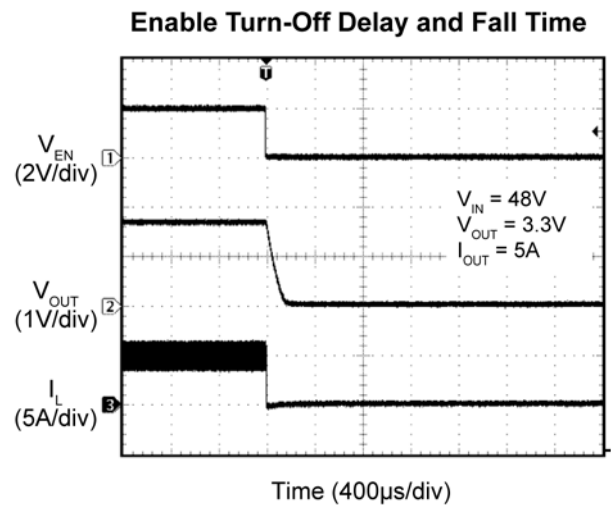
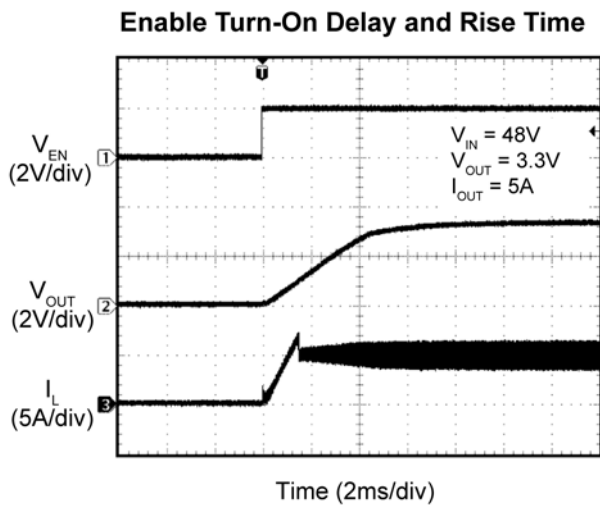
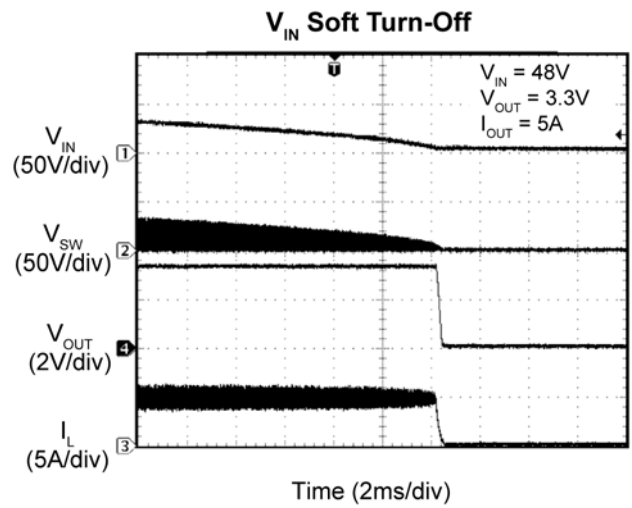
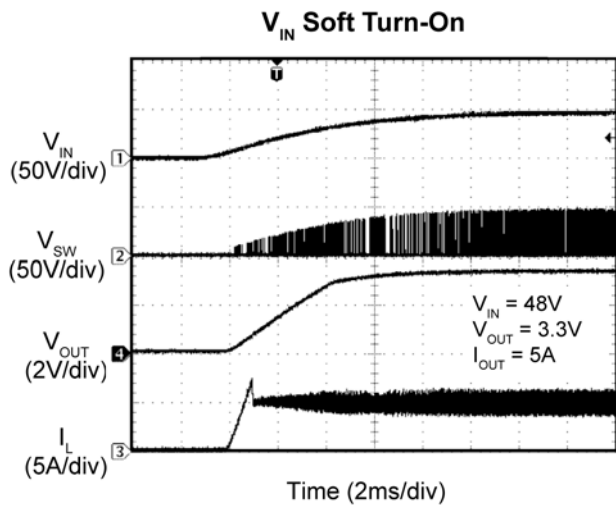
**Case Temperature\*** : The temperature measurement was taken at the hottest point on the MIC2176 case mounted on a 5 square inch PCB, see Thermal Measurement section. Actual results will depend upon the size of the PCB, ambient temperature and proximity to other heat emitting components.



### Typical Characteristics (Continued)

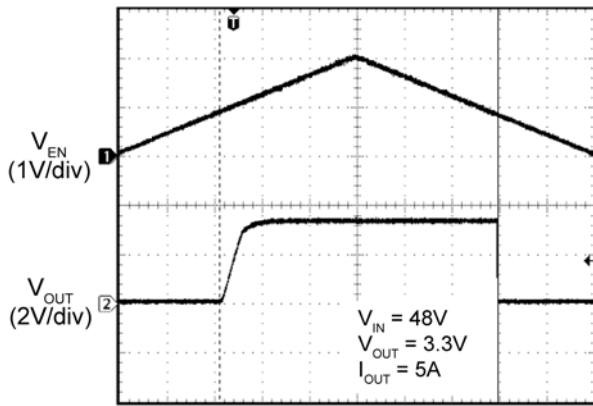


## Functional Characteristics



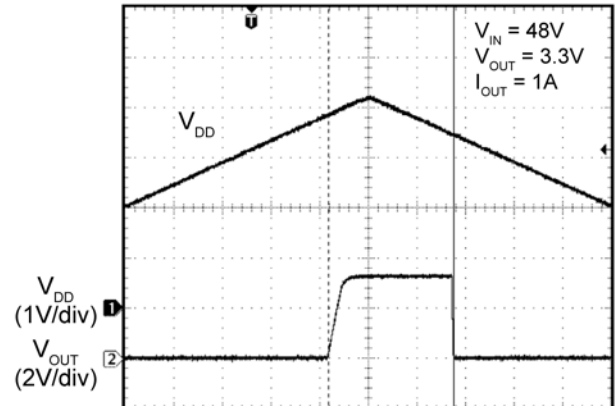
### Functional Characteristics (Continued)

**Enable Thresholds**



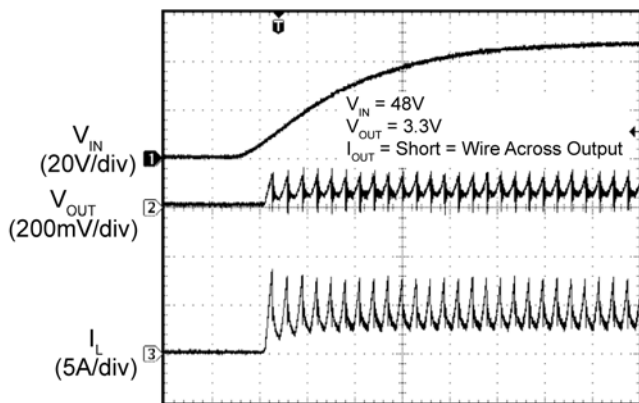
Time (10ms/div)

**$V_{DD}$  UVLO Thresholds**



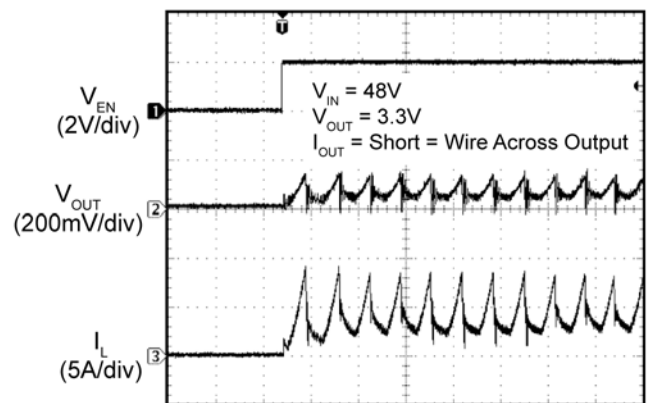
Time (20ms/div)

**Power-Up Into Short Circuit**



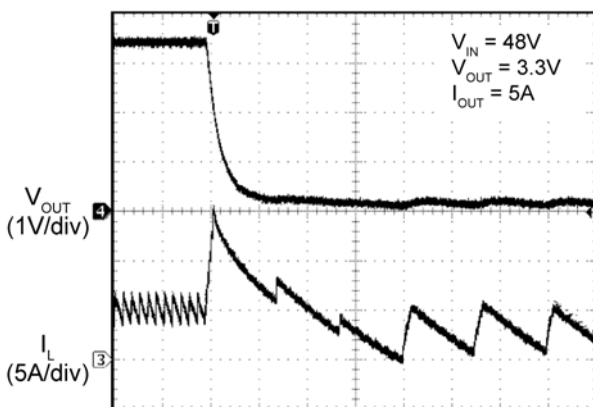
Time (2ms/div)

**Enabled Into Short Circuit**



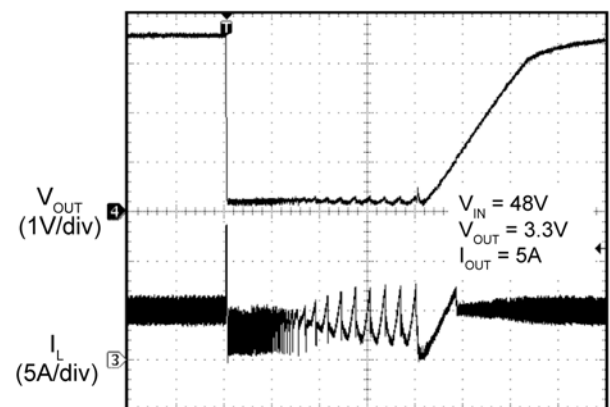
Time (1ms/div)

**Short Circuit**



Time (20 $\mu$ s/div)

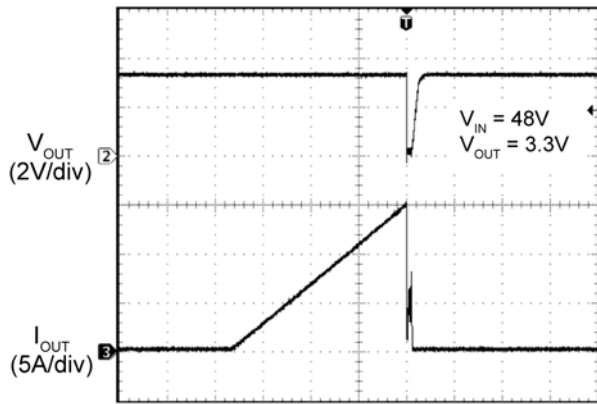
**Output Recovery from Short Circuit**



Time (2ms/div)

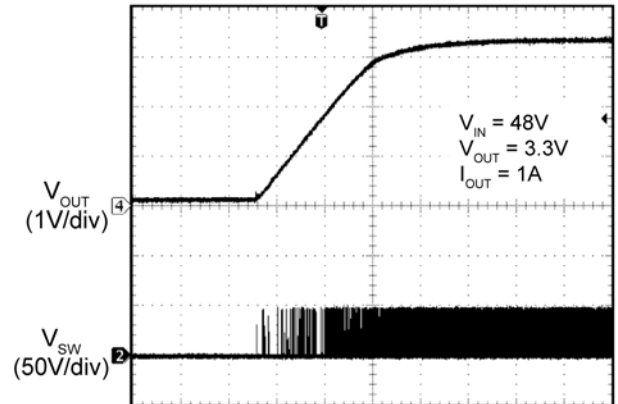
## Functional Characteristics (Continued)

**Peak Current-Limit Threshold**



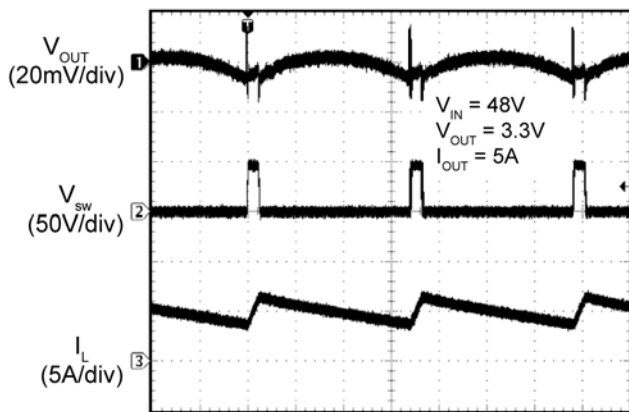
Time (40ms/div)

**Output Recovery from Thermal Shutdown**



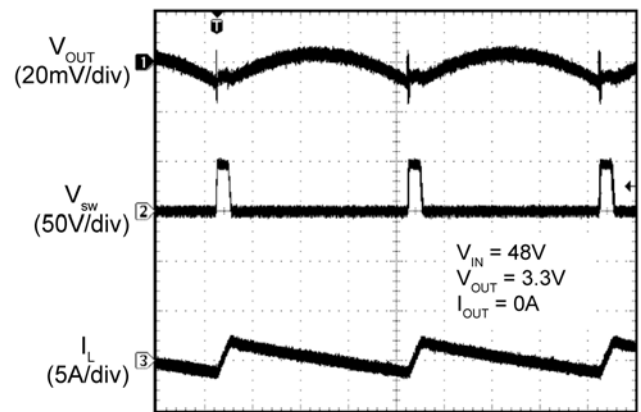
Time (2ms/div)

**Switching Waveforms:  $I_{OUT} = 5A$**



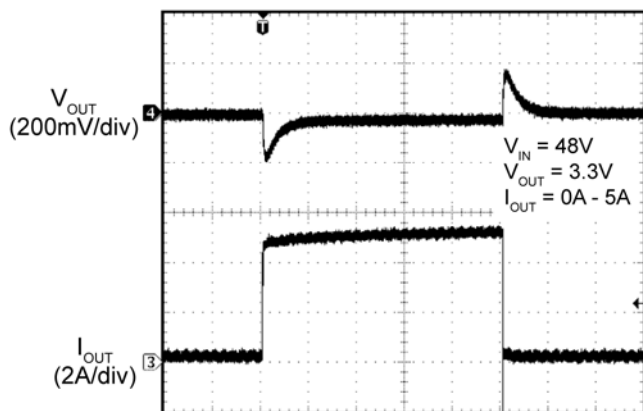
Time (1 $\mu$ s/div)

**Switching Waveforms:  $I_{OUT} = 0A$**



Time (1 $\mu$ s/div)

**Transient Response**



Time (200 $\mu$ s/div)

### Functional Diagram

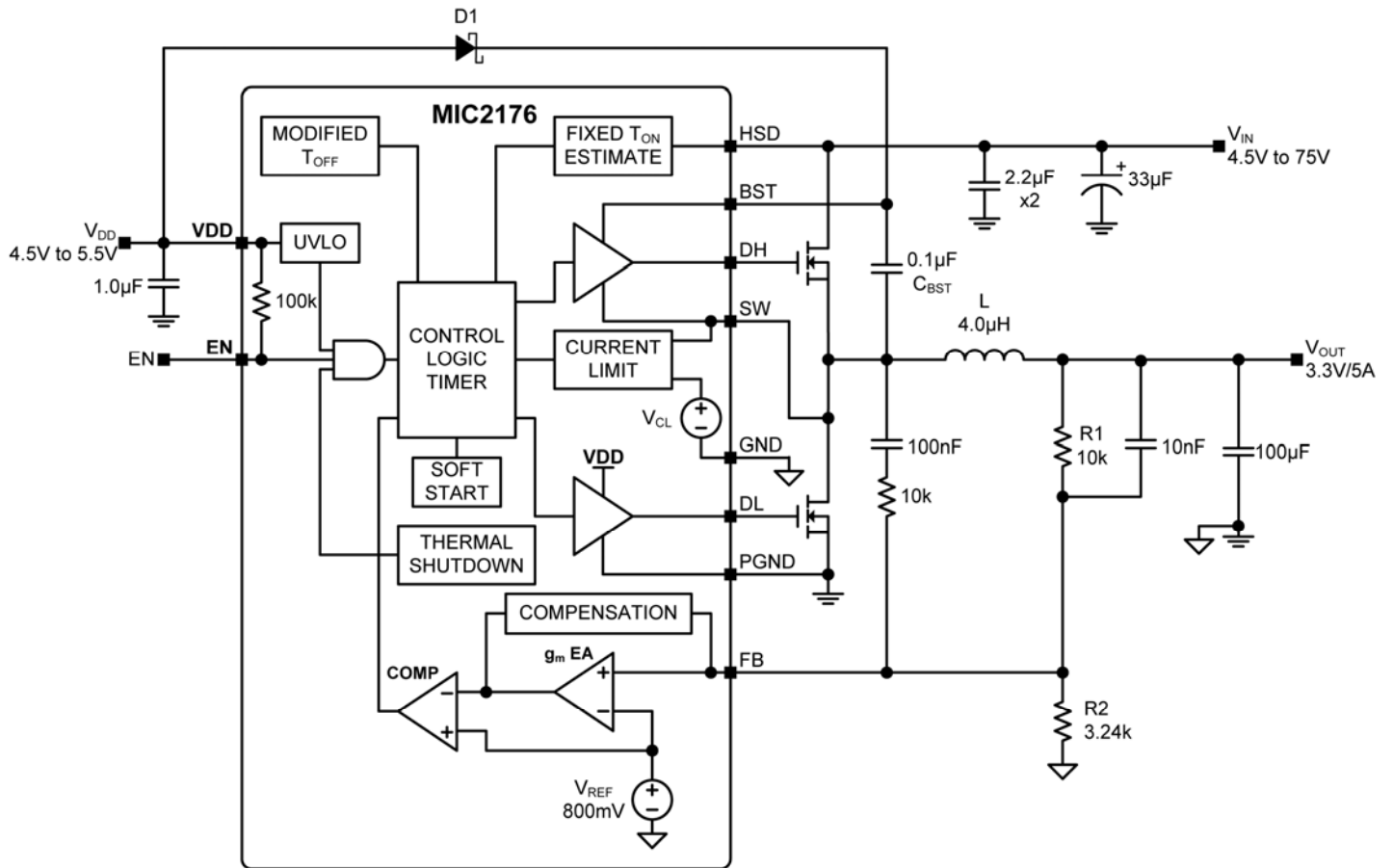


Figure 1. MIC2176 Functional Diagram

## Functional Description

The MIC2176 is an adaptive on-time synchronous buck controller family built for high-input voltage and low output voltage applications. It is designed to operate over a wide input voltage range from, 4.5V to 75V and the output is adjustable with an external resistive divider. A digitally modified adaptive on-time control scheme is employed in to obtain a constant switching frequency and to simplify the control compensation. Over-current protection is implemented by sensing low-side MOSFET's  $R_{DS(ON)}$ . The device features internal soft-start, enable, UVLO, and thermal shutdown.

### Theory of Operation

Figure 1 illustrates the block diagram of the MIC2176. The output voltage is sensed by the MIC2176 feedback pin FB via the voltage divider R1 and R2, and compared to a 0.8V reference voltage  $V_{REF}$  at the error comparator through a low-gain transconductance ( $g_m$ ) amplifier. If the feedback voltage decreases and the amplifier output is below 0.8V, then the error comparator will trigger the control logic and generate an ON-time period. The ON-time period length is predetermined by the "Fixed  $t_{ON}$  Estimator" circuitry:

$$t_{ON(estimated)} = \frac{V_{OUT}}{V_{IN} \times f_{SW}} \quad (1)$$

where  $V_{OUT}$  is the output voltage,  $V_{IN}$  is the power stage input voltage, and  $f_{SW}$  is the switching frequency (100kHz for MIC2176-1, 200kHz for MIC2176-2, and 300kHz for MIC2176-3).

At the end of the ON-time period, the internal high-side driver turns off the high-side MOSFET and the low-side driver turns on the low-side MOSFET. The OFF-time period length depends upon the feedback voltage in most cases. When the feedback voltage decreases and the output of the  $g_m$  amplifier is below 0.8V, the ON-time period is triggered and the OFF-time period ends. If the OFF-time period determined by the feedback voltage is less than the minimum OFF-time  $t_{OFF(min)}$ , which is about 360ns, the MIC2176 control logic will apply the  $t_{OFF(min)}$  instead.  $t_{OFF(min)}$  is required to maintain enough energy in the boost capacitor ( $C_{BST}$ ) to drive the high-side MOSFET.

The maximum duty cycle is obtained from the 360ns  $t_{OFF(min)}$ :

$$D_{max} = \frac{t_S - t_{OFF(min)}}{t_S} = 1 - \frac{360ns}{t_S} \quad (2)$$

where  $t_S = 1/f_{SW}$ . It is not recommended to use MIC2176 with a OFF-time close to  $t_{OFF(min)}$  during steady-state operation.

The adaptive ON-time control scheme results in a constant switching frequency in the MIC2176. The actual ON-time and resulting switching frequency will vary with the different rising and falling times of the external MOSFETs. Also, the minimum  $t_{ON}$  results in a lower switching frequency in high  $V_{IN}$  to  $V_{OUT}$  applications, such as 48V to 1.0V. The minimum  $t_{ON}$  measured on the MIC2176 evaluation board is about 60ns. During load transients, the switching frequency is changed due to the varying OFF-time.

To illustrate the control loop operation, we will analyze both the steady-state and load transient scenarios. For easy analysis, the gain of the  $g_m$  amplifier is assumed to be 1. With this assumption, the inverting input of the error comparator is the same as the feedback voltage.

Figure 2 shows the MIC2176 control loop timing during steady-state operation. During steady-state, the  $g_m$  amplifier senses the feedback voltage ripple, which is proportional to the output voltage ripple plus injected voltage ripple, to trigger the ON-time period. The ON-time is predetermined by the  $t_{ON}$  estimator. The termination of the OFF-time is controlled by the feedback voltage. At the valley of the feedback voltage ripple, which occurs when  $V_{FB}$  falls below  $V_{REF}$ , the OFF period ends and the next ON-time period is triggered through the control logic circuitry.

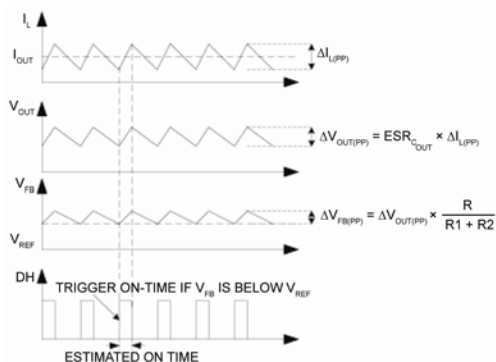


Figure 2. MIC2176 Control Loop Timing

Figure 3 shows the operation of the MIC2176 during a load transient. The output voltage drops due to the sudden load increase, which causes the  $V_{FB}$  to be less than  $V_{REF}$ . This will cause the error comparator to trigger an ON-time period. At the end of the ON-time period, a minimum OFF-time  $t_{OFF(min)}$  is generated to charge  $C_{BST}$  since the feedback voltage is still below  $V_{REF}$ . Then, the next ON-time period is triggered due to the low feedback voltage. Therefore, the switching frequency changes during the load transient, but returns to the nominal fixed frequency once the output has stabilized at the new load current level. With the varying duty cycle and switching frequency, the output recovery time is fast and the output voltage deviation is small in MIC2176 converter.

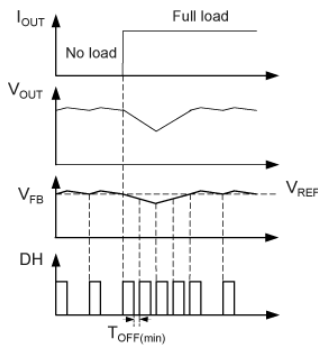


Figure 3. MIC2176 Load Transient Response

Unlike true current-mode control, the MIC2176 uses the output voltage ripple to trigger an ON-time period. The output voltage ripple is proportional to the inductor current ripple if the ESR of the output capacitor is large enough. The MIC2176 control loop has the advantage of eliminating the need for slope compensation.

In order to meet the stability requirements, the MIC2176 feedback voltage ripple should be in phase with the inductor current ripple and large enough to be sensed by the  $g_m$  amplifier and the error comparator. The recommended feedback voltage ripple is 20mV~100mV. If a low ESR output capacitor is selected, then the feedback voltage ripple may be too small to be sensed by the  $g_m$  amplifier and the error comparator. Also, the output voltage ripple and the feedback voltage ripple are not necessarily in phase with the inductor current ripple if the ESR of the output capacitor is very low. In these cases, ripple injection is required to ensure proper operation. Please refer to “Ripple Injection” subsection in *Application Information* for more details about the ripple injection technique.

**Soft-Start**

Soft-start reduces the power supply input surge current at startup by controlling the output voltage rise time. The input surge appears while the output capacitor is charged up. A slower output rise time will draw a lower input surge current.

The MIC2176 implements an internal digital soft-start by making the 0.8V reference voltage  $V_{REF}$  ramp from 0 to 100% in about 6ms with 9.7mV steps. Therefore, the output voltage is controlled to increase slowly by a staircase  $V_{FB}$  ramp. Once the soft-start cycle ends, the related circuitry is disabled to reduce current consumption.  $V_{DD}$  must be powered up at the same time or after  $V_{IN}$  to make the soft-start function correctly.

**Current Limit**

The MIC2176 uses the  $R_{DS(ON)}$  of the low-side power MOSFET to sense over-current conditions. This method will avoid adding cost, board space and power losses taken by discrete current sense resistors. The low-side MOSFET is used because it displays much lower parasitic oscillations during switching than the high-side MOSFET.

In each switching cycle of the MIC2176 converter, the inductor current is sensed by monitoring the low-side MOSFET in the OFF period. The sensed voltage is compared with a current-limit threshold voltage  $V_{CL}$  after a blanking time of 150ns. If the sensed voltage is over  $V_{CL}$ , which is 133mV typical at 0.8V  $V_{FB}$ , then the MIC2176 turns off the high-side and low-side MOSFETs and a soft-start sequence is triggered. This mode of operation is called “hiccup mode” and its purpose is to protect the downstream load in case of a hard short. The current limit threshold  $V_{CL}$  has a foldback characteristic related to the FB voltage. Please refer to the “Typical Characteristics” for the curve of current limit threshold vs. FB voltage percentage. The circuit in Figure 4 illustrates the MIC2176 current limiting circuit.

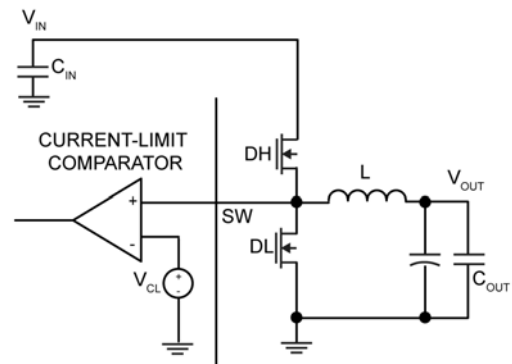


Figure 4. MIC2176 Current Limiting Circuit

Using the typical  $V_{CL}$  value of 130mV, the current-limit value is roughly estimated as:

$$I_{CL} \approx \frac{130\text{mV}}{R_{DS(ON)}} \quad (3)$$

For designs where the current ripple is significant compared to the load current  $I_{OUT}$ , or for low duty cycle operation, calculating the current limit  $I_{CL}$  should take into account that one is sensing the peak inductor current and that there is a blanking delay of approximately 150ns.

$$I_{CL} = \frac{130\text{mV}}{R_{DS(ON)}} + \frac{V_{OUT} \times T_{DLY}}{L} - \frac{\Delta I_{L(pp)}}{2} \quad (4)$$

$$\Delta I_{L(pp)} = \frac{V_{OUT} \times (1-D)}{f_{SW} \times L} \quad (5)$$

where

$V_{OUT}$  = The output voltage

$T_{DLY}$  = Current-limit blanking time, 150ns typical

$\Delta I_{L(pp)}$  = Inductor current ripple peak-to-peak value

$D$  = Duty Cycle

$f_{SW}$  = Switching frequency

The MOSFET  $R_{DS(ON)}$  varies 30% to 40% with temperature; therefore, it is recommended to add a 50% margin to  $I_{CL}$  in the above equation to avoid false current limiting due to increased MOSFET junction temperature rise. It is also recommended to connect SW pin directly to the drain of the low-side MOSFET to accurately sense the MOSFETs  $R_{DS(ON)}$ .

### MOSFET Gate Drive

The MIC2176 high-side drive circuit is designed to switch an N-Channel MOSFET. Figure 1 shows a bootstrap circuit, consisting of D1 (a Schottky diode is recommended) and  $C_{BST}$ . This circuit supplies energy to the high-side drive circuit. Capacitor  $C_{BST}$  is charged while the low-side MOSFET is on and the voltage on the SW pin is approximately 0V. When the high-side MOSFET driver is turned on, energy from  $C_{BST}$  is used to turn the MOSFET on. As the high-side MOSFET turns on, the voltage on the SW pin increases to approximately  $V_{IN}$ . Diode D1 is reverse biased and  $C_{BST}$  floats high while continuing to keep the high-side MOSFET on. The bias current of the high-side driver is less than 10mA so a 0.1 $\mu$ F to 1 $\mu$ F is sufficient to hold the gate voltage with minimal droop for the power stroke (high-side switching) cycle, i.e.  $\Delta BST = 10\text{mA} \times 3.33\mu\text{s}/0.1\mu\text{F} = 333\text{mV}$ . When the low-side MOSFET is turned back on,  $C_{BST}$  is recharged through D1. A small resistor  $R_G$ , which is in series with  $C_{BST}$ , can be used to slow down the turn-on time of the high-side N-channel MOSFET.

The drive voltage is derived from the  $V_{DD}$  supply voltage. The nominal low-side gate drive voltage is  $V_{DD}$  and the nominal high-side gate drive voltage is approximately  $V_{DD} - V_{DIODE}$ , where  $V_{DIODE}$  is the voltage drop across D1. An approximate 30ns delay between the high-side and low-side driver transitions is used to prevent current from simultaneously flowing unimpeded through both MOSFETs.



## Application Information

### MOSFET Selection

The MIC2176 controller works from power stage input voltages of 4.5V to 73V and has an external 4.5V to 5.5V  $V_{IN}$  to provide power to turn the external N-Channel power MOSFETs for the high- and low-side switches. For applications where  $V_{DD} < 5V$ , it is necessary that the power MOSFETs used are sub-logic level and are in full conduction mode for  $V_{GS}$  of 2.5V. For applications when  $V_{DD} > 5V$ ; logic-level MOSFETs, whose operation is specified at  $V_{GS} = 4.5V$  must be used.

There are different criteria for choosing the high-side and low-side MOSFETs. These differences are more significant at lower duty cycles. In such an application, the high-side MOSFET is required to switch as quickly as possible to minimize transition losses, whereas the low-side MOSFET can switch slower, but must handle larger RMS currents. When the duty cycle approaches 50%, the current carrying capability of the high-side MOSFET starts to become critical.

It is important to note that the on-resistance of a MOSFET increases with increasing temperature. A 75°C rise in junction temperature will increase the channel resistance of the MOSFET by 50% to 75% of the resistance specified at 25°C. This change in resistance must be accounted for when calculating MOSFET power dissipation and in calculating the value of current limit. Total gate charge is the charge required to turn the MOSFET on and off under specified operating conditions ( $V_{DS}$  and  $V_{GS}$ ). The gate charge is supplied by the MIC2176 gate-drive circuit. At 300kHz switching frequency, the gate charge can be a significant source of power dissipation in the MIC2176. At low output load, this power dissipation is noticeable as a reduction in efficiency. The average current required to drive the high-side MOSFET is:

$$I_{G[\text{high-side}]}(\text{avg}) = Q_G \times f_{SW} \quad (6)$$

where:

$I_{G[\text{high-side}]}(\text{avg})$  = Average high-side MOSFET gate current

$Q_G$  = Total gate charge for the high-side MOSFET taken from the manufacturer's data sheet for  $V_{GS} = V_{DD}$ .

$f_{SW}$  = Switching Frequency

The low-side MOSFET is turned on and off at  $V_{DS} = 0$  because an internal body diode or external freewheeling diode is conducting during this time. The switching loss for the low-side MOSFET is usually negligible. Also, the gate-drive current for the low-side MOSFET is more

accurately calculated using  $C_{ISS}$  at  $V_{DS} = 0$  instead of gate charge.

For the low-side MOSFET:

$$I_{G[\text{low-side}]}(\text{avg}) = C_{ISS} \times V_{GS} \times f_{SW} \quad (7)$$

Since the current from the gate drive comes from the  $V_{DD}$ , the power dissipated in the MIC2176 due to gate drive is:

$$P_{\text{GATEDRIVE}} = V_{DD} \times (I_{G[\text{high-side}]}(\text{avg}) + I_{G[\text{low-side}]}(\text{avg})) \quad (8)$$

A convenient figure of merit for switching MOSFETs is the on resistance times the total gate charge  $R_{DS(\text{ON})} \times Q_G$ . Lower numbers translate into higher efficiency. Low gate-charge logic-level MOSFETs are a good choice for use with the MIC2176. Also, the  $R_{DS(\text{ON})}$  of the low-side MOSFET will determine the current-limit value. Please refer to "Current Limit" subsection in *Functional Description* for more details.

Parameters that are important to MOSFET switch selection are:

- Voltage rating
- On-resistance
- Total gate charge

The voltage ratings for the high-side and low-side MOSFETs are essentially equal to the power stage input voltage  $V_{HSD}$ . A safety factor of 20% should be added to the  $V_{DS(\text{max})}$  of the MOSFETs to account for voltage spikes due to circuit parasitic elements.

The power dissipated in the MOSFETs is the sum of the conduction losses during the on-time ( $P_{\text{CONDUCTION}}$ ) and the switching losses during the period of time when the MOSFETs turn on and off ( $P_{AC}$ ).

$$P_{SW} = P_{\text{CONDUCTION}} + P_{AC} \quad (9)$$

$$P_{\text{CONDUCTION}} = I_{SW(\text{RMS})}^2 \times R_{DS(\text{ON})} \quad (10)$$

$$P_{AC} = P_{AC(\text{off})} + P_{AC(\text{on})} \quad (11)$$

where:

$R_{DS(\text{ON})}$  = On-resistance of the MOSFET switch

$D$  = Duty Cycle =  $V_{OUT} / V_{HSD}$

Making the assumption that the turn-on and turn-off transition times are equal; the transition times can be approximated by:

$$t_T = \frac{C_{ISS} \times V_{IN} + C_{OSS} \times V_{HSD}}{I_G} \quad (12)$$

where:

$C_{ISS}$  and  $C_{OSS}$  are measured at  $V_{DS} = 0$

$I_G$  = Gate-drive current

The total high-side MOSFET switching loss is:

$$P_{AC} = (V_{HSD} + V_D) \times I_{PK} \times t_T \times f_{SW} \quad (13)$$

where:

$t_T$  = Switching transition time

$V_D$  = Body diode drop (0.5V)

$f_{SW}$  = Switching Frequency

The high-side MOSFET switching losses increase with the switching frequency and the input voltage  $V_{HSD}$ . The low-side MOSFET switching losses are negligible and can be ignored for these calculations.

### Inductor Selection

Values for inductance, peak, and RMS currents are required to select the output inductor. The input and output voltages and the inductance value determine the peak-to-peak inductor ripple current. Generally, higher inductance values are used with higher input voltages. Larger peak-to-peak ripple currents will increase the power dissipation in the inductor and MOSFETs. Larger output ripple currents will also require more output capacitance to smooth out the larger ripple current. Smaller peak-to-peak ripple currents require a larger inductance value and therefore a larger and more expensive inductor.

A good compromise between size, loss and cost is to set the inductor ripple current to be equal to 20% of the maximum output current.

The inductance value is calculated by Equation 14:

$$L = \frac{V_{OUT} \times (V_{IN(max)} - V_{OUT})}{V_{IN(max)} \times f_{sw} \times 20\% \times I_{OUT(max)}} \quad (14)$$

where:

$f_{SW}$  = Switching frequency, 300kHz

20% = Ratio of AC ripple current to DC output current

$V_{IN(max)}$  = Maximum power stage input voltage

The peak-to-peak inductor current ripple is:

$$\Delta I_{L(pp)} = \frac{V_{OUT} \times (V_{IN(max)} - V_{OUT})}{V_{IN(max)} \times f_{sw} \times L} \quad (15)$$

The peak inductor current is equal to the average output current plus one half of the peak-to-peak inductor current ripple.

$$I_{L(pk)} = I_{OUT(max)} + 0.5 \times \Delta I_{L(pp)} \quad (16)$$

The RMS inductor current is used to calculate the  $I^2R$  losses in the inductor.

$$I_{L(RMS)} = \sqrt{I_{OUT(max)}^2 + \frac{\Delta I_{L(pp)}^2}{12}} \quad (17)$$

Maximizing efficiency requires the proper selection of core material and minimizing the winding resistance. The high frequency operation of the MIC2176 requires the use of ferrite materials for all but the most cost sensitive applications. Lower cost iron powder cores may be used but the increase in core loss will reduce the efficiency of the power supply. This is especially noticeable at low output power. The winding resistance decreases efficiency at the higher output current levels. The winding resistance must be minimized although this usually comes at the expense of a larger inductor. The power dissipated in the inductor is equal to the sum of the core and copper losses. At higher output loads, the core losses are usually insignificant and can be ignored. At lower output currents, the core losses can be a significant contributor. Core loss information is usually available from the magnetics vendor.

Copper loss in the inductor is calculated by Equation 18:

$$P_{\text{INDUCTOR(Cu)}} = I_{L(\text{RMS})}^2 \times R_{\text{WINDING}} \quad (18)$$

The resistance of the copper wire,  $R_{\text{WINDING}}$ , increases with the temperature. The value of the winding resistance used should be at the operating temperature.

$$P_{\text{WINDING(Ht)}} = R_{\text{WINDING}(20^\circ\text{C})} \times (1 + 0.0042 \times (T_{\text{H}} - T_{20^\circ\text{C}})) \quad (19)$$

where:

$T_{\text{H}}$  = temperature of wire under full load

$T_{20^\circ\text{C}}$  = ambient temperature

$R_{\text{WINDING}(20^\circ\text{C})}$  = room temperature winding resistance (usually specified by the manufacturer)

### Output Capacitor Selection

The type of the output capacitor is usually determined by its ESR (equivalent series resistance). Voltage and RMS current capability are two other important factors for selecting the output capacitor. Recommended capacitor types are tantalum, low-ESR aluminum electrolytic, OS-CON and POSCAP. The output capacitor's ESR is usually the main cause of the output ripple. The output capacitor ESR also affects the control loop from a stability point of view. The maximum value of ESR is calculated:

$$\text{ESR}_{\text{C}_{\text{OUT}}} \leq \frac{\Delta V_{\text{OUT(pp)}}}{\Delta I_{L(\text{PP})}} \quad (20)$$

where:

$\Delta V_{\text{OUT(pp)}}$  = peak-to-peak output voltage ripple

$\Delta I_{L(\text{PP})}$  = peak-to-peak inductor current ripple

The total output ripple is a combination of the ESR and output capacitance. The total ripple is calculated in Equation 21:

$$\Delta V_{\text{OUT(pp)}} = \sqrt{\left(\frac{\Delta I_{L(\text{PP})}}{\text{C}_{\text{OUT}} \times f_{\text{SW}} \times 8}\right)^2 + (\Delta I_{L(\text{PP})} \times \text{ESR}_{\text{C}_{\text{OUT}}})^2} \quad (21)$$

where:

D = duty cycle

$\text{C}_{\text{OUT}}$  = output capacitance value

$f_{\text{sw}}$  = switching frequency

As described in the "Theory of Operation" subsection in *Functional Description*, the MIC2176 requires at least 20mV peak-to-peak ripple at the FB pin to make the  $g_m$  amplifier and the error comparator behave properly. Also, the output voltage ripple should be in phase with the inductor current. Therefore, the output voltage ripple caused by the output capacitors value should be much smaller than the ripple caused by the output capacitor ESR. If low ESR capacitors, such as ceramic capacitors, are selected as the output capacitors, a ripple injection method should be applied to provide the enough feedback voltage ripple. Please refer to the "Ripple Injection" subsection for more details.

The voltage rating of the capacitor should be twice the output voltage for a tantalum and 20% greater for aluminum electrolytic or OS-CON. The output capacitor RMS current is calculated in Equation 22:

$$I_{\text{C}_{\text{OUT}}(\text{RMS})} = \frac{\Delta I_{L(\text{PP})}}{\sqrt{12}} \quad (22)$$

The power dissipated in the output capacitor is:

$$P_{\text{DISS(C}_{\text{OUT}})}} = I_{\text{C}_{\text{OUT}}(\text{RMS})}^2 \times \text{ESR}_{\text{C}_{\text{OUT}}} \quad (23)$$

### Input Capacitor Selection

The input capacitor for the power stage input  $V_{\text{IN}}$  should be selected for ripple current rating and voltage rating. Tantalum input capacitors may fail when subjected to high inrush currents, caused by turning the input supply on. A tantalum input capacitor's voltage rating should be at least two times the maximum input voltage to maximize reliability. Aluminum electrolytic, OS-CON, and multilayer polymer film capacitors can handle the higher inrush currents without voltage de-rating. The input voltage ripple will primarily depend on the input capacitor's ESR. The peak input current is equal to the peak inductor current, so:

$$\Delta V_{\text{IN}} = I_{L(\text{pk})} \times \text{ESR}_{\text{C}_{\text{IN}}} \quad (24)$$

The input capacitor must be rated for the input current ripple. The RMS value of input capacitor current is determined at the maximum output current. Assuming the peak-to-peak inductor current ripple is low:

$$I_{CIN(RMS)} \approx I_{OUT(max)} \times \sqrt{D \times (1-D)} \quad (25)$$

The power dissipated in the input capacitor is:

$$P_{DISS(CIN)} = I_{CIN(RMS)}^2 \times ESR_{CIN} \quad (26)$$

### Voltage Setting Components

The MIC2176 requires two resistors to set the output voltage as shown in Figure 5:

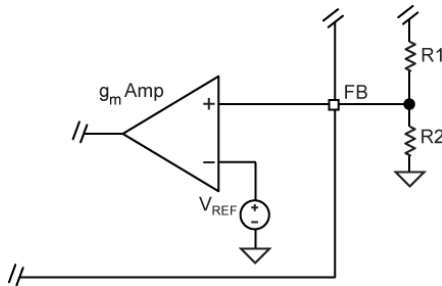


Figure 5. Voltage-Divider Configuration

The output voltage is determined by the equation:

$$V_{OUT} = V_{FB} \times \left(1 + \frac{R1}{R2}\right) \quad (27)$$

where,  $V_{FB} = 0.8V$ . A typical value of R1 can be between 3kΩ and 10kΩ. If R1 is too large, it may allow noise to be introduced into the voltage feedback loop. If R1 is too small in value, it will decrease the efficiency of the power supply, especially at light loads. Once R1 is selected, R2 can be calculated using:

$$R2 = \frac{V_{FB} \times R1}{V_{OUT} - V_{FB}} \quad (28)$$

### Ripple Injection

The  $V_{FB}$  ripple required for proper operation of the MIC2176  $g_m$  amplifier and error comparator is 20mV to 100mV. However, the output voltage ripple is generally designed as 1% to 2% of the output voltage. For a low output voltage, such as a 1V, the output voltage ripple is only 10mV to 20mV, and the feedback voltage ripple is

less than 20mV. If the feedback voltage ripple is so small that the  $g_m$  amplifier and error comparator can't sense it, then the MIC2176 will lose control and the output voltage is not regulated. In order to have some amount of  $V_{FB}$  ripple, a ripple injection method is applied for low output voltage ripple applications.

The applications are divided into three situations according to the amount of the feedback voltage ripple:

1. Enough ripple at the feedback voltage due to the large ESR of the output capacitors.

As shown in Figure 6a, the converter is stable without any ripple injection. The feedback voltage ripple is:

$$\Delta V_{FB(pp)} = \frac{R2}{R1 + R2} \times ESR_{C_{OUT}} \times \Delta I_{L(pp)} \quad (29)$$

where  $\Delta I_{L(pp)}$  is the peak-to-peak value of the inductor current ripple.

2. Inadequate ripple at the feedback voltage due to the small ESR of the output capacitors.

The output voltage ripple is fed into the FB pin through a feedforward capacitor  $C_{ff}$  in this situation, as shown in Figure 6b. The typical  $C_{ff}$  value is between 1nF and 100nF. With the feedforward capacitor, the feedback voltage ripple is very close to the output voltage ripple:

$$\Delta V_{FB(pp)} \approx ESR \times \Delta I_{L(pp)} \quad (30)$$

3. Virtually no ripple at the FB pin voltage due to the very-low ESR of the output capacitors:

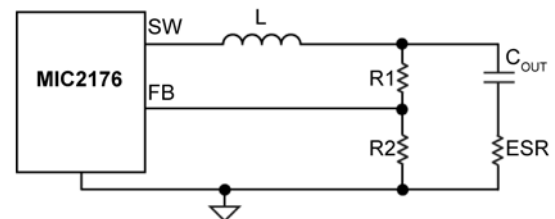


Figure 6a. Enough Ripple at FB

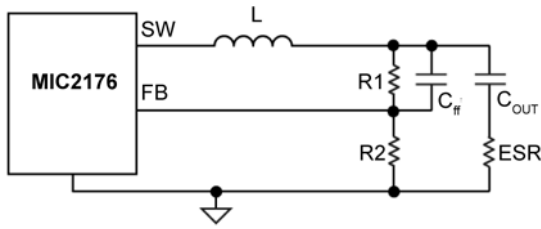


Figure 6b. Inadequate Ripple at FB

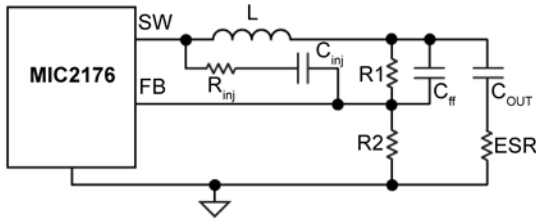


Figure 6c. Invisible Ripple at FB

In this situation, the output voltage ripple is less than 20mV. Therefore, additional ripple is injected into the FB pin from the switching node SW via a resistor  $R_{inj}$  and a capacitor  $C_{inj}$ , as shown in Figure 6c. The injected ripple is:

$$\Delta V_{FB(pp)} = V_{IN} \times K_{div} \times D \times (1-D) \times \frac{1}{f_{SW} \times \tau} \quad (31)$$

$$K_{div} = \frac{R1//R2}{R_{inj} + R1//R2} \quad (32)$$

where:

$V_{IN}$  = Power stage input voltage

$D$  = Duty cycle

$f_{SW}$  = Switching frequency

$\tau = (R1//R2//R_{inj}) \times C_{ff}$

In Equations 21 and 22, it is assumed that the time constant associated with  $C_{ff}$  must be much greater than the switching period:

$$\frac{1}{f_{SW} \times \tau} = \frac{T}{\tau} \ll 1 \quad (33)$$

If the voltage divider resistors  $R1$  and  $R2$  are in the  $k\Omega$  range, a  $C_{ff}$  of 1nF to 100nF can easily satisfy the large time constant requirements. Also, a 100nF injection capacitor  $C_{inj}$  is used in order to be considered as short for a wide range of the frequencies.

The process of sizing the ripple injection resistor and capacitors is:

**Step 1.** Select  $C_{ff}$  to feed all output ripples into the feedback pin and make sure the large time constant assumption is satisfied. Typical choice of  $C_{ff}$  is 1nF to 100nF if  $R1$  and  $R2$  are in  $k\Omega$  range.

**Step 2.** Select  $R_{inj}$  according to the expected feedback voltage ripple using Equation 24:

$$K_{div} = \frac{\Delta V_{FB(pp)}}{V_{IN}} \times \frac{f_{SW} \times \tau}{D \times (1-D)} \quad (34)$$

Then the value of  $R_{inj}$  is obtained as:

$$R_{inj} = (R1//R2) \times \left( \frac{1}{K_{div}} - 1 \right) \quad (35)$$

**Step 3.** Select  $C_{inj}$  as 100nF, which could be considered as short for a wide range of the frequencies.

## PCB Layout Guidelines

**Warning!!! To minimize EMI and output noise, follow these layout recommendations.**

PCB Layout is critical to achieve reliable, stable and efficient performance. A ground plane is required to control EMI and minimize the inductance in power, signal and return paths.

The following guidelines should be followed to insure proper operation of the MIC2176 converter.

### IC

- The 1 $\mu$ F ceramic capacitor, which is connected to the VDD pin, must be located right at the IC. The VDD pin is very noise sensitive and placement of the capacitor is very critical. Use wide traces to connect to the VDD and PGND pins.
- The signal ground pin (GND) must be connected directly to the ground planes. Do not route the GND pin to the PGND pin on the top layer.
- Place the IC close to the point of load (POL).
- Use fat traces to route the input and output power lines.
- Signal and power grounds should be kept separate and connected at only one location.

### Input Capacitor

- Place the input capacitor next.
- Place the input capacitors on the same side of the board and as close to the MOSFETs as possible.
- Place several vias to the ground plane close to the input capacitor ground terminal.
- Use either X7R or X5R dielectric input capacitors. Do not use Y5V or Z5U type capacitors.
- Do not replace the ceramic input capacitor with any other type of capacitor. Any type of capacitor can be placed in parallel with the input capacitor.
- If a Tantalum input capacitor is placed in parallel with the input capacitor, it must be recommended for switching regulator applications and the operating voltage must be derated by 50%.
- In "Hot-Plug" applications, a Tantalum or Electrolytic bypass capacitor must be used to limit the over-voltage spike seen on the input supply with power is suddenly applied.

### RC Snubber

- Place the RC snubber on the same side of the board and as close to the SW pin as possible.

### Inductor

- Keep the inductor connection to the switch node (SW) short.
- Do not route any digital lines underneath or close to the inductor.
- Keep the switch node (SW) away from the feedback (FB) pin.
- The SW pin should be connected directly to the drain of the low-side MOSFET to accurately sense the voltage across the low-side MOSFET.
- To minimize noise, place a ground plane underneath the inductor.

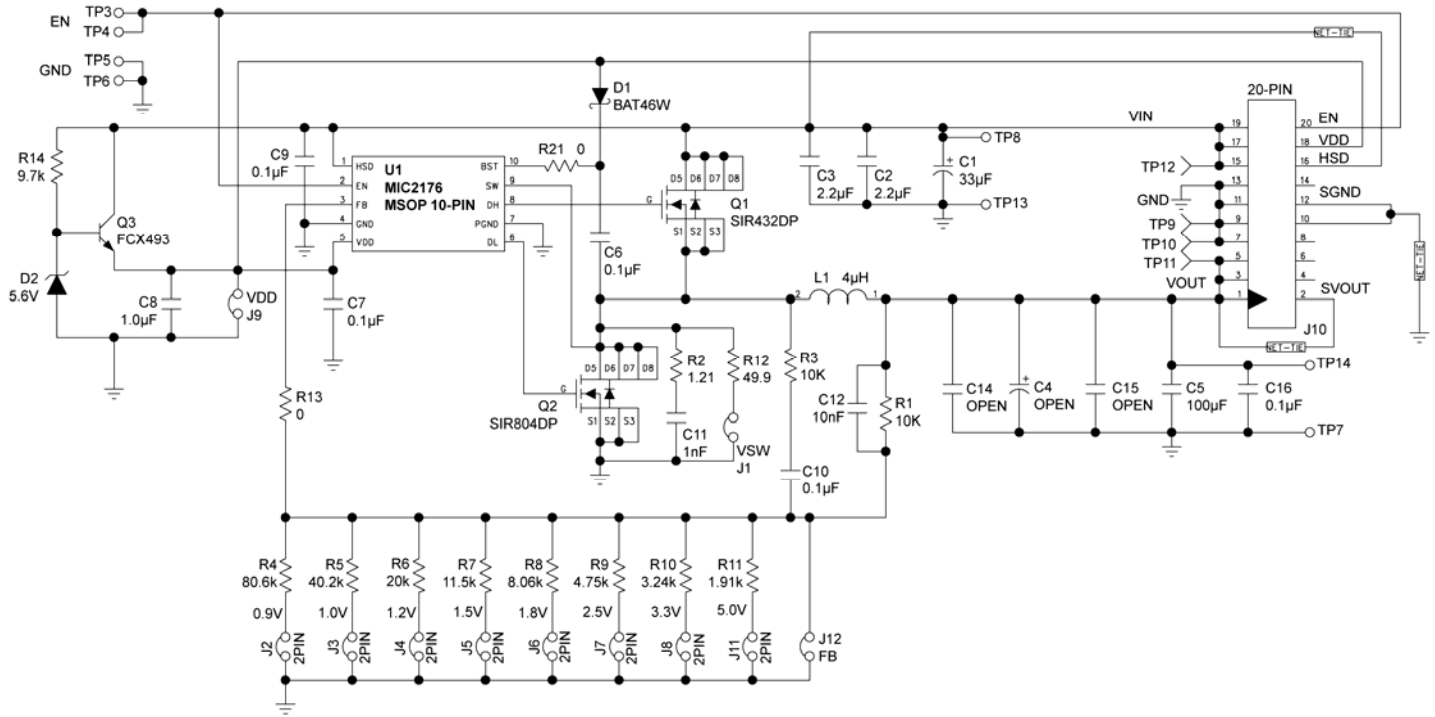
### Output Capacitor

- Use a wide trace to connect the output capacitor ground terminal to the input capacitor ground terminal.
- Phase margin will change as the output capacitor value and ESR changes. Contact the factory if the output capacitor is different from what is shown in the BOM.
- The feedback trace should be separate from the power trace and connected as close as possible to the output capacitor. Sensing a long high-current load trace can degrade the DC load regulation.

### MOSFETs

- Low-side MOSFET gate drive trace (DL pin to MOSFET gate pin) must be short and routed over a ground plane. The ground plane should be the connection between the MOSFET source and PGND.
- Choose a low-side MOSFET with a high  $C_{GS}/C_{GD}$  ratio and a low internal gate resistance to minimize the effect of  $dv/dt$  inducted turn-on.
- Do not put a resistor between the Low-side MOSFET gate drive output and the gate.
- Use a 4.5V  $V_{GS}$  rated MOSFET. Its higher gate threshold voltage is more immune to glitches than a 2.5V or 3.3V rated MOSFET. MOSFETs that are rated for operation at less than 4.5V  $V_{GS}$  should not be used.

### Evaluation Board Schematic



**Figure 7. Schematic of MIC2176 Evaluation Board**  
 (J1, J9, J12, R12, and R13 are for testing purposes)

**Bill of Materials**

Item	Part Number	Manufacturer	Description	Qty
C1	B41125A9336M	EPCOS <sup>(1)</sup>	33 $\mu$ F Aluminum Capacitor, SMD, 100V	1
C2, C3	GRM32ER72A225K	Murata <sup>(2)</sup>	2.2 $\mu$ F/100V Ceramic Capacitor, X7R, Size 1210	2
C4	6SEPC470M	Sanyo <sup>(3)</sup>	470 $\mu$ F/6.3V OSCON Capacitor	1
C5, C15	GRM32ER60J104KA94D	Murata <sup>(2)</sup>	100 $\mu$ F/6.3V Ceramic Capacitor, X7R, Size 1210	2
C6, C7, C16	GRM188R71H104KA94L	Murata <sup>(2)</sup>	0.1 $\mu$ F/6.3V Ceramic Capacitor, X7R, Size 0603	3
C8	GRM188R70J105KA01D	Murata <sup>(2)</sup>	1 $\mu$ F/6.3V Ceramic Capacitor, X7R, Size 0603	1
C9, C10	GRM188R72A104KA35D	Murata <sup>(2)</sup>	0.1 $\mu$ F/100V Ceramic Capacitor, X7R, Size 0603	2
C11	GRM188R72A102KA01D	Murata <sup>(2)</sup>	1nF/100V Cermelec Capacitor, X7R, Size 0603	1
C12	GRM188R71H103K	Murata <sup>(2)</sup>	10nF/50V Ceramic Capacitor, X7R, Size 0603	1
C14	GRM31CR60J475KA01L	Murata <sup>(2)</sup>	4.7 $\mu$ F/6.3V Ceramic Capacitor, X5R, Size 1206	1
D1	BAT46W	Diodes, Inc. <sup>(4)</sup>	100V Small Signal Schottky Diode, SOD123	1
D2	CMDZ5L6	Central Semi <sup>(5)</sup>	5.6V Zener Diode, SOD323	1
L1	HCL1305-4R0-R	Cooper Bussmann <sup>(6)</sup>	4.0 $\mu$ H Inductor, 10A RMS Current	1
Q1	SIR432DP	Vishay <sup>(7)</sup>	MOSFET, N-CH, Power SO-8	1
Q2	SIR804DP	Vishay <sup>(7)</sup>	MOSFET, N-CH, Power SO-8	1
Q3	FCX493	ZETEX <sup>(4)</sup>	100V NPN Transistor, SOT89	1
R1, R3	CRCW060310K0FKEA	Vishay Dale <sup>(7)</sup>	10k $\Omega$ Resistor, Size 0603, 1%	2
R2	CRCW08051R21FKEA	Vishay Dale <sup>(7)</sup>	1.21 $\Omega$ Resistor, Size 0805, 5%	1
R4	CRCW060380K6FKEA	Vishay Dale <sup>(7)</sup>	80.6k $\Omega$ Resistor, Size 0603, 1%	1
R5	CRCW060340K2FKEA	Vishay Dale <sup>(7)</sup>	40.2k $\Omega$ Resistor, Size 0603, 1%	1
R6	CRCW060320K0FKEA	Vishay Dale <sup>(7)</sup>	20k $\Omega$ Resistor, Size 0603, 1%	1

**Notes:**

1. EPCOS: [www.epcos.com](http://www.epcos.com).
2. Murata: [www.murata.com](http://www.murata.com).
3. Sanyo: [www.sanyo.com](http://www.sanyo.com).
4. Diodes Inc.: [www.diodes.com](http://www.diodes.com).
5. Central Semi: [www.centalsemi.com](http://www.centalsemi.com).
6. Cooper Bussmann: [www.cooperbussmann.com](http://www.cooperbussmann.com).
7. Vishay: [www.vishay.com](http://www.vishay.com).



**Bill of Materials (Continued)**

Item	Part Number	Manufacturer	Description	Qty
R7	CRCW060311K5FKEA	Vishay Dale <sup>(7)</sup>	11.5kΩ Resistor, Size 0603, 1%	1
R8	CRCW06038K06FKEA	Vishay Dale <sup>(7)</sup>	8.06kΩ Resistor, Size 0603, 1%	1
R9	CRCW06034K75FKEA	Vishay Dale <sup>(7)</sup>	4.75kΩ Resistor, Size 0603, 1%	1
R10	CRCW06033K24FKEA	Vishay Dale <sup>(7)</sup>	3.24kΩ Resistor, Size 0603, 1%	1
R11	CRCW06031K91FKEA	Vishay Dale <sup>(7)</sup>	1.91kΩ Resistor, Size 0603, 1%	1
R12	CRCW060349K24FKEA	Vishay Dale <sup>(7)</sup>	49.9Ω Resistor, Size 0603, 1%	1
R13, R21	CRCW06030000FKEA	Vishay Dale <sup>(7)</sup>	0Ω Resistor, Size 0603, 5%	2
R14	CRCW08059K7FKEA	Vishay Dale <sup>(7)</sup>	9.7kΩ Resistor, Size 0805, 5%	1
<b>U1</b>	<b>MIC2176-2YMM</b>	<b>Micrel, Inc.<sup>(8)</sup></b>	<b>75V Synchronous Buck DC-DC Regulator</b>	<b>1</b>

**Notes:**

8. Micrel, Inc.: [www.micrel.com](http://www.micrel.com).

# PCB Layout

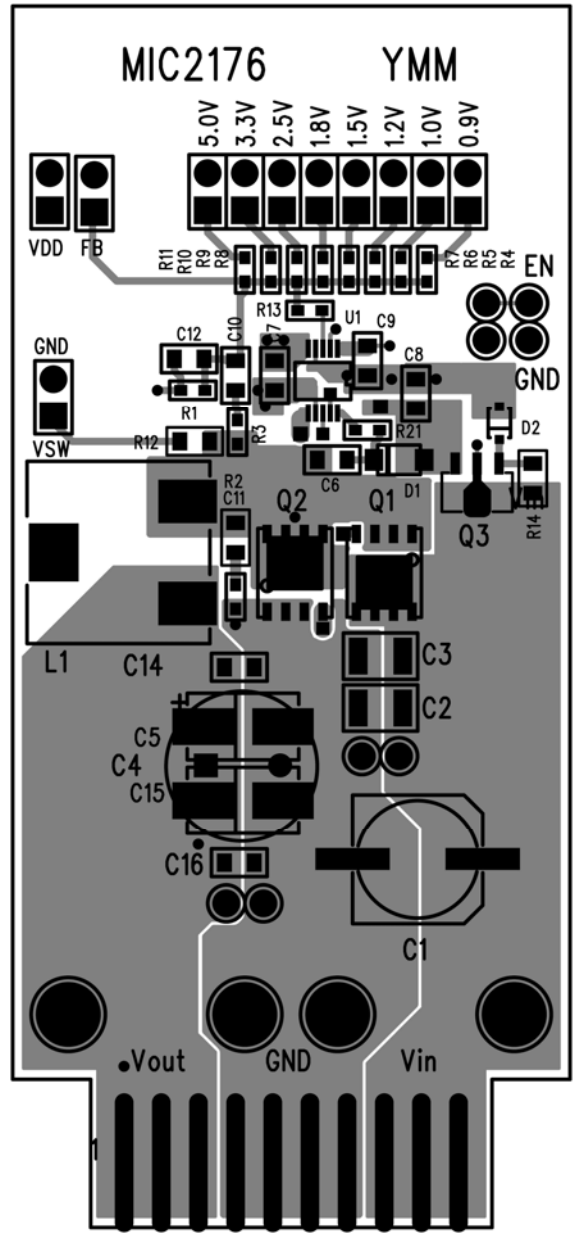


Figure 8. MIC2176 Evaluation Board Top Layer

### PCB Layout (Continued)

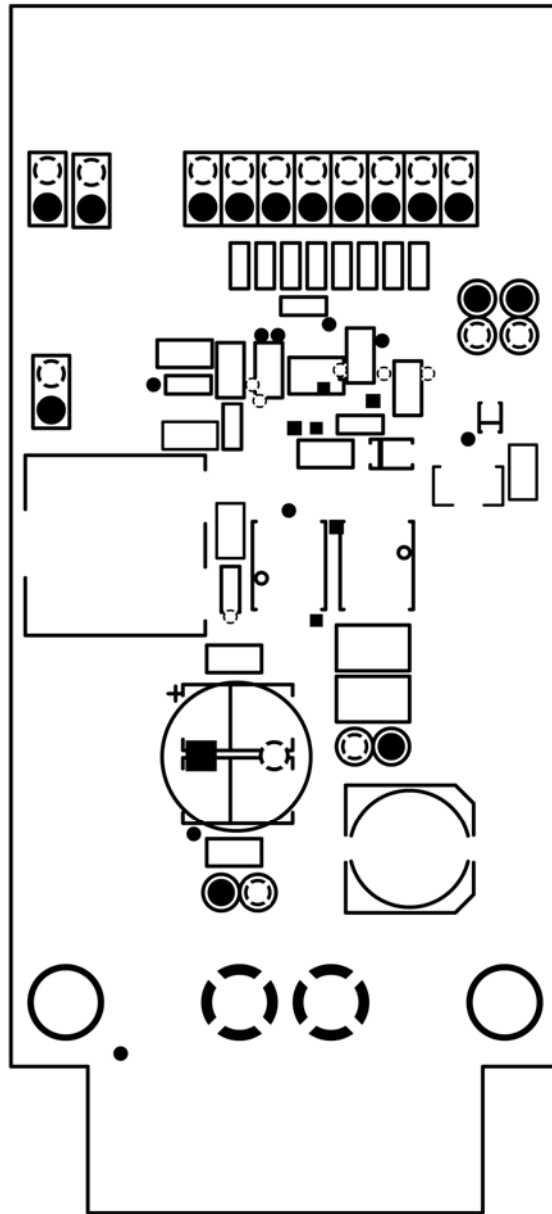


Figure 9. MIC2176 Evaluation Board Mid-Layer 1 (Ground Plane)

### PCB Layout (Continued)

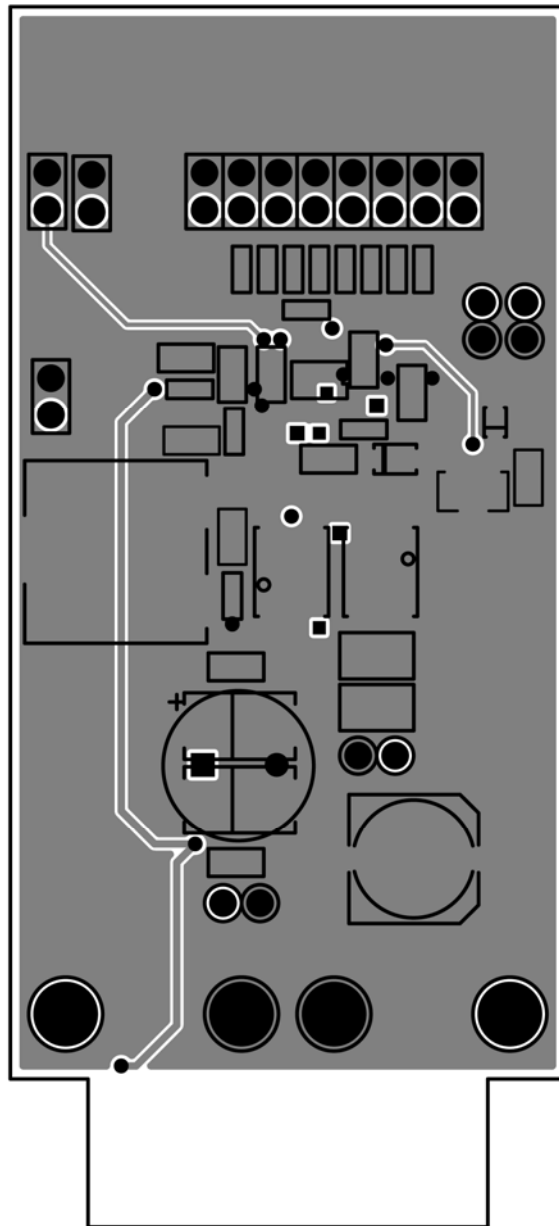


Figure 10. MIC2176 Evaluation Board Mid-Layer 2

### PCB Layout (Continued)

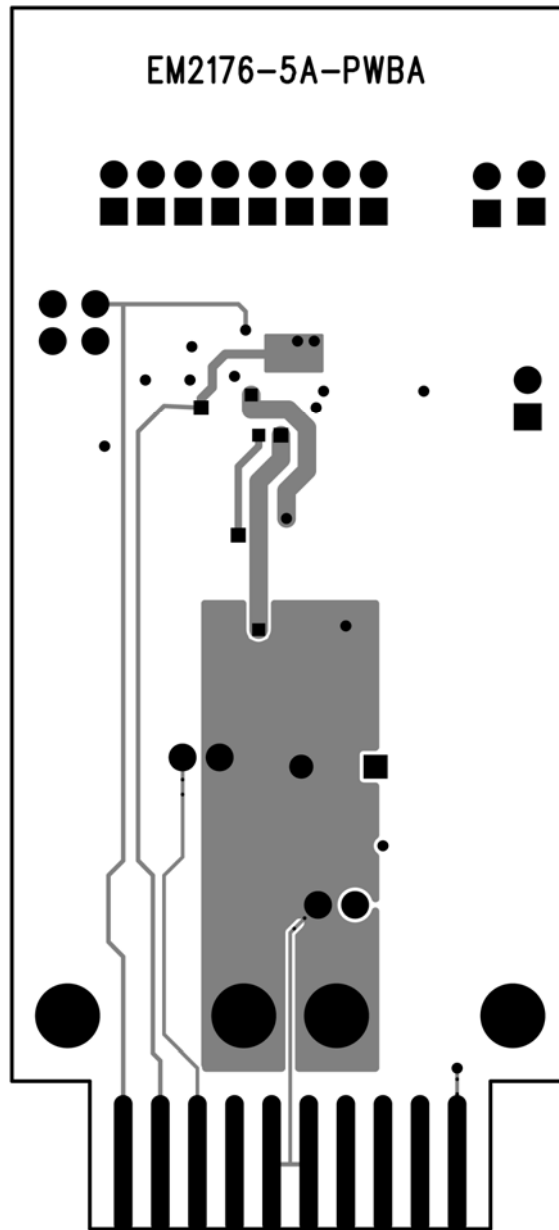


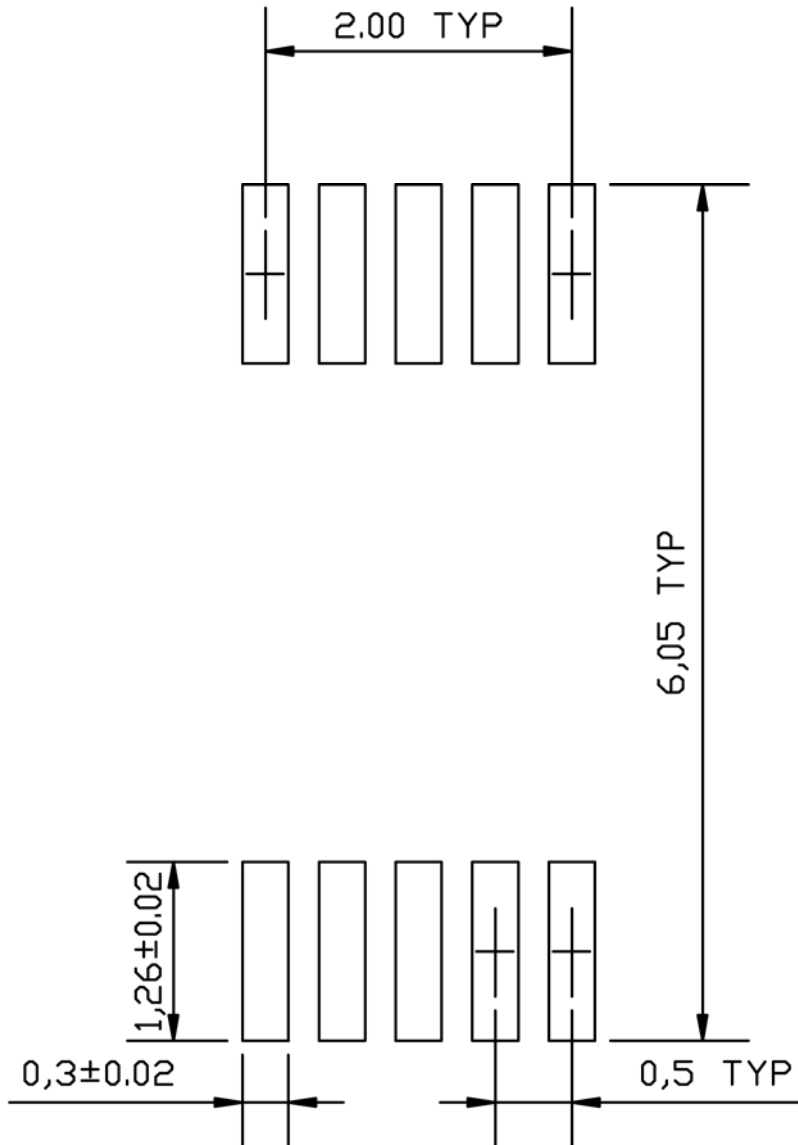
Figure 11. MIC2176 Evaluation Board Bottom Layer

### Recommended Land Pattern

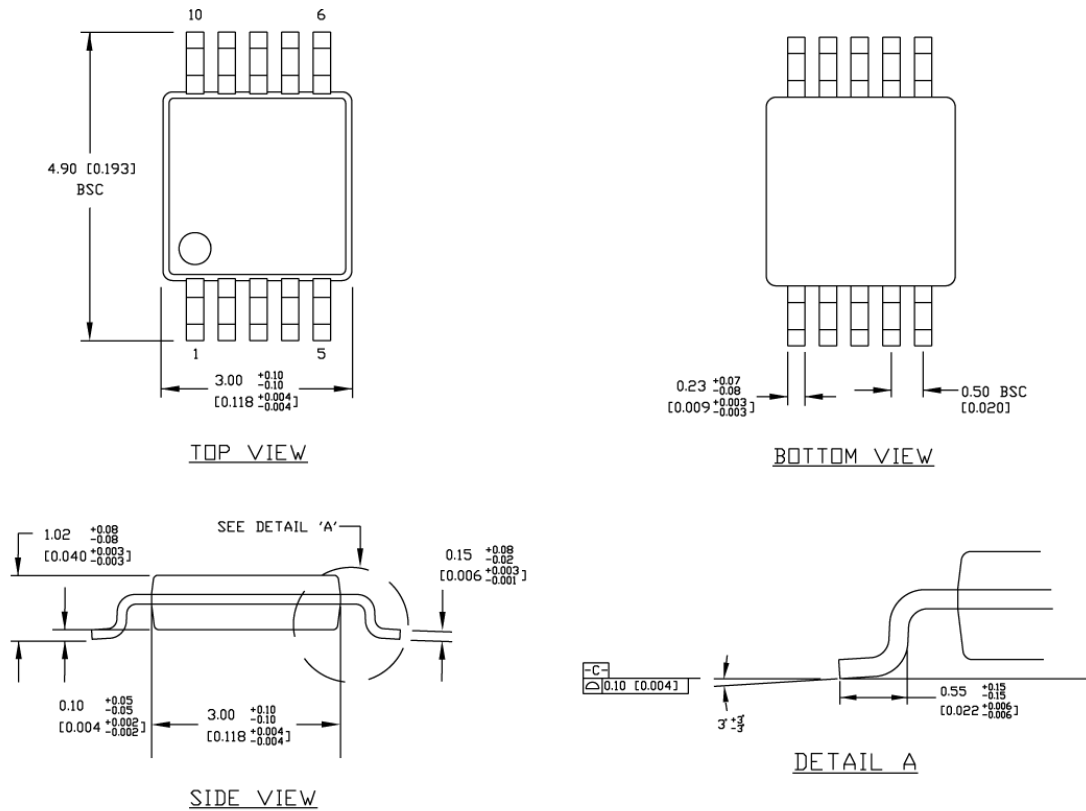
LP # MSOP-10LD-LP-1

All units are in mm

Tolerance  $\pm 0.05$  if not noted



**Package Information**



**NOTES:**

1. DIMENSIONS ARE IN MM [INCHES].
2. CONTROLLING DIMENSION: MM
3. DIMENSION DOES NOT INCLUDE MOLD FLASH OR PROTRUSIONS, EITHER OF WHICH SHALL NOT EXCEED 0.20 [0.008] PER SIDE.

**10-Pin MSOP (MM)**

**MICREL, INC. 2180 FORTUNE DRIVE SAN JOSE, CA 95131 USA**

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